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**AQUIFER TESTING SUMMARY REPORT
L.E. CARPENTER SITE
WHARTON, NEW JERSEY**

October 1996

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Prepared on Behalf of
L.E. CARPENTER AND COMPANY
for the New Jersey Department of Environmental
Protection

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TABLE OF CONTENTS

<u>Section</u>	<u>Title</u>	<u>Page</u>
1.0	INTRODUCTION.....	1-1
	1.1 Objectives	1-1
	1.2 Scope of Work	1-1
	1.3 Report Organization.....	1-1
	1.4 Site Geology	1-2
	1.5 Site Hydrogeology.....	1-2
	1.6 Groundwater Remediation Strategy.....	1-3
2.0	AQUIFER TESTING METHODOLOGY.....	2-1
	2.1 Background Trends	2-1
	2.2 Step-Drawdown Test	2-1
	2.3 Constant Rate Pumping Test	2-2
	2.4 Infiltration Test.....	2-3
	2.5 Injection Test	2-3
3.0	AQUIFER TESTING RESULTS	3-1
	3.1 Antecedent Trends	3-1
	3.2 Step-Drawdown Test	3-1
	3.3 Constant Rate Pumping Test	3-2
	3.4 Infiltration Test.....	3-3
	3.5 Injection Test	3-4
4.0	CONCLUSIONS	4-1
	4.1 Findings.....	4-1
	4.2 Conclusions.....	4-2



AQUIFER TESTING SUMMARY REPORT

LIST OF APPENDICES

Appendix A - Background Trend Data

Appendix B - Step-Drawdown Data

Appendix C - Constant Rate Pumping Test Data

Appendix D - Tables/Analytical Results of Groundwater Samples

Appendix E - Injection Test Data

Appendix F - Figures



SECTION 1.0 INTRODUCTION

Roy F. Weston, Inc. (WESTON), on behalf of L.E. Carpenter and Company, is pleased to submit this Aquifer Testing Summary Report for the former manufacturing facility located at 170 North Main Street, Borough of Wharton, Morris County, New Jersey. This report provides a summary of the aquifer testing activities performed at this site, the results and findings of these activities, and an evaluation of the results as they pertain to the selected groundwater remedial action strategy.

1.1 OBJECTIVES

The objectives of the aquifer testing activities performed at the site include the following:

- 1) To provide estimates of aquifer characteristics.
- 2) To identify the rates of water withdrawal from the aquifer beneath the site, and determine the resultant area of influence associated with a given pumping rate.
- 3) To determine the infiltration and injection rates of water into the site's vadose zone and into the shallow aquifer zone beneath the site, respectively.
- 4) To obtain data for the design and sizing of an effective and cost-efficient on-site groundwater treatment unit.

1.2 SCOPE OF WORK

The scope of work for the aquifer testing conducted at the site is outlined in the report entitled *Aquifer Testing (Aquifer Pumping Test Protocols), L.E. Carpenter Site, Wharton, New Jersey*, dated October 1995. Evaluation of the data acquired through the aquifer testing activities outlined in the above-referenced report is essential for the design of a cost-effective groundwater remediation system at the site.

1.3 REPORT ORGANIZATION

The remainder of Section 1.0 presents the site-specific geology, the site-specific hydrogeology, and a description of the groundwater remediation strategy presented in the Record of Decision (ROD). Section 2.0 presents the methodology and procedures of the aquifer testing program conducted at the site. Section 3.0 presents the results of the testing, and Section 4.0 presents the conclusions that can be drawn from these results.



1.4 SITE GEOLOGY

The site-specific geology has been developed based on lithologic and stratigraphic data collected at the site. Soil boring data collected during Second Quarter 1996 sampling activities supplemented the existing data and confirmed the geologic conceptual model. The lines of geologic cross section are presented on Figure 1. Generalized geologic cross sections are presented as Figures 2, 3, and 4 of this report.

The site-specific geology consists of unconsolidated material made up of fill material with discontinuous and heterogeneous fine-grained deposits underlying the majority of the site. These deposits extend to a depth of approximately 10 feet below grade, and are subdivided by their physical and chemical composition, color, plasticity, and organic content. At several boring locations, fine-grained materials were either not present, or were identified at a thickness of less than 0.5 feet.

Underlying these shallow deposits are highly permeable sands and gravels with little to trace amounts of silts and clays. This material extends to the top of the weathered bedrock, which was encountered between 40 and 170 feet below grade.

1.5 SITE HYDROGEOLOGY

Three hydraulically connected hydrostratigraphic (aquifer) zones are present at the site, and are identified as the shallow, the intermediate, and the deep. Monitoring points installed at the site to monitor these aquifer zones are presented in Figure 5. The shallow zone consists of the portion of the aquifer that extends from the water table to 30 feet below grade. The intermediate zone includes the portion of the aquifer that is composed of unconsolidated deposits between 30 and 50 feet below grade. The deep zone is monitored by four monitoring wells which are screened directly above or within bedrock, which is present at depths between 40 and 170 feet below grade. During the period of the aquifer testing activities, groundwater was encountered between 0.11 feet below grade (MW-14S) and 8.90 feet below grade (MW-19).

Analytical results of groundwater samples collected during previous phases of investigation indicate that the shallow aquifer zone is the only portion of the aquifer beneath the site that is chemically impacted. The primary constituents of concern (present at concentrations in excess of regulatory requirements) in the dissolved phase and non-aqueous phase include ethylbenzene, xylenes (total), and bis(2-ethylhexyl)phthalate (DEHP). Figures identifying the distribution of the Light Non Aqueous Phase Liquid (LNAPL), volatile organic compounds (VOCs), and DEHP are presented as Figures 6, 7, and 8; respectively.

Groundwater flow directions and gradients representative of the shallow and intermediate aquifer zones are presented in each of the quarterly monitoring reports that have been forwarded to the New Jersey Department of Environmental Protection (NJDEP). Within the shallow aquifer zone, groundwater predominantly flows across the site from the Rockaway River toward the drainage channel (generally west to east). The Rockaway River is a losing stream across most of the site



due to a dam that controls flow from the upstream Washington Forge Pond. These surface water bodies, Washington Forge Pond, the Rockaway River, and the drainage channel, directly impact shallow groundwater flow direction and hydraulic gradients at the site. In the intermediate aquifer zone, groundwater flow is consistently toward the east. Recent groundwater equipotential maps presented in the *Second Quarter 1996 Quarterly Monitoring Report* for the shallow and intermediate aquifer zones are presented as Figures 9 and 10 of this report, respectively.

1.6 GROUNDWATER REMEDIATION STRATEGY

Alternative #4 presented in the ROD presents the groundwater remediation strategy for the site. This alternative consists of two separate phases. Phase I encompasses the removal of immiscible product. Phase II of this strategy incorporates the extraction of groundwater, and discharge to three areas.



SECTION 2.0 AQUIFER TESTING METHODOLOGY

2.1 BACKGROUND TRENDS

Prior to performing the constant rate pumping test, background water level trends were assessed so that flow conditions in the static (non-stressed) aquifer could be evaluated. This assessment included the collection of water level measurements at select monitoring points on a continuous basis. The evaluation of water level and product thickness measurements collected over the past 3 years during quarterly monitoring events were reviewed. In addition to water level and product thickness measurements, barometric pressure readings were collected. The local National Oceanographic and Atmospheric Administration (NOAA) weather station located in Long Valley, New Jersey was contacted and provided daily precipitation measurements of July and August 1996, the months during which the aquifer testing activities were performed.

Beginning at 15:00 on 3 July 1996, water levels were measured at fifteen minute intervals using calibrated pressure transducers in monitoring points designated RW-2, MW-3, MW-14S, MW-14I, and DC-P3. Water level readings were also collected at 15-minute intervals in monitoring well MW-17S beginning at 14:00 on 3 July 1996. Barometric pressure measurements were collected simultaneously with the water level measurements. Water levels and barometric pressure readings continued at the same frequency (every 15-minutes) until the test was terminated on 8 July 1996. Data logger printouts, precipitation data, and the associated hydrographs are presented in Appendix A.

2.2 STEP-DRAWDOWN TEST

On 10 July 1996, a step-drawdown test was performed in recovery well RW-2 to identify a pumping rate for the constant rate pumping test. Water accumulated during the step-drawdown test was stored in on-site holding tanks. Prior to initiation of the step-drawdown test, water level and product thickness measurements were collected in monitoring points RW-2, MW-3, MW-14S, MW-14I, and DC-P3. (LNAPL was measured in RW-2 and MW-3 with apparent product thicknesses of 0.05 feet at each location). During the performance of the step-drawdown test, water level measurements were collected at these monitoring points using a calibrated pressure transducers to measure drawdown associated with the different pumping rates.

During the step-drawdown test, water was pumped at three successively higher rates (steps) into the on-site storage tanks. The pumping rates associated with the three steps were 15 gallons per minute (gpm), 30 gpm, and 65 gpm (the maximum rate the pump could produce). Each step lasted approximately 100 minutes. The discharge rate (Q) was measured using a calibrated in-line flow meter, which was periodically checked by measuring the time required to fill a bucket of a known volume. The data logger printout and the associated hydrographs for Recovery Well RW-2 during the step-drawdown test are presented in Appendix B.



During the performance of the step-drawdown test, product thickness measurements were collected in recovery well RW-2. These measurements indicated that during pumping, the apparent product thickness in RW-2 decreased to a sheen.

Upon conclusion of the step-drawdown test, the pump was shut off and recovery measurements were collected. Water level measurements were collected using calibrated pressure transducers installed in select monitoring points. The data logger printouts and the recovery hydrographs are presented in Appendix B.

2.3 CONSTANT RATE PUMPING TEST

On 16 July 1996, a constant rate pumping test was performed at the site between 12:40 and 18:51. The purpose of the test was to provide data for the estimation of aquifer parameters, identification of an area of influence associated with a constant pumping rate, and to obtain data for the design and sizing of a groundwater treatment unit. During the test, RW-2 was pumped at a constant rate of 150 gpm for 371 minutes. All water acquired during the test was stored in on-site storage tanks. During the test, Q was periodically measured using a calibrated in-line flow meter.

Prior to, during, and after the constant rate pumping test, water level and product thicknesses were measured at monitoring points at the site to determine the effects of pumping on the aquifer.

Prior to the constant rate pumping test, a complete round of water level and product thickness measurements were collected from all of the site's monitoring points. Figure 11 and Figure 12 present the equipotential maps of pre-pumping conditions in the shallow and intermediate aquifer zones, respectively. Upon initiation of pumping, water levels were measured continuously with calibrated pressure transducers at monitoring points RW-2, MW-2R, MW-3, MW-6R, MW-14S, MW-14I, MW-15I, MW-17S, and DC-P3. In addition to the continuous measurements collected from the above-listed monitoring points, periodic water level and product thickness measurements were collected from many of the site's monitoring points. In addition, a complete round of measurements were collected prior to termination of pumping. Figure 13 and Figure 14 present the equipotential maps for the shallow and intermediate aquifer zones under pumping conditions. Upon termination of pumping, recovery water level readings were measured continuously using calibrated pressure transducers at monitoring points RW-2, MW-2R, MW-3, MW-6R, MW-14S, MW-14I, MW-15I, MW-17S, and DC-P3. The data logger printouts, data tables presenting the corrected water level elevations from the two synoptic rounds of water levels and product measurements, and associated hydrographs are presented in Appendix C.

During the constant rate pumping test, two groundwater samples were collected from a sampling port installed in the discharge line from RW-2. The first sample, GW-1, was collected 60 minutes (13:40 on 16 July 1996) after the start of the constant rate pumping test. The second sample, GW-2, was collected 350 minutes (18:20 on 16 July 1996) after the start of the constant rate pumping test. The analytical results are presented in Table 1 of Appendix D.



2.4 INFILTRATION TEST

On 11 July 1996, during a period of no precipitation, a 14-hour infiltration test was performed at the site to develop design parameters for in-situ soil bioremediation and a groundwater infiltration system which would manage (dispose of) recovered groundwater acquired during the performance of the selected groundwater remedial action. This test was conducted in the pilot-scale infiltration gallery constructed at the site using groundwater acquired during the step-drawdown test.

During the infiltration test, manual measurements were collected from monitoring points in the vicinity of the pilot-scale infiltration gallery, using calibrated oil/water interface probes and electronic water level indicators. These measurements were taken to identify mounding of groundwater associated with the infiltration of water into the vadose zone. In addition to groundwater level monitoring, two temporary "staff gauges" were installed within pooled surface water in the former Waste Disposal Area (WDA). Monitoring of these "staff gauges" would identify horizontal leakage, if it occurred, out of the sides of the pilot-scale infiltration gallery during the test.

Flow rates into the pilot-scale system were adjusted during the infiltration test to determine the optimum rate for infiltration. For the initial 108 minutes into the test, water was pumped from the on-site storage tanks into the pilot-scale infiltration gallery at 5.2 gpm. After 108 minutes, the flow rate was increased to 10.0 gpm. After pumping for 145 minutes at 10.0 gpm (a total of approximately 2010 gallons of water), water was identified migrating through the surface cover over the infiltration gallery, and pooling on ground surface. Water level measurements collected in the drop-pipe of the infiltration gallery indicated that the water level in the gallery was above ground surface. In addition, the puddles identified in the former WDA began to increase in size and depth as measured from the temporary "staff gauges". As a result of these observations, flow into the infiltration gallery was terminated for 30 minutes, after which infiltration was started again at a rate of 3.5 gpm. Flow into the gallery continued at 3.5 gpm for 120 minutes during which time the water level in the drop-pipe rose to a level that corresponds to above ground surface. As a result, the flow rate was reduced to 2.8 gpm for a period of 225 minutes during which time the submersible pump overheated. After a 7-minute pumping hiatus, a replacement pump was turned on and pumped for 323 minutes at 2.6 gpm. At the conclusion of pumping at 2.6 gpm for 323 minutes, the test was terminated because of groundwater mounding, and horizontal leakage from the pilot-scale system.

2.5 INJECTION TEST

As part of the aquifer testing conducted at the site, an injection test was performed in the shallow aquifer zone to identify a rate at which water could be injected into it. This test, in conjunction with the infiltration test, was performed to determine disposal rates for the recovered groundwater during the performance of the selected groundwater remedial action. The injection test was conducted in Caisson Well CW-1 using groundwater acquired during the constant rate pumping test.



On 17 July 1996, a test using CW-1 as the injection point was initiated. Due to a flow meter malfunction, and an initially high injection rate (12 gpm), the test was terminated after injecting 172 gallons.

On 18 July 1996, after allowing the aquifer to recover from the 17 July testing, an injection test was performed at the site. Prior to and during the injection test, water level and product thickness measurements were collected in monitoring points in the vicinity of CW-1. In addition, at monitoring points CW-1, MW-2R, MW-6R, MW-11I, MW-15I, MW-17S, WP-B2, WP-B5, and WP-B10, water levels were collected continuously with calibrated pressure transducers. In addition, barometric pressure readings were collected at the same frequency as water level measurements which were monitored using pressure transducers. The data logger printouts are provided in Appendix E.

Water was pumped from the on-site tankers at 2.1 gpm into CW-1 for 543 minutes. After 543 minutes, the injection flow rate increased to 2.25 gpm. Injection continued at 2.25 gpm for 685 minutes until the water level in CW-1 rose to an access hole installed in the riser of CW-1. The injection flow rate was then reduced to 1.9 gpm for 5 hours at which time the test was terminated.



SECTION 3.0 AQUIFER TESTING RESULTS

3.1 BACKGROUND TRENDS

The general trends in groundwater levels, as well as the effects of barometric pressure and precipitation on the aquifer beneath the site, were analyzed as part of the background trends evaluation conducted as part of the aquifer testing activities. In general, there was a decline in groundwater levels in all of the monitoring points. A comparison of groundwater levels in monitoring points RW-2, MW-3, MW-14S, and MW-14I indicated these wells had similar responses due to the effects of precipitation and barometric pressure. During the period of background trend monitoring, precipitation (rainfall) occurred on 4 July (0.13 inches) and 5 July (0.08 inches). Barometric pressure, as monitored using the calibrated barometric pressure transducer connected to a data logger, fluctuated between a low of 32.69818 feet of water (16:00, 3 July) and a high of 33.27948 feet of water (01:15, July 6).

Barometric pressure effects on groundwater levels (specifically at MW-14S and MW-14I, locations where LNAPL has not been identified) were evaluated during specific periods of no precipitation (3 and 7 July). No direct correlation between barometric pressure and groundwater levels was distinguishable based on an evaluation of the collected data, which is not unusual in water table aquifers. As a result of the evaluation of the barometric data, the correction of groundwater levels for barometric effects was not required.

Precipitation as rainfall occurred on 4 and 5 July (the period of 540 through 3405 minutes into the background trend monitoring). This limited amount of rainfall resulted in temporary increases in the otherwise declining trend of groundwater levels beneath the site. As a result of the data gathered, short-term precipitation events of limited intensity have slight effect on general groundwater trends in the monitoring wells and piezometers. Water level trends in the drainage channel were in general, similar to those observed in the monitoring wells and piezometers. However, short duration water level increases were noted during periods of no precipitation and may represent discharges to the drainage channel through outfalls at the Air Products facility. Hydrographs presenting the background trends are in Appendix A.

3.2 STEP-DRAWDOWN TEST

The performance of the step-drawdown test and evaluation of the resultant data provided insight into Recovery Well RW-2's yield; specific capacity; component of head loss due to laminar flow; an estimate of the aquifer's transmissivity (T); and an estimate of the aquifer's hydraulic conductivity (K). Worksheets in Appendix B present the calculations made for these variables and aquifer parameters. A "T" estimate of 19.3 square centimeters per second (cm^2/sec), and a "K" estimate of 1.91×10^{-3} centimeters per second (cm/second) were calculated. This "K" value falls within the expected range of values for well-sorted sands, glacial outwash (Fetter, 1988, p.80).



3.3 CONSTANT RATE PUMPING TEST

Due to the lack of precipitation and the limited duration of the test, water levels did not require correction for barometric pressure and precipitation effects. At monitoring points where LNAPL was present, water levels were corrected using the method presented in previous quarterly reports (WESTON, April 1992). This formula is the following:

$$(\text{Static Depth to Water}) - (\text{Apparent Product Thickness} \times \text{Specific Gravity}) = \text{Corrected Depth to Water}$$

At monitoring points where field specific gravity tests were performed, the results of these field-tests were used in the correction of water level elevations. A summary of the field-determined specific gravity results are presented in Table 2 of Appendix D.

Data from the constant rate pumping test were analyzed using AQTESOLV Version 2.01. Several analytical methods within this program were used to calculate aquifer parameters. The Theis (1935) type curve solution, the Cooper-Jacob (1946) straight line solution, and the Neuman (1974) Type A and Type B curve solution were used to estimate aquifer characteristics.

Analysis of the constant rate drawdown data by the methods presented above produced values for "T", the coefficient of storage (S), specific yield (Sy), and hydraulic conductivity (K) of the aquifer. "T" values ranged between 55.61 cm²/sec and 330.3 cm²/sec. "S" values ranged between 8.65E-04 and 1.28E-01, and "Sy" values ranged between 7.58E-03 and 1.66E-02. "K" values ranged between 9.37E-02 cm/sec and 1.55E-01 cm/sec. Geometric and arithmetic means were calculated for "K", and are within the expected ranges established for an aquifer consisting of well-sorted sands, glacial outwash (Fetter, 1988, p.80). The geometric and arithmetic means of "S" of the aquifer at the site are close to the range (0.02 to 0.30) presented for unconfined aquifers (Fetter, p.107). The calculated values of these aquifer parameters by each method of analysis are presented in Table 3 of Appendix C. The AQTESOLV Version 2.01 printouts are presented in Appendix C.

Evaluation of groundwater level measurements collected during the aquifer test identified drawdown in the shallow and intermediate aquifer zones. Drawdowns in monitoring points screened in the shallow aquifer zone were impacted by the heterogeneous nature of the unconsolidated deposits. Table 4 in Appendix C presents the change in corrected water level elevations between the two synoptic water level rounds measured on 16 July 1996.

The presence of the surface water bodies impacted the drawdown curve associated with the pumping well. This is displayed on the drawdown plot of RW-2 by the flattening of the drawdown curve, which indicates that an apparent recharge boundary was encountered. A radius of influence of 35 feet was calculated based on the constant rate pumping test results, although drawdowns were measured at greater distances from the pumping well. The presence of heterogeneous low permeability deposits in the shallow aquifer zone may have influenced drawdown in several of the monitoring points. Whether an observation showed the influence of

pumping, appeared to depend on the materials the well penetrated. For example, Monitoring Well MW-6R, which is approximately 105 feet from RW-2, identified a drawdown of approximately 1.10 feet, and Well Point WP-C3, which is 335 feet from RW-2, identified a drawdown 2.11 feet. Drawdown contour maps for the shallow and intermediate aquifer zones are presented on Figure 15 and Figure 16, respectively. This difference in drawdown suggests that some of the monitoring points are locally confined. The calculations to determine a radius of influence is presented in Appendix C.

Measurements of product levels collected in RW-2 and MW-3 did not indicate a change in product thickness during the performance of the constant rate pumping test. A summary of product levels collected during the test are presented in summary tables in Appendix C.

Results of the groundwater samples collected from the discharge water from RW-2 indicated the presence of ethylbenzene, xylene (total), and bis(2-ethylhexyl)phthalate (DEHP) at concentrations above the relevant groundwater quality standards (GWQS). In sample GW-1, ethylbenzene, xylene (total), and DEHP were detected at concentrations of 460 micrograms per liter (ug/L), 1,400 ug/L, and 670 ug/L, respectively. In sample GW-2, ethylbenzene, xylene (total), and DEHP were detected at concentrations of 180 ug/L, 630 ug/L, and 68 ug/L, respectively. Arsenic, iron, and manganese were detected above GWQS in both groundwater samples. Samples collected for lead analysis indicated that lead was not present at the laboratory's method detection limit (MDL) of 2.3 ug/L. Due to the sampling method employed, there is a potential that lower concentrations of chemical constituents are present in the shallow aquifer zone.

3.4 INFILTRATION TEST

During the infiltration test, manual water level and product thickness measurements were collected from monitoring points in the vicinity of the pilot-scale infiltration gallery using calibrated oil/water interface probes and electronic water level indicators. Mounding was identified in monitoring points MW-6R (0.76 feet) and WP-B6 (0.07 feet), which are between the pilot-scale infiltration gallery and the Rockaway River. In addition, ponded surface water in the WDA in proximity to pilot-scale gallery increased in size and depth during the test. As a result of these conditions, mounding towards the Rockaway River, and horizontal seepage out of the sidewalls of the gallery, the test was terminated.

On 12 July 1996, an additional round of water level and product thickness measurements were collected from select monitoring points. The water level in WP-B6 continued to rise an additional 0.24 feet throughout the night after the termination of the test for a total increase in water level of 0.31 feet since commencement of the test. The water level in MW-6R, as well as at the additional monitoring points declined to near pre-test levels. Performance of this test identified that the infiltration of water into the vadose zone can be performed at a rate of 3 gpm, and at this low rate, a groundwater mound developed. A percolation rate of 0.01 gpm per square foot was calculated based on the 2.6 gpm infiltration rate divided by the 150 square foot area of the infiltration gallery.



3.5 INJECTION TEST

Groundwater levels were monitored continuously in CW-1 (the injection point), MW-2R, MW-6R, MW-11I, MW-15I, MW-17S, WP-B2, WP-B5, and WP-B10 with a calibrated pressure transducer set into each monitoring point. Of the locations monitored, increases in water levels were identified in only two monitoring points: CW-1 (6.13 feet) and MW-6R (0.11 feet). Performance of this test identified that the injection of water into the upper portion of the shallow aquifer zone can only be performed at a very low rate (less than 2 gpm).



SECTION 4.0

FINDINGS AND CONCLUSIONS

4.1 FINDINGS

The findings of the Aquifer Testing Program conducted during July 1996 at the L.E. Carpenter Site in Wharton, New Jersey can be summarized as follows:

- The chemically impacted portion of the aquifer beneath the site includes shallow fine-grained materials and deeper, well-sorted, coarse-grained materials. These deeper coarse-grained materials have been determined to be capable of yielding large quantities of water, as represented by the pumping test results from RW-2, which demonstrated a sustainable yield of more than 150 gpm.
- The high permeability of the deeper, well-sorted, coarse-grained materials has been confirmed by calculated "K" values which ranged from 1.55E-01 cm/sec to 9.37E-02 cm/sec in RW-2 and observation wells across the site.
- Drawdown observed in on-site monitoring points indicates the influence of fine-grained, low permeability materials in the subsurface and nearby surface water bodies. Drawdown was also observed in the intermediate aquifer zone at monitoring wells MW-11I, MW-13I, and MW-14I, indicating hydraulic communication between the non-impacted intermediate aquifer zone and the overlying shallow aquifer zone.
- Infiltration (less than 3 gpm) and injection (less than 2 gpm) of water into the shallow aquifer zone can only occur at very low rates. Even at such low rates, groundwater mounding was observed in the vicinity of the pilot infiltration gallery during the short-term injection and infiltration testing.
- Laboratory analysis of groundwater samples collected from RW-2 under pumping conditions indicates elevated concentrations of chemical constituents. However, the analytical data indicate a decrease in concentration with pumping duration: ethylbenzene decreased from 460 ug/L to 180 ug/L, xylenes (total) decreased from 1,400 ug/L to 630 ug/L, and DEHP decreased from 670 ug/L to 68ug/L.
- Based on the calculated radius of influence of 35 feet for pumping well RW-2 during the constant rate drawdown test, it is estimated that 3 to 5 wells would be required for capture of the groundwater contaminant plume at the site. The volume of groundwater from the combined discharge of these recovery wells would be several orders of magnitude in excess of the volume that could be infiltrated or injected into the vadose zone or shallow aquifer zone beneath the site.



- Analysis of the background groundwater trends for the site indicates that water levels in both the shallow and intermediate aquifer zone respond similarly to precipitation events. In addition, barometric effects did not directly affect water levels in the monitoring points.
- Groundwater levels observed at monitoring point DC-P3 identified short duration water level increases that do not correlate to precipitation events or barometric fluctuations. These increases are attributed to other influences, and may represent discharges to the drainage channel from outfalls located on the Air Products property.
- Based on the infiltration results for the area in and around the pilot infiltration gallery, a percolation rate of 0.01 gpm per square foot of infiltration area was calculated under ideal weather conditions (i.e. no precipitation). Precipitation events and other influences (i.e. snowmelt, localized fine-grained materials) may reduce this percolation rate.

4.2 CONCLUSIONS

Based on the findings of the Aquifer Testing Program, the following conclusions are made with regard to the consideration of future remedial alternatives for the L.E. Carpenter Site:

- Based on the observed well yield of RW-2, the combined discharge rates of the number of recovery wells required to maintain capture and containment in the shallow aquifer zone would far exceed the volume of water that could be infiltrated or injected into the vadose zone or shallow aquifer zone at the site. Surplus water would have to be managed through alternative methods of disposal (i.e. enhanced treatment and intermediate/deep aquifer zone re-injection or discharge to the surface water or POTW).
- Drawdown data indicate that the radius of influence of RW-2 extends to include adjacent surface water bodies and to off-site monitoring points. This condition may result in the capture of large quantities of uncontaminated groundwater from the Rockaway River and potentially contaminated groundwater from off-site sources (i.e. Air Products, Inc.).



APPENDIX A
BACKGROUND TREND DATA

Real Time	Elapsed Time	RW-2				MW-3				14S				14I				DC-P3				Atmospheric Pressure		
		Reference Value	Adjusted DTW	Water Level Elevation	Delta H	Reference Value	Adjusted DTW	Water Level Elevation	Delta H	Reference Value	Adjusted DTW	Water Level Elevation	Delta H	Reference Value	Adjusted DTW	Water Level Elevation	Delta H	Reference Value	Adjusted DTW	Water Level Elevation	Delta H	Ft H2O	Delta P	
03-Jul-96	15:00	0	100	6.68	625	0.089	100	7.28	625.28	0.064	100	3.78	624.63	0.096	99.993	8.253	624.977	0.05	99.993	0.773	624.447	0.126	32.70972	0.034605
	15:15	15	100	6.68	625	0.089	100.006	7.286	625.274	0.07	100	3.78	624.63	0.096	100	3.26	624.97	0.057	99.981	0.761	624.459	0.114	32.71433	0.039219
	15:30	30	100	6.68	625	0.089	100.006	7.286	625.274	0.07	100.006	3.786	624.624	0.102	100	3.26	624.97	0.057	99.981	0.761	624.459	0.114	32.70972	0.034605
	15:45	45	100.006	6.686	624.994	0.095	100.006	7.286	625.274	0.07	100.012	3.792	624.618	0.108	100	3.26	624.97	0.057	99.981	0.761	624.459	0.114	32.7051	0.029992
	16:00	60	100.006	6.686	624.994	0.095	100.006	7.286	625.274	0.07	100.006	3.786	624.624	0.102	100	3.26	624.97	0.057	99.974	0.754	624.466	0.107	32.69818	0.023071
	16:15	75	100.006	6.686	624.994	0.095	100.006	7.286	625.274	0.07	100.006	3.786	624.624	0.102	100	3.26	624.97	0.057	99.974	0.754	624.466	0.107	32.70049	0.025378
	16:30	90	100.018	6.698	624.982	0.107	100.012	7.292	625.268	0.076	100.006	3.786	624.624	0.102	100.012	3.272	624.958	0.069	99.974	0.754	624.466	0.107	32.71894	0.043832
	16:45	105	100.006	6.686	624.994	0.095	100.006	7.286	625.274	0.07	99.987	3.767	624.643	0.083	100	3.26	624.97	0.057	99.968	0.748	624.472	0.101	32.71433	0.039219
	17:00	120	99.987	6.667	625.013	0.076	99.993	7.273	625.287	0.057	99.917	3.697	624.713	0.013	99.968	3.228	625.002	0.025	99.892	0.672	624.548	0.025	32.69587	0.020765
	17:15	135	99.962	6.642	625.038	0.051	99.98	7.26	625.3	0.044	99.917	3.697	624.713	0.013	99.962	3.222	625.008	0.019	99.867	0.647	624.573	0	32.68203	0.006924
	17:30	150	99.955	6.635	625.045	0.044	99.974	7.254	625.306	0.038	99.904	3.684	624.726	0	99.949	3.209	625.021	0.006	99.886	0.666	624.554	0.019	32.67511	3.75E-06
	17:45	165	99.955	6.635	625.045	0.044	99.974	7.254	625.306	0.038	99.917	3.697	624.713	0.013	99.955	3.215	625.015	0.012	99.905	0.685	624.535	0.038	32.70279	0.027685
	18:00	180	99.949	6.629	625.051	0.038	99.974	7.254	625.306	0.038	99.923	3.703	624.707	0.019	99.962	3.222	625.008	0.019	99.905	0.685	624.535	0.038	32.72125	0.046139
	18:15	195	99.949	6.629	625.051	0.038	99.974	7.254	625.306	0.038	99.93	3.71	624.7	0.026	99.962	3.222	625.008	0.019	99.911	0.691	624.529	0.044	32.73278	0.057673
	18:30	210	99.943	6.623	625.057	0.032	99.974	7.254	625.306	0.038	99.93	3.71	624.7	0.026	99.955	3.215	625.015	0.012	99.911	0.691	624.529	0.044	32.7397	0.064593
	18:45	225	99.936	6.616	625.064	0.025	99.968	7.248	625.312	0.032	99.93	3.71	624.7	0.026	99.955	3.215	625.015	0.012	99.911	0.691	624.529	0.044	32.73278	0.057673
	19:00	240	99.93	6.61	625.07	0.019	99.968	7.248	625.312	0.032	99.93	3.71	624.7	0.026	99.949	3.209	625.021	0.006	99.911	0.691	624.529	0.044	32.73278	0.057673
	19:15	255	99.93	6.61	625.07	0.019	99.961	7.241	625.319	0.025	99.93	3.71	624.7	0.026	99.949	3.209	625.021	0.006	99.911	0.691	624.529	0.044	32.74201	0.0669
	19:30	270	99.924	6.604	625.076	0.013	99.955	7.235	625.325	0.019	99.93	3.71	624.7	0.026	99.949	3.209	625.021	0.006	99.911	0.691	624.529	0.044	32.72817	0.053059
	19:45	285	99.917	6.597	625.083	0.006	99.955	7.235	625.325	0.019	99.923	3.703	624.707	0.019	99.943	3.203	625.027	0	99.911	0.691	624.529	0.044	32.72586	0.050752
	20:00	300	99.917	6.597	625.083	0.006	99.955	7.235	625.325	0.019	99.93	3.71	624.7	0.026	99.949	3.209	625.021	0.006	99.911	0.691	624.529	0.044	32.73278	0.057673
	20:15	315	99.917	6.597	625.083	0.006	99.955	7.235	625.325	0.019	99.93	3.71	624.7	0.026	99.949	3.209	625.021	0.006	99.911	0.691	624.529	0.044	32.7397	0.064593
	20:30	330	99.924	6.604	625.076	0.013	99.955	7.235	625.325	0.019	99.93	3.71	624.7	0.026	99.949	3.209	625.021	0.006	99.911	0.691	624.529	0.044	32.74893	0.07382
	20:45	345	99.917	6.597	625.083	0.006	99.948	7.228	625.332	0.012	99.93	3.71	624.7	0.026	99.949	3.209	625.021	0.006	99.911	0.691	624.529	0.044	32.74893	0.07382
	21:00	360	99.917	6.597	625.083	0.006	99.948	7.228	625.332	0.012	99.93	3.71	624.7	0.026	99.949	3.209	625.021	0.006	99.911	0.691	624.529	0.044	32.75124	0.076127
	21:15	375	99.917	6.597	625.083	0.006	99.948	7.228	625.332	0.012	99.93	3.71	624.7	0.026	99.943	3.203	625.027	0	99.911	0.691	624.529	0.044	32.75124	

Real Time	Elapsed Time	RW-2				MW-3				14S				14I				DC-P3				Atmospheric Pressure		
		Reference Value	Adjusted DTW	Water Level (ft H2O)	Delta H (ft H2O)	Reference Value	Adjusted DTW	Water Level (msl)	Delta H (ft H2O)	Reference Value	Adjusted DTW	Water Level (ft H2O)	Elevation (ft H2O)	Delta H (ft H2O)	Reference Value	Adjusted DTW	Water Level (ft H2O)	Elevation (msl)	Delta H (ft H2O)	Reference Value	Adjusted DTW	Water Level (ft H2O)	Elevation (msl)	Delta H (ft H2O)
3:00	720	99.924	6.604	625.076	0.013	99.942	7.222	625.338	0.006	99.942	3.722	624.688	0.038	99.949	3.209	625.021	0.006	99.93	0.71	624.51	0.063	32.75354	0.078433	
3:15	735	99.924	6.604	625.076	0.013	99.942	7.222	625.338	0.006	99.942	3.722	624.688	0.038	99.949	3.209	625.021	0.006	99.93	0.71	624.51	0.063	32.74893	0.07382	
3:30	750	99.924	6.604	625.076	0.013	99.936	7.216	625.344	0	99.942	3.722	624.688	0.038	99.949	3.209	625.021	0.006	99.93	0.71	624.51	0.063	32.74432	0.069206	
3:45	765	99.924	6.604	625.076	0.013	99.942	7.222	625.338	0.006	99.942	3.722	624.688	0.038	99.955	3.215	625.015	0.012	99.93	0.71	624.51	0.063	32.74893	0.07382	
4:00	780	99.924	6.604	625.076	0.013	99.942	7.222	625.338	0.006	99.942	3.722	624.688	0.038	99.955	3.215	625.015	0.012	99.93	0.71	624.51	0.063	32.74662	0.071513	
4:15	795	99.93	6.61	625.07	0.019	99.942	7.222	625.338	0.006	99.942	3.722	624.688	0.038	99.955	3.215	625.015	0.012	99.93	0.71	624.51	0.063	32.75124	0.076127	
4:30	810	99.93	6.61	625.07	0.019	99.942	7.222	625.338	0.006	99.942	3.722	624.688	0.038	99.955	3.215	625.015	0.012	99.93	0.71	624.51	0.063	32.74893	0.07382	
4:45	825	99.93	6.61	625.07	0.019	99.942	7.222	625.338	0.006	99.942	3.722	624.688	0.038	99.955	3.215	625.015	0.012	99.93	0.71	624.51	0.063	32.74662	0.071513	
5:00	840	99.93	6.61	625.07	0.019	99.942	7.222	625.338	0.006	99.942	3.729	624.681	0.045	99.955	3.215	625.015	0.012	99.93	0.71	624.51	0.063	32.74432	0.069206	
5:15	855	99.93	6.61	625.07	0.019	99.942	7.222	625.338	0.006	99.942	3.722	624.688	0.038	99.955	3.215	625.015	0.012	99.93	0.71	624.51	0.063	32.75124	0.076127	
5:30	870	99.936	6.616	625.064	0.025	99.948	7.228	625.332	0.012	99.949	3.729	624.681	0.045	99.955	3.215	625.015	0.012	99.936	0.716	624.504	0.069	32.75124	0.076127	
5:45	885	99.943	6.623	625.057	0.032	99.948	7.228	625.332	0.012	99.949	3.729	624.681	0.045	99.962	3.222	625.008	0.019	99.936	0.716	624.504	0.069	32.75585	0.08074	
6:00	900	99.936	6.616	625.064	0.025	99.948	7.228	625.332	0.012	99.949	3.729	624.681	0.045	99.962	3.222	625.008	0.019	99.936	0.716	624.504	0.069	32.76508	0.089967	
6:15	915	99.943	6.623	625.057	0.032	99.948	7.228	625.332	0.012	99.949	3.729	624.681	0.045	99.962	3.222	625.008	0.019	99.936	0.716	624.504	0.069	32.76738	0.092274	
6:30	930	99.943	6.623	625.057	0.032	99.948	7.228	625.332	0.012	99.955	3.735	624.675	0.051	99.962	3.222	625.008	0.019	99.936	0.716	624.504	0.069	32.76969	0.094581	
6:45	945	99.943	6.623	625.057	0.032	99.948	7.228	625.332	0.012	99.955	3.735	624.675	0.051	99.962	3.222	625.008	0.019	99.936	0.716	624.504	0.069	32.772	0.096887	
7:00	960	99.943	6.623	625.057	0.032	99.948	7.228	625.332	0.012	99.955	3.735	624.675	0.051	99.962	3.222	625.008	0.019	99.936	0.716	624.504	0.069	32.7743	0.099194	
7:15	975	99.943	6.623	625.057	0.032	99.948	7.228	625.332	0.012	99.955	3.735	624.675	0.051	99.962	3.222	625.008	0.019	99.936	0.716	624.504	0.069	32.7743	0.099194	
7:30	990	99.943	6.623	625.057	0.032	99.948	7.228	625.332	0.012	99.955	3.735	624.675	0.051	99.962	3.222	625.008	0.019	99.936	0.716	624.504	0.069	32.78353	0.108421	
7:45	1005	99.949	6.629	625.051	0.038	99.955	7.235	625.325	0.019	99.961	3.741	624.669	0.057	99.962	3.222	625.008	0.019	99.943	0.723	624.497	0.076	32.79045	0.115341	
8:00	1020	99.949	6.629	625.051	0.038	99.955	7.235	625.325	0.019	99.961	3.741	624.669	0.057	99.962	3.222	625.008	0.019	99.943	0.723	624.497	0.076	32.79276	0.117648	
8:15	1035	99.949	6.629	625.051	0.038	99.961	7.241	625.319	0.025	99.961	3.741	624.669	0.057	99.962	3.222	625.008	0.019	99.936	0.716	624.504	0.069	32.79506	0.119955	
8:30	1050	99.949	6.629	625.051	0.038	99.955	7.235	625.325	0.019	99.961	3.741	624.669	0.057	99.968	3.228	625.002	0.025	99.943	0.723	624.497	0.076	32.79968	0.124568	
8:45	1065	99.949	6.629	625.051	0.038	99.961	7.241	625.319	0.025	99.961	3.741	624.669	0.057	99.962	3.222	625.008	0.019	99.943	0.723	624.497	0.076	32.79968	0.124568	
9:00	1080	99.955	6.635	625.045	0.044	99.961	7.241	625.319	0.025	99.968	3.748	624.662	0.064	99.968	3.228	625.002	0.025	99.943	0.723	624.497	0.076	32.80199	0.126875	
9:15	1095	99.955	6.635	625.045	0.044	99.968	7.248	625.312	0.032	99.968	3.748	624.662	0.064	99.9										

Real Time	Elapsed Time	RW-2				MW-3				14S				14I				DC-P3				Atmospheric Pressure	
		Reference Value	Adjusted DTW	Water Level (ft H2O)	Elevation (msl)	Reference Value	Adjusted DTW	Water Level (ft H2O)	Elevation (msl)	Reference Value	Adjusted DTW	Water Level (ft H2O)	Elevation (msl)	Reference Value	Adjusted DTW	Water Level (ft H2O)	Elevation (msl)	Reference Value	Adjusted DTW	Water Level (ft H2O)	Elevation (msl)	Ft H2O	Delta P
15:00	1440	99.981	6.661	625.019	0.07	99.987	7.267	625.293	0.051	99.98	3.76	624.65	0.076	99.981	3.241	624.989	0.038	99.943	0.723	624.497	0.076	32.87119	0.196078
15:15	1455	99.981	6.661	625.019	0.07	99.987	7.267	625.293	0.051	99.987	3.767	624.643	0.083	99.987	3.247	624.983	0.044	99.943	0.723	624.497	0.076	32.87349	0.198384
15:30	1470	99.981	6.661	625.019	0.07	99.987	7.267	625.293	0.051	99.987	3.767	624.643	0.083	99.987	3.247	624.983	0.044	99.943	0.723	624.497	0.076	32.87119	0.196078
15:45	1485	99.981	6.661	625.019	0.07	99.993	7.273	625.287	0.057	99.987	3.767	624.643	0.083	99.987	3.247	624.983	0.044	99.943	0.723	624.497	0.076	32.87119	0.196078
16:00	1500	99.981	6.661	625.019	0.07	99.993	7.273	625.287	0.057	99.987	3.767	624.643	0.083	99.987	3.247	624.983	0.044	99.943	0.723	624.497	0.076	32.86888	0.193771
16:15	1515	99.981	6.661	625.019	0.07	99.993	7.273	625.287	0.057	99.987	3.767	624.643	0.083	99.987	3.247	624.983	0.044	99.943	0.723	624.497	0.076	32.87119	0.196078
16:30	1530	99.987	6.667	625.013	0.076	99.993	7.273	625.287	0.057	99.993	3.773	624.637	0.089	99.987	3.247	624.983	0.044	99.943	0.723	624.497	0.076	32.86888	0.193771
16:45	1545	99.993	6.673	625.007	0.082	100	7.28	625.28	0.064	99.993	3.773	624.637	0.089	99.993	3.253	624.977	0.05	99.943	0.723	624.497	0.076	32.8758	0.200691
17:00	1560	99.993	6.673	625.007	0.082	100.006	7.286	625.274	0.07	99.993	3.773	624.637	0.089	99.993	3.253	624.977	0.05	99.943	0.723	624.497	0.076	32.88272	0.207611
17:15	1575	99.993	6.673	625.007	0.082	100.006	7.286	625.274	0.07	99.993	3.773	624.637	0.089	100	3.26	624.97	0.057	99.949	0.729	624.491	0.082	32.89195	0.216838
17:30	1590	99.993	6.673	625.007	0.082	100.006	7.286	625.274	0.07	99.993	3.773	624.637	0.089	99.993	3.253	624.977	0.05	99.943	0.723	624.497	0.076	32.89426	0.219145
17:45	1605	99.993	6.673	625.007	0.082	100.012	7.292	625.268	0.076	99.993	3.773	624.637	0.089	99.993	3.253	624.977	0.05	99.943	0.723	624.497	0.076	32.89195	0.216838
18:00	1620	99.993	6.673	625.007	0.082	100.012	7.292	625.268	0.076	100	3.78	624.63	0.096	99.993	3.253	624.977	0.05	99.943	0.723	624.497	0.076	32.89656	0.221452
18:15	1635	100	6.68	625	0.089	100.012	7.292	625.268	0.076	100	3.78	624.63	0.096	100	3.26	624.97	0.057	99.949	0.729	624.491	0.082	32.90579	0.230679
18:30	1650	100	6.68	625	0.089	100.012	7.292	625.268	0.076	100	3.78	624.63	0.096	100	3.26	624.97	0.057	99.949	0.729	624.491	0.082	32.91271	0.237599
18:45	1665	100	6.68	625	0.089	100.012	7.292	625.268	0.076	100	3.78	624.63	0.096	100	3.26	624.97	0.057	99.949	0.729	624.491	0.082	32.91732	0.242213
19:00	1680	100	6.68	625	0.089	100.019	7.299	625.261	0.083	100	3.78	624.63	0.096	100	3.26	624.97	0.057	99.949	0.729	624.491	0.082	32.92655	0.25144
19:15	1695	100	6.68	625	0.089	100.019	7.299	625.261	0.083	100	3.78	624.63	0.096	100.006	3.266	624.964	0.063	99.949	0.729	624.491	0.082	32.93116	0.256053
19:30	1710	100	6.68	625	0.089	100.019	7.299	625.261	0.083	100	3.78	624.63	0.096	100	3.26	624.97	0.057	99.949	0.729	624.491	0.082	32.93578	0.260667
19:45	1725	100	6.68	625	0.089	100.012	7.292	625.268	0.076	100	3.78	624.63	0.096	100	3.26	624.97	0.057	99.949	0.729	624.491	0.082	32.93578	0.260667
20:00	1740	100	6.68	625	0.089	100.019	7.299	625.261	0.083	100	3.78	624.63	0.096	100	3.26	624.97	0.057	99.949	0.729	624.491	0.082	32.94039	0.26528
20:15	1755	100.006	6.686	624.994	0.095	100.019	7.299	625.261	0.083	100	3.78	624.63	0.096	100	3.26	624.97	0.057	99.949	0.729	624.491	0.082	32.9427	0.267587
20:30	1770	100	6.68	625	0.089	100.012	7.292	625.268	0.076	99.993	3.773	624.637	0.089	100	3.26	624.97	0.057	99.949	0.729	624.491	0.082	32.9427	0.267587
20:45	1785	100	6.68	625	0.089	100.012	7.292	625.268	0.076	100	3.78	624.63	0.096	100	3.26	624.97	0.057	99.949	0.729	624.491	0.082	32.94731	0.2722
21:00	1800	100.006	6.686	624.994	0.095	100.012	7.292	625.268	0.076	99.993	3.773	624.637	0.089	100	3.26	624.97	0.057	99.949	0.729	624.491	0.082	32.95423	0.279121
21:15	1815	100.006	6.686	624.994	0.095	100.019	7.299	625.261	0.083	100	3.78	624.63	0.096	100.006	3.266	624.964	0.063	99.949	0.729	624.491	0.082	32.95654	0.281427
21:30	1830	100.006	6.686	624.994	0.095	100.019	7																

Real Time	Elapsed Time	RW-2				MW-3				14S				14I				DC-P3				Atmospheric Pressure	
		Reference Value	Adjusted DTW	Water Level Elevation	Delta H	Reference Value	Adjusted DTW	Water Level Elevation	Delta H	Reference Value	Adjusted DTW	Water Level Elevation	Delta H	Reference Value	Adjusted DTW	Water Level Elevation	Delta H	Reference Value	Adjusted DTW	Water Level Elevation	Delta H	Ft H2O	Delta P
3:00	2160	100.018	6.698	624.982	0.107	100.031	7.311	625.249	0.095	100.006	3.786	624.624	0.102	100.012	3.272	624.958	0.069	99.962	0.742	624.478	0.095	33.04189	0.366777
3:15	2175	100.018	6.698	624.982	0.107	100.031	7.311	625.249	0.095	100.006	3.786	624.624	0.102	100.012	3.272	624.958	0.069	99.962	0.742	624.478	0.095	33.0465	0.371391
3:30	2190	100.018	6.698	624.982	0.107	100.031	7.311	625.249	0.095	100.006	3.786	624.624	0.102	100.012	3.272	624.958	0.069	99.962	0.742	624.478	0.095	33.03727	0.362164
3:45	2205	100.012	6.692	624.988	0.101	100.031	7.311	625.249	0.095	100.006	3.786	624.624	0.102	100.012	3.272	624.958	0.069	99.962	0.742	624.478	0.095	33.04189	0.366777
4:00	2220	100.018	6.698	624.982	0.107	100.031	7.311	625.249	0.095	100.006	3.786	624.624	0.102	100.012	3.272	624.958	0.069	99.962	0.742	624.478	0.095	33.04419	0.369084
4:15	2235	100.018	6.698	624.982	0.107	100.038	7.318	625.242	0.102	100.006	3.786	624.624	0.102	100.012	3.272	624.958	0.069	99.962	0.742	624.478	0.095	33.0465	0.371391
4:30	2250	100.018	6.698	624.982	0.107	100.038	7.318	625.242	0.102	100.006	3.786	624.624	0.102	100.018	3.278	624.952	0.075	99.962	0.742	624.478	0.095	33.06495	0.389845
4:45	2265	100.018	6.698	624.982	0.107	100.038	7.318	625.242	0.102	100.012	3.792	624.618	0.108	100.018	3.278	624.952	0.075	99.955	0.735	624.485	0.088	33.06726	0.392151
5:00	2280	100.025	6.705	624.975	0.114	100.038	7.318	625.242	0.102	100.012	3.792	624.618	0.108	100.018	3.278	624.952	0.075	99.955	0.735	624.485	0.088	33.0788	0.403685
5:15	2295	100.025	6.705	624.975	0.114	100.038	7.318	625.242	0.102	100.012	3.792	624.618	0.108	100.018	3.278	624.952	0.075	99.955	0.735	624.485	0.088	33.09033	0.415219
5:30	2310	100.025	6.705	624.975	0.114	100.038	7.318	625.242	0.102	100.012	3.792	624.618	0.108	100.025	3.285	624.945	0.082	99.949	0.729	624.491	0.082	33.09264	0.417526
5:45	2325	100.025	6.705	624.975	0.114	100.044	7.324	625.236	0.108	100.012	3.792	624.618	0.108	100.025	3.285	624.945	0.082	99.949	0.729	624.491	0.082	33.10648	0.431366
6:00	2340	100.031	6.711	624.969	0.12	100.044	7.324	625.236	0.108	100.019	3.799	624.618	0.115	100.025	3.285	624.945	0.082	99.949	0.729	624.491	0.082	33.12032	0.445207
6:15	2355	100.031	6.711	624.969	0.12	100.044	7.324	625.236	0.108	100.019	3.799	624.611	0.115	100.025	3.285	624.945	0.082	99.949	0.729	624.491	0.082	33.12724	0.452127
6:30	2370	100.031	6.711	624.969	0.12	100.044	7.324	625.236	0.108	100.019	3.799	624.611	0.115	100.025	3.285	624.945	0.082	99.955	0.735	624.485	0.088	33.13185	0.45674
6:45	2385	100.031	6.711	624.969	0.12	100.044	7.324	625.236	0.108	100.019	3.799	624.611	0.115	100.025	3.285	624.945	0.082	99.955	0.735	624.485	0.088	33.13416	0.459047
7:00	2400	100.031	6.711	624.969	0.12	100.044	7.324	625.236	0.108	100.019	3.799	624.611	0.115	100.031	3.291	624.939	0.088	99.955	0.735	624.485	0.088	33.14569	0.470581
7:15	2415	100.037	6.717	624.963	0.126	100.044	7.324	625.236	0.108	100.025	3.805	624.605	0.121	100.031	3.291	624.939	0.088	99.955	0.735	624.485	0.088	33.15492	0.479808
7:30	2430	100.031	6.711	624.969	0.12	100.044	7.324	625.236	0.108	100.019	3.799	624.611	0.115	100.031	3.291	624.939	0.088	99.955	0.735	624.485	0.088	33.15722	0.482115
7:45	2445	100.037	6.717	624.963	0.126	100.051	7.331	625.229	0.115	100.025	3.805	624.605	0.121	100.031	3.291	624.939	0.088	99.955	0.735	624.485	0.088	33.16645	0.491342
8:00	2460	100.037	6.717	624.963	0.126	100.051	7.331	625.229	0.115	100.025	3.805	624.605	0.121	100.031	3.291	624.939	0.088	99.955	0.735	624.485	0.088	33.17337	0.498262
8:15	2475	100.037	6.717	624.963	0.126	100.051	7.331	625.229	0.115	100.025	3.805	624.605	0.121	100.031	3.291	624.939	0.088	99.955	0.735	624.485	0.088	33.17337	0.498262
8:30	2490	100.037	6.717	624.963	0.126	100.051	7.331	625.229	0.115	100.031	3.811	624.599	0.127	100.031	3.291	624.939	0.088	99.955	0.735	624.485	0.088	33.17568	0.500569
8:45	2505	100.037	6.717	624.963	0.126	100.057	7.337	625.223	0.121	100.031	3.811	624.599	0.127	100.031	3.291	624.939	0.088	99.955	0.735	624.485	0.088	33.18491	0.509796
9:00	2520	100.044	6.724	624.956	0.133	100.057	7.337	625.223	0.121	100.031	3.811	624.599	0.127	100.037	3.297	624.933	0.094	99.962	0.742	624.478	0.095	33.18952	0.514409
9:15	2535	100.044	6.724	624.956	0.133	100.057	7.337	625.223	0.121	100.031	3												

Real Time	Elapsed Time	RW-2				MW-3				14S				14I				DC-P3				Atmospheric Pressure	
		Reference Value	Adjusted DTW	Water Level Elevation	Delta H	Reference Value	Adjusted DTW	Water Level Elevation	Delta H	Reference Value	Adjusted DTW	Water Level Elevation	Delta H	Reference Value	Adjusted DTW	Water Level Elevation	Delta H	Reference Value	Adjusted DTW	Water Level Elevation	Delta H	Ft H2O	Delta P
(ft H2O)	(ft H2O)	(msl)	(ft H2O)	(ft H2O)	(ft H2O)	(ft H2O)	(ft H2O)	(msl)	(ft H2O)	(ft H2O)	(msl)	(ft H2O)	(ft H2O)	(ft H2O)	(ft H2O)	(ft H2O)	(ft H2O)	(ft H2O)	(ft H2O)	(ft H2O)	(ft H2O)	(ft H2O)	(ft H2O)
15:00	2880	100.075	6.755	624.925	0.164	100.089	7.369	625.191	0.153	100.069	3.849	624.561	0.165	100.063	3.323	624.907	0.12	99.898	0.678	624.542	0.031	33.2172	0.54209
15:15	2895	100.075	6.755	624.925	0.164	100.089	7.369	625.191	0.153	100.069	3.849	624.561	0.165	100.063	3.323	624.907	0.12	99.911	0.691	624.529	0.044	33.21951	0.544397
15:30	2910	100.075	6.755	624.925	0.164	100.089	7.369	625.191	0.153	100.069	3.849	624.561	0.165	100.069	3.329	624.901	0.126	99.905	0.685	624.535	0.038	33.2172	0.54209
15:45	2925	100.075	6.755	624.925	0.164	100.095	7.375	625.185	0.159	100.069	3.849	624.561	0.165	100.069	3.329	624.901	0.126	99.898	0.678	624.542	0.031	33.22412	0.54901
16:00	2940	100.075	6.755	624.925	0.164	100.089	7.369	625.191	0.153	100.069	3.849	624.561	0.165	100.069	3.329	624.901	0.126	99.892	0.672	624.548	0.025	33.2172	0.54209
16:15	2955	100.075	6.755	624.925	0.164	100.095	7.375	625.185	0.159	100.069	3.849	624.561	0.165	100.069	3.329	624.901	0.126	99.892	0.672	624.548	0.025	33.21951	0.544397
16:30	2970	100.075	6.755	624.925	0.164	100.095	7.375	625.185	0.159	100.069	3.849	624.561	0.165	100.069	3.329	624.901	0.126	99.892	0.672	624.548	0.025	33.2172	0.54209
16:45	2985	100.075	6.755	624.925	0.164	100.095	7.375	625.185	0.159	100.069	3.849	624.561	0.165	100.063	3.323	624.907	0.12	99.892	0.672	624.548	0.025	33.21028	0.53517
17:00	3000	100.075	6.755	624.925	0.164	100.095	7.375	625.185	0.159	100.069	3.849	624.561	0.165	100.063	3.323	624.907	0.12	99.892	0.672	624.548	0.025	33.20797	0.532863
17:15	3015	100.075	6.755	624.925	0.164	100.095	7.375	625.185	0.159	100.069	3.849	624.561	0.165	100.063	3.323	624.907	0.12	99.898	0.678	624.542	0.031	33.21028	0.53517
17:30	3030	100.075	6.755	624.925	0.164	100.095	7.375	625.185	0.159	100.069	3.849	624.561	0.165	100.069	3.329	624.901	0.126	99.905	0.685	624.535	0.038	33.20105	0.525943
17:45	3045	100.075	6.755	624.925	0.164	100.095	7.375	625.185	0.159	100.069	3.849	624.561	0.165	100.069	3.329	624.901	0.126	99.911	0.691	624.529	0.044	33.20567	0.530556
18:00	3060	100.075	6.755	624.925	0.164	100.095	7.375	625.185	0.159	100.069	3.849	624.561	0.165	100.069	3.329	624.901	0.126	99.917	0.697	624.523	0.05	33.20567	0.530556
18:15	3075	100.075	6.755	624.925	0.164	100.095	7.375	625.185	0.159	100.069	3.849	624.561	0.165	100.069	3.329	624.901	0.126	99.924	0.704	624.516	0.057	33.20797	0.532863
18:30	3090	100.082	6.762	624.918	0.171	100.095	7.375	625.185	0.159	100.069	3.849	624.561	0.165	100.069	3.329	624.901	0.126	99.924	0.704	624.516	0.057	33.20797	0.532863
18:45	3105	100.082	6.762	624.918	0.171	100.095	7.375	625.185	0.159	100.069	3.849	624.561	0.165	100.069	3.329	624.901	0.126	99.924	0.704	624.516	0.057	33.20797	0.532863
19:00	3120	100.082	6.762	624.918	0.171	100.095	7.375	625.185	0.159	100.069	3.849	624.561	0.165	100.069	3.329	624.901	0.126	99.93	0.71	624.51	0.063	33.21259	0.537477
19:15	3135	100.082	6.762	624.918	0.171	100.102	7.382	625.178	0.166	100.069	3.849	624.561	0.165	100.075	3.335	624.895	0.132	99.936	0.716	624.504	0.069	33.21489	0.539783
19:30	3150	100.082	6.762	624.918	0.171	100.095	7.375	625.185	0.159	100.069	3.849	624.561	0.165	100.069	3.329	624.901	0.126	99.936	0.716	624.504	0.069	33.21951	0.544397
19:45	3165	100.082	6.762	624.918	0.171	100.102	7.382	625.178	0.166	100.069	3.849	624.561	0.165	100.069	3.329	624.901	0.126	99.943	0.723	624.497	0.076	33.22873	0.553624
20:00	3180	100.082	6.762	624.918	0.171	100.102	7.382	625.178	0.166	100.069	3.849	624.561	0.165	100.075	3.335	624.895	0.132	99.949	0.729	624.491	0.082	33.23335	0.558237
20:15	3195	100.082	6.762	624.918	0.171	100.102	7.382	625.178	0.166	100.069	3.849	624.561	0.165	100.075	3.335	624.895	0.132	99.949	0.729	624.491	0.082	33.23796	0.562851
20:30	3210	100.082	6.762	624.918	0.171	100.095	7.375	625.185	0.159	100.063	3.843	624.567	0.159	100.075	3.335	624.895	0.132	99.949	0.729	624.491	0.082	33.23796	0.562851
20:45	3225	100.082	6.762	624.918	0.171	100.102	7.382	625.178	0.166	100.063	3.843	624.567	0.159	100.075	3.335	624.895	0.132	99.949	0.729	624.			

Real Time	Elapsed Time	RW-2				MW-3				14S				14I				DC-P3				Atmospheric Pressure	
		Reference Value	Adjusted DTW	Water Level Elevation	Delta H	Reference Value	Adjusted DTW	Water Level Elevation	Delta H	Reference Value	Adjusted DTW	Water Level Elevation	Delta H	Reference Value	Adjusted DTW	Water Level Elevation	Delta H	Reference Value	Adjusted DTW	Water Level Elevation	Delta H	Ft H2O	Delta P
3:00	3600	100.069	6.749	624.931	0.158	100.083	7.363	625.197	0.147	100.044	3.824	624.586	0.14	100.063	3.323	624.907	0.12	99.962	0.742	624.478	0.095	33.26334	0.588225
3:15	3615	100.069	6.749	624.931	0.158	100.089	7.369	625.191	0.153	100.044	3.824	624.586	0.14	100.069	3.329	624.901	0.126	99.962	0.742	624.478	0.095	33.26334	0.588225
3:30	3630	100.075	6.755	624.925	0.164	100.089	7.369	625.191	0.153	100.044	3.824	624.586	0.14	100.063	3.323	624.907	0.12	99.962	0.742	624.478	0.095	33.26564	0.590532
3:45	3645	100.075	6.755	624.925	0.164	100.089	7.369	625.191	0.153	100.05	3.83	624.58	0.146	100.063	3.323	624.907	0.12	99.962	0.742	624.478	0.095	33.26564	0.590532
4:00	3660	100.069	6.749	624.931	0.158	100.083	7.363	625.197	0.147	100.044	3.824	624.586	0.14	100.063	3.323	624.907	0.12	99.968	0.748	624.472	0.101	33.26795	0.592839
4:15	3675	100.069	6.749	624.931	0.158	100.089	7.369	625.191	0.153	100.05	3.83	624.58	0.146	100.063	3.323	624.907	0.12	99.968	0.748	624.472	0.101	33.26564	0.590532
4:30	3690	100.069	6.749	624.931	0.158	100.083	7.363	625.197	0.147	100.044	3.824	624.586	0.14	100.063	3.323	624.907	0.12	99.968	0.748	624.472	0.101	33.25872	0.583612
4:45	3705	100.069	6.749	624.931	0.158	100.083	7.363	625.197	0.147	100.05	3.83	624.58	0.146	100.063	3.323	624.907	0.12	99.968	0.748	624.472	0.101	33.25872	0.583612
5:00	3720	100.069	6.749	624.931	0.158	100.083	7.363	625.197	0.147	100.05	3.83	624.58	0.146	100.063	3.323	624.907	0.12	99.968	0.748	624.472	0.101	33.26103	0.585918
5:15	3735	100.069	6.749	624.931	0.158	100.083	7.363	625.197	0.147	100.044	3.824	624.586	0.14	100.063	3.323	624.907	0.12	99.968	0.748	624.472	0.101	33.25872	0.583612
5:30	3750	100.069	6.749	624.931	0.158	100.083	7.363	625.197	0.147	100.044	3.824	624.586	0.14	100.063	3.323	624.907	0.12	99.968	0.748	624.472	0.101	33.25872	0.583612
5:45	3765	100.069	6.749	624.931	0.158	100.083	7.363	625.197	0.147	100.044	3.824	624.586	0.14	100.063	3.323	624.907	0.12	99.974	0.754	624.466	0.107	33.26103	0.585918
6:00	3780	100.075	6.755	624.925	0.164	100.083	7.363	625.197	0.147	100.05	3.83	624.58	0.146	100.069	3.329	624.901	0.126	99.968	0.748	624.472	0.101	33.26564	0.590532
6:15	3795	100.075	6.755	624.925	0.164	100.083	7.363	625.197	0.147	100.05	3.83	624.58	0.146	100.063	3.323	624.907	0.12	99.974	0.754	624.466	0.107	33.26564	0.590532
6:30	3810	100.069	6.749	624.931	0.158	100.083	7.363	625.197	0.147	100.044	3.824	624.586	0.14	100.063	3.323	624.907	0.12	99.974	0.754	624.466	0.107	33.25872	0.583612
6:45	3825	100.069	6.749	624.931	0.158	100.089	7.369	625.191	0.153	100.05	3.83	624.58	0.146	100.069	3.329	624.901	0.126	99.974	0.754	624.466	0.107	33.26795	0.592839
7:00	3840	100.069	6.749	624.931	0.158	100.083	7.363	625.197	0.147	100.044	3.824	624.586	0.14	100.063	3.323	624.907	0.12	99.968	0.748	624.472	0.101	33.25872	0.583612
7:15	3855	100.069	6.749	624.931	0.158	100.083	7.363	625.197	0.147	100.044	3.824	624.586	0.14	100.063	3.323	624.907	0.12	99.974	0.754	624.466	0.107	33.26103	0.585918
7:30	3870	100.069	6.749	624.931	0.158	100.083	7.363	625.197	0.147	100.05	3.83	624.58	0.146	100.063	3.323	624.907	0.12	99.974	0.754	624.466	0.107	33.26103	0.585918
7:45	3885	100.075	6.755	624.925	0.164	100.083	7.363	625.197	0.147	100.05	3.83	624.58	0.146	100.063	3.323	624.907	0.12	99.974	0.754	624.466	0.107	33.25872	0.583612
8:00	3900	100.075	6.755	624.925	0.164	100.083	7.363	625.197	0.147	100.05	3.83	624.58	0.146	100.069	3.329	624.901	0.126	99.974	0.754	624.466	0.107	33.26334	0.588225
8:15	3915	100.075	6.755	624.925	0.164	100.089	7.369	625.191	0.153	100.057	3.837	624.573	0.153	100.069	3.329	624.901	0.126	99.974	0.754	624.466	0.107	33.27026	0.595145
8:30	3930	100.082	6.762	624.918	0.171	100.089	7.369	625.191	0.153	100.057	3.837	624.573	0.153	100.069	3.329	624.901	0.126	99.974	0.754	624.466	0.107	33.26564	0.590532
8:45	3945	100.082	6.762	624.918	0.171	100.089	7.369	625.191	0.153	100.057	3.837	624.573	0.153	100.069	3.329	624.901	0.126	99.974	0.754	624.466	0.107	33.26795	0.592839
9:00	3960	100.082	6.762	624.918	0.171	100.095	7.375	625.185	0.159	100.057	3.837	624.573	0.153	100.075	3.335	624.895	0.132	99.974	0.754	624.466	0.107	33.27718	0.602066
9:15	3975	100.082	6.762	624.918	0.171	100.095	7.375	625.185	0.159	100.057	3.837	624.573	0.153	100.069	3.329								

Real Time	Elapsed Time	RW-2				MW-3				14S				14I				DC-P3				Atmospheric Pressure	
		Reference Value	Adjusted DTW	Water Level Elevation (ft H2O)	Delta H (msl)	Reference Value	Adjusted DTW	Water Level Elevation (ft H2O)	Delta H (ft H2O)	Reference Value	Adjusted DTW	Water Level Elevation (ft H2O)	Delta H (ft H2O)	Reference Value	Adjusted DTW	Water Level Elevation (ft H2O)	Delta H (ft H2O)	Reference Value	Adjusted DTW	Water Level Elevation (ft H2O)	Delta H (ft H2O)	Ft H2O	Delta P
15:00	4320	100.107	6.787	624.893	0.196	100.121	7.401	625.159	0.185	100.101	3.881	624.529	0.197	100.101	3.361	624.869	0.158	99.968	0.748	624.472	0.101	33.17568	0.500569
15:15	4335	100.107	6.787	624.893	0.196	100.121	7.401	625.159	0.185	100.101	3.881	624.529	0.197	100.101	3.361	624.869	0.158	99.968	0.748	624.472	0.101	33.17337	0.498262
15:30	4350	100.107	6.787	624.893	0.196	100.121	7.401	625.159	0.185	100.101	3.881	624.529	0.197	100.101	3.361	624.869	0.158	99.968	0.748	624.472	0.101	33.16876	0.493648
15:45	4365	100.113	6.793	624.887	0.202	100.127	7.407	625.153	0.191	100.101	3.881	624.529	0.197	100.101	3.361	624.869	0.158	99.968	0.748	624.472	0.101	33.16645	0.491342
16:00	4380	100.113	6.793	624.887	0.202	100.127	7.407	625.153	0.191	100.107	3.887	624.523	0.203	100.107	3.367	624.863	0.164	99.968	0.748	624.472	0.101	33.17107	0.495955
16:15	4395	100.113	6.793	624.887	0.202	100.127	7.407	625.153	0.191	100.101	3.881	624.529	0.197	100.101	3.361	624.869	0.158	99.968	0.748	624.472	0.101	33.16184	0.486728
16:30	4410	100.113	6.793	624.887	0.202	100.127	7.407	625.153	0.191	100.107	3.887	624.523	0.203	100.107	3.367	624.863	0.164	99.968	0.748	624.472	0.101	33.16184	0.486728
16:45	4425	100.113	6.793	624.887	0.202	100.127	7.407	625.153	0.191	100.107	3.887	624.523	0.203	100.107	3.367	624.863	0.164	99.968	0.748	624.472	0.101	33.15722	0.482115
17:00	4440	100.119	6.799	624.881	0.208	100.127	7.407	625.153	0.191	100.107	3.887	624.523	0.203	100.107	3.367	624.863	0.164	99.968	0.748	624.472	0.101	33.16414	0.489035
17:15	4455	100.119	6.799	624.881	0.208	100.134	7.414	625.146	0.198	100.107	3.887	624.523	0.203	100.107	3.367	624.863	0.164	99.968	0.748	624.472	0.101	33.15492	0.479808
17:30	4470	100.119	6.799	624.881	0.208	100.134	7.414	625.146	0.198	100.107	3.887	624.523	0.203	100.107	3.367	624.863	0.164	99.968	0.748	624.472	0.101	33.15953	0.484421
17:45	4485	100.119	6.799	624.881	0.208	100.134	7.414	625.146	0.198	100.107	3.887	624.523	0.203	100.107	3.367	624.863	0.164	99.968	0.748	624.472	0.101	33.15953	0.484421
18:00	4500	100.119	6.799	624.881	0.208	100.134	7.414	625.146	0.198	100.107	3.887	624.523	0.203	100.113	3.373	624.857	0.17	99.968	0.748	624.472	0.101	33.16414	0.489035
18:15	4515	100.119	6.799	624.881	0.208	100.134	7.414	625.146	0.198	100.107	3.887	624.523	0.203	100.113	3.373	624.857	0.17	99.968	0.748	624.472	0.101	33.16414	0.489035
18:30	4530	100.126	6.806	624.874	0.215	100.14	7.42	625.14	0.204	100.107	3.887	624.523	0.203	100.113	3.373	624.857	0.17	99.968	0.748	624.472	0.101	33.16184	0.486728
18:45	4545	100.126	6.806	624.874	0.215	100.14	7.42	625.14	0.204	100.107	3.887	624.523	0.203	100.113	3.373	624.857	0.17	99.968	0.748	624.472	0.101	33.16645	0.491342
19:00	4560	100.126	6.806	624.874	0.215	100.14	7.42	625.14	0.204	100.107	3.887	624.523	0.203	100.113	3.373	624.857	0.17	99.968	0.748	624.472	0.101	33.17107	0.495955
19:15	4575	100.126	6.806	624.874	0.215	100.14	7.42	625.14	0.204	100.107	3.887	624.523	0.203	100.113	3.373	624.857	0.17	99.968	0.748	624.472	0.101	33.17107	0.495955
19:30	4590	100.126	6.806	624.874	0.215	100.147	7.427	625.133	0.211	100.107	3.887	624.523	0.203	100.113	3.373	624.857	0.17	99.968	0.748	624.472	0.101	33.16876	0.493648
19:45	4605	100.126	6.806	624.874	0.215	100.14	7.42	625.14	0.204	100.101	3.881	624.529	0.197	100.113	3.373	624.857	0.17	99.968	0.748	624.472	0.101	33.18029	0.505182
20:00	4620	100.126	6.806	624.874	0.215	100.14	7.42	625.14	0.204	100.101	3.881	624.529	0.197	100.113	3.373	624.857	0.17	99.968	0.748	624.472	0.101	33.18029	0.505182
20:15	4635	100.126	6.806	624.874	0.215	100.14	7.42	625.14	0.204	100.101	3.881	624.529	0.197	100.113	3.373	624.857	0.17	99.968	0.748	624.472	0.101	33.1826	0.507489
20:30	4650	100.119	6.799	624.881	0.208	100.14	7.42	625.14	0.204	100.095	3.875	624.535	0.191	100.113	3.373	624.857	0.17	99.968	0.748	624.472	0.101	33.17568	0.500569
20:45	4665	100.119	6.799	624.881	0.208	100.14	7.42	625.14	0.204	100.095	3.875	624.535	0.191	100.107	3.367	624.863	0.164	99.968	0.748	624.472	0.101	33.17568	0.500569
21:00	4680	100.119	6.799	624.881	0.208	100.14	7.42	625.14	0.204	100.095	3.875	624.535	0.191	100.113	3.373	624.857	0.17	99.968	0.748	624.472	0.101	33.18029	0.505182
21:15	4695	100.119																					

Real Time	Elapsed Time	RW-2				MW-3				14S				14I				DC-P3				Atmospheric Pressure	
		Reference Value	Adjusted DTW	Water Level Elevation	Delta H	Reference Value	Adjusted DTW	Water Level Elevation	Delta H	Reference Value	Adjusted DTW	Water Level Elevation	Delta H	Reference Value	Adjusted DTW	Water Level Elevation	Delta H	Reference Value	Adjusted DTW	Water Level Elevation	Delta H	Ft H2O	Delta P
(ft H2O)	(ft H2O)	(msl)	(ft H2O)	(ft H2O)	(ft H2O)	(ft H2O)	(ft H2O)	(msl)	(ft H2O)	(ft H2O)	(ft H2O)	(ft H2O)	(ft H2O)	(ft H2O)	(ft H2O)	(ft H2O)	(ft H2O)	(ft H2O)	(ft H2O)	(ft H2O)	(ft H2O)	(ft H2O)	(ft H2O)
3:00	5040	100.107	6.787	624.893	0.196	100.127	7.407	625.153	0.191	100.082	3.862	624.548	0.178	100.101	3.361	624.869	0.158	99.962	0.742	624.478	0.095	33.15722	0.482115
3:15	5055	100.107	6.787	624.893	0.196	100.121	7.401	625.159	0.185	100.082	3.862	624.548	0.178	100.101	3.361	624.869	0.158	99.955	0.735	624.485	0.088	33.15722	0.482115
3:30	5070	100.107	6.787	624.893	0.196	100.121	7.401	625.159	0.185	100.082	3.862	624.548	0.178	100.101	3.361	624.869	0.158	99.955	0.735	624.485	0.088	33.148	0.472887
3:45	5085	100.107	6.787	624.893	0.196	100.121	7.401	625.159	0.185	100.082	3.862	624.548	0.178	100.101	3.361	624.869	0.158	99.955	0.735	624.485	0.088	33.15492	0.479808
4:00	5100	100.107	6.787	624.893	0.196	100.121	7.401	625.159	0.185	100.082	3.862	624.548	0.178	100.101	3.361	624.869	0.158	99.955	0.735	624.485	0.088	33.148	0.472887
4:15	5115	100.113	6.793	624.887	0.202	100.121	7.401	625.159	0.185	100.082	3.862	624.548	0.178	100.107	3.367	624.863	0.164	99.962	0.742	624.478	0.095	33.1503	0.475194
4:30	5130	100.107	6.787	624.893	0.196	100.121	7.401	625.159	0.185	100.082	3.862	624.548	0.178	100.101	3.361	624.869	0.158	99.962	0.742	624.478	0.095	33.1503	0.475194
4:45	5145	100.107	6.787	624.893	0.196	100.121	7.401	625.159	0.185	100.082	3.862	624.548	0.178	100.107	3.367	624.863	0.164	99.962	0.742	624.478	0.095	33.15492	0.479808
5:00	5160	100.113	6.793	624.887	0.202	100.121	7.401	625.159	0.185	100.082	3.862	624.548	0.178	100.107	3.367	624.863	0.164	99.962	0.742	624.478	0.095	33.15492	0.479808
5:15	5175	100.107	6.787	624.893	0.196	100.121	7.401	625.159	0.185	100.082	3.862	624.548	0.178	100.101	3.361	624.869	0.158	99.962	0.742	624.478	0.095	33.148	0.472887
5:30	5190	100.107	6.787	624.893	0.196	100.121	7.401	625.159	0.185	100.082	3.862	624.548	0.178	100.107	3.367	624.863	0.164	99.962	0.742	624.478	0.095	33.148	0.472887
5:45	5205	100.113	6.793	624.887	0.202	100.127	7.407	625.153	0.191	100.082	3.862	624.548	0.178	100.107	3.367	624.863	0.164	99.962	0.742	624.478	0.095	33.15492	0.479808
6:00	5220	100.107	6.787	624.893	0.196	100.121	7.401	625.159	0.185	100.082	3.862	624.548	0.178	100.101	3.361	624.869	0.158	99.962	0.742	624.478	0.095	33.14569	0.470581
6:15	5235	100.107	6.787	624.893	0.196	100.121	7.401	625.159	0.185	100.082	3.862	624.548	0.178	100.107	3.367	624.863	0.164	99.962	0.742	624.478	0.095	33.148	0.472887
6:30	5250	100.113	6.793	624.887	0.202	100.121	7.401	625.159	0.185	100.082	3.862	624.548	0.178	100.107	3.367	624.863	0.164	99.968	0.748	624.472	0.101	33.15492	0.479808
6:45	5265	100.113	6.793	624.887	0.202	100.121	7.401	625.159	0.185	100.088	3.868	624.542	0.184	100.107	3.367	624.863	0.164	99.968	0.748	624.472	0.101	33.16184	0.486728
7:00	5280	100.113	6.793	624.887	0.202	100.127	7.407	625.153	0.191	100.088	3.868	624.542	0.184	100.107	3.367	624.863	0.164	99.968	0.748	624.472	0.101	33.16414	0.489035
7:15	5295	100.113	6.793	624.887	0.202	100.127	7.407	625.153	0.191	100.088	3.868	624.542	0.184	100.107	3.367	624.863	0.164	99.968	0.748	624.472	0.101	33.16645	0.491342
7:30	5310	100.113	6.793	624.887	0.202	100.127	7.407	625.153	0.191	100.088	3.868	624.542	0.184	100.113	3.373	624.857	0.17	99.974	0.754	624.466	0.107	33.17107	0.495955
7:45	5325	100.113	6.793	624.887	0.202	100.127	7.407	625.153	0.191	100.088	3.868	624.542	0.184	100.107	3.367	624.863	0.164	99.968	0.748	624.472	0.101	33.16876	0.493648
8:00	5340	100.113	6.793	624.887	0.202	100.127	7.407	625.153	0.191	100.088	3.868	624.542	0.184	100.107	3.367	624.863	0.164	99.974	0.754	624.466	0.107	33.16876	0.493648
8:15	5355	100.113	6.793	624.887	0.202	100.127	7.407	625.153	0.191	100.088	3.868	624.542	0.184	100.107	3.367	624.863	0.164	99.968	0.748	624.472	0.101	33.16876	0.493648
8:30	5370	100.119	6.799	624.881	0.208	100.127	7.407	625.153	0.191	100.088	3.868	624.542	0.184	100.113	3.373	624.857	0.17	99.968	0.748	624.472	0.101	33.16876	0.493648
8:45	5385	100.119	6.799	624.881	0.208	100.134	7.414	625.146	0.198	100.095	3.875	624.535	0.191	100.113	3.373	624.857	0.17	99.974	0.754	624.466	0.107	33.171	

Real Time	Elapsed Time	RW-2				MW-3				14S				14I				DC-P3				Atmospheric Pressure	
		Reference Value (ft H2O)	Adjusted DTW (ft H2O)	Water Level Elevation (msl)	Delta H (ft H2O)	Reference Value (ft H2O)	Adjusted DTW (ft H2O)	Water Level Elevation (msl)	Delta H (ft H2O)	Reference Value (ft H2O)	Adjusted DTW (ft H2O)	Water Level Elevation (msl)	Delta H (ft H2O)	Reference Value (ft H2O)	Adjusted DTW (ft H2O)	Water Level Elevation (msl)	Delta H (ft H2O)	Reference Value (ft H2O)	Adjusted DTW (ft H2O)	Water Level Elevation (msl)	Delta H (ft H2O)	Ft H2O	Delta P
15:00	5760	100.145	6.825	624.855	0.234	100.159	7.439	625.121	0.223	100.133	3.913	624.497	0.229	100.138	3.398	624.832	0.195	99.981	0.761	624.459	0.114	33.07418	0.399072
15:15	5775	100.145	6.825	624.855	0.234	100.159	7.439	625.121	0.223	100.133	3.913	624.497	0.229	100.138	3.398	624.832	0.195	99.981	0.761	624.459	0.114	33.06957	0.394458
15:30	5790	100.145	6.825	624.855	0.234	100.159	7.439	625.121	0.223	100.133	3.913	624.497	0.229	100.132	3.392	624.838	0.189	99.981	0.761	624.459	0.114	33.07187	0.396765
15:45	5805	100.145	6.825	624.855	0.234	100.159	7.439	625.121	0.223	100.133	3.913	624.497	0.229	100.138	3.398	624.832	0.195	99.981	0.761	624.459	0.114	33.06034	0.385231
16:00	5820	100.151	6.831	624.849	0.24	100.166	7.446	625.114	0.23	100.145	3.925	624.485	0.241	100.151	3.411	624.819	0.208	99.987	0.767	624.453	0.12	33.06495	0.389845
16:15	5835	100.151	6.831	624.849	0.24	100.166	7.446	625.114	0.23	100.139	3.919	624.491	0.235	100.145	3.405	624.825	0.202	99.987	0.767	624.453	0.12	33.05803	0.382924
16:30	5850	100.151	6.831	624.849	0.24	100.159	7.439	625.121	0.223	100.139	3.919	624.491	0.235	100.145	3.405	624.825	0.202	99.987	0.767	624.453	0.12	33.04881	0.373697
16:45	5865	100.151	6.831	624.849	0.24	100.166	7.446	625.114	0.23	100.139	3.919	624.491	0.235	100.138	3.398	624.832	0.195	99.987	0.767	624.453	0.12	33.04419	0.369084
17:00	5880	100.151	6.831	624.849	0.24	100.166	7.446	625.114	0.23	100.133	3.913	624.497	0.229	100.138	3.398	624.832	0.195	99.987	0.767	624.453	0.12	33.03727	0.362164
17:15	5895	100.151	6.831	624.849	0.24	100.166	7.446	625.114	0.23	100.139	3.919	624.491	0.235	100.145	3.405	624.825	0.202	99.987	0.767	624.453	0.12	33.03727	0.362164
17:30	5910	100.151	6.831	624.849	0.24	100.159	7.439	625.121	0.223	100.133	3.913	624.497	0.229	100.145	3.405	624.825	0.202	99.987	0.767	624.453	0.12	33.03266	0.35755
17:45	5925	100.151	6.831	624.849	0.24	100.166	7.446	625.114	0.23	100.133	3.913	624.497	0.229	100.145	3.405	624.825	0.202	99.987	0.767	624.453	0.12	33.03497	0.359857
18:00	5940	100.151	6.831	624.849	0.24	100.166	7.446	625.114	0.23	100.139	3.919	624.491	0.235	100.145	3.405	624.825	0.202	99.993	0.773	624.447	0.126	33.02343	0.348323
18:15	5955	100.151	6.831	624.849	0.24	100.166	7.446	625.114	0.23	100.133	3.913	624.497	0.229	100.145	3.405	624.825	0.202	99.993	0.773	624.447	0.126	33.02113	0.346016
18:30	5970	100.151	6.831	624.849	0.24	100.166	7.446	625.114	0.23	100.133	3.913	624.497	0.229	100.145	3.405	624.825	0.202	99.993	0.773	624.447	0.126	33.02343	0.348323
18:45	5985	100.151	6.831	624.849	0.24	100.166	7.446	625.114	0.23	100.133	3.913	624.497	0.229	100.145	3.405	624.825	0.202	99.993	0.773	624.447	0.126	33.02343	0.348323
19:00	6000	100.157	6.837	624.843	0.246	100.166	7.446	625.114	0.23	100.133	3.913	624.497	0.229	100.145	3.405	624.825	0.202	99.993	0.773	624.447	0.126	33.02343	0.348323
19:15	6015	100.157	6.837	624.843	0.246	100.172	7.452	625.108	0.236	100.133	3.913	624.497	0.229	100.145	3.405	624.825	0.202	99.993	0.773	624.447	0.126	33.02574	0.35063
19:30	6030	100.157	6.837	624.843	0.246	100.172	7.452	625.108	0.236	100.133	3.913	624.497	0.229	100.145	3.405	624.825	0.202	99.993	0.773	624.447	0.126	33.02574	0.35063
19:45	6045	100.151	6.831	624.849	0.24	100.166	7.446	625.114	0.23	100.126	3.906	624.504	0.222	100.145	3.405	624.825	0.202	99.993	0.773	624.447	0.126	33.02574	0.35063
20:00	6060	100.151	6.831	624.849	0.24	100.172	7.452	625.108	0.236	100.126	3.906	624.504	0.222	100.145	3.405	624.825	0.202	99.993	0.773	624.447	0.126	33.02805	0.352937
20:15	6075	100.151	6.831	624.849	0.24	100.172	7.452	625.108	0.236	100.126	3.906	624.504	0.222	100.145	3.405	624.825	0.202	99.993	0.773	624.447	0.126	33.03266	0.35755
20:30	6090	100.151	6.831	624.849	0.24	100.172	7.452	625.108	0.236	100.12	3.9	624.51	0.216	100.145	3.405	624.825	0.202	99.993	0.773	624.447	0.126	33.02805	0.352937
20:45	6105	100.151	6.831	624.849	0.24	100.166	7.446	625.114	0.23	100.12	3.9	624.51	0.216	100.145	3.405	624.825	0.202	99.993	0.773	624.447	0.126	33.02343	0.348323
21:00	6120	100.151	6.831	624.849	0.24	100.166	7.446	625.114	0.23	100.12	3.9	624.51	0.216										

Real Time	Elapsed Time	RW-2					MW-3					14S					14I					DC-P3					Atmospheric Pressure	
		Reference Value	Adjusted DTW	Water Level (ft H2O)	Elevation (msl)	Delta H (ft H2O)	Reference Value	Adjusted DTW	Water Level (ft H2O)	Elevation (msl)	Delta H (ft H2O)	Reference Value	Adjusted DTW	Water Level (ft H2O)	Elevation (msl)	Delta H (ft H2O)	Reference Value	Adjusted DTW	Water Level (ft H2O)	Elevation (msl)	Delta H (ft H2O)	Reference Value	Adjusted DTW	Water Level (ft H2O)	Elevation (msl)	Delta H (ft H2O)	Ft H2O	Delta P
3:00	6480	100.132	6.812	624.868	0.221	100.147	7.427	625.133	0.211	100.107	3.887	624.523	0.203	100.132	3.392	624.838	0.189	99.993	0.773	624.447	0.126	32.95192	0.276814					
3:15	6495	100.138	6.818	624.862	0.227	100.147	7.427	625.133	0.211	100.107	3.887	624.523	0.203	100.132	3.392	624.838	0.189	99.993	0.773	624.447	0.126	32.945	0.269894					
3:30	6510	100.132	6.812	624.868	0.221	100.147	7.427	625.133	0.211	100.107	3.887	624.523	0.203	100.132	3.392	624.838	0.189	99.993	0.773	624.447	0.126	32.93808	0.262973					
3:45	6525	100.132	6.812	624.868	0.221	100.14	7.42	625.14	0.204	100.107	3.887	624.523	0.203	100.132	3.392	624.838	0.189	99.993	0.773	624.447	0.126	32.93116	0.256053					
4:00	6540	100.138	6.818	624.862	0.227	100.147	7.427	625.133	0.211	100.107	3.887	624.523	0.203	100.132	3.392	624.838	0.189	99.993	0.773	624.447	0.126	32.93116	0.256053					
4:15	6555	100.138	6.818	624.862	0.227	100.147	7.427	625.133	0.211	100.107	3.887	624.523	0.203	100.132	3.392	624.838	0.189	99.993	0.773	624.447	0.126	32.92886	0.253746					
4:30	6570	100.132	6.812	624.868	0.221	100.147	7.427	625.133	0.211	100.107	3.887	624.523	0.203	100.132	3.392	624.838	0.189	99.993	0.773	624.447	0.126	32.92655	0.25144					
4:45	6585	100.138	6.818	624.862	0.227	100.14	7.42	625.14	0.204	100.107	3.887	624.523	0.203	100.132	3.392	624.838	0.189	99.993	0.773	624.447	0.126	32.92194	0.246826					
5:00	6600	100.138	6.818	624.862	0.227	100.14	7.42	625.14	0.204	100.107	3.887	624.523	0.203	100.132	3.392	624.838	0.189	99.993	0.773	624.447	0.126	32.92655	0.25144					
5:15	6615	100.145	6.825	624.855	0.234	100.147	7.427	625.133	0.211	100.114	3.894	624.516	0.21	100.138	3.398	624.832	0.195	99.993	0.773	624.447	0.126	32.93116	0.256053					
5:30	6630	100.138	6.818	624.862	0.227	100.147	7.427	625.133	0.211	100.107	3.887	624.523	0.203	100.138	3.398	624.832	0.195	99.993	0.773	624.447	0.126	32.92886	0.253746					
5:45	6645	100.138	6.818	624.862	0.227	100.147	7.427	625.133	0.211	100.107	3.887	624.523	0.203	100.138	3.398	624.832	0.195	99.993	0.773	624.447	0.126	32.92886	0.253746					
6:00	6660	100.145	6.825	624.855	0.234	100.147	7.427	625.133	0.211	100.114	3.894	624.516	0.21	100.138	3.398	624.832	0.195	99.993	0.773	624.447	0.126	32.93116	0.256053					
6:15	6675	100.138	6.818	624.862	0.227	100.147	7.427	625.133	0.211	100.107	3.887	624.523	0.203	100.138	3.398	624.832	0.195	99.993	0.773	624.447	0.126	32.92886	0.253746					
6:30	6690	100.138	6.818	624.862	0.227	100.147	7.427	625.133	0.211	100.107	3.887	624.523	0.203	100.138	3.398	624.832	0.195	99.993	0.773	624.447	0.126	32.92424	0.249133					
6:45	6705	100.138	6.818	624.862	0.227	100.147	7.427	625.133	0.211	100.107	3.887	624.523	0.203	100.132	3.392	624.838	0.189	99.993	0.773	624.447	0.126	32.91732	0.242213					
7:00	6720	100.138	6.818	624.862	0.227	100.147	7.427	625.133	0.211	100.107	3.887	624.523	0.203	100.132	3.392	624.838	0.189	99.993	0.773	624.447	0.126	32.91502	0.239906					
7:15	6735	100.138	6.818	624.862	0.227	100.147	7.427	625.133	0.211	100.107	3.887	624.523	0.203	100.132	3.392	624.838	0.189	99.993	0.773	624.447	0.126	32.90579	0.230679					
7:30	6750	100.145	6.825	624.855	0.234	100.147	7.427	625.133	0.211	100.114	3.894	624.516	0.21	100.138	3.398	624.832	0.195	99.993	0.773	624.447	0.126	32.91963	0.244519					

Date	Time	ET (min)	Feet H2O	Elevation	Delta H	Celsius
			msl			
07/03/96	14:00:00	0	100	625.75	0.012	13.22
07/03/96	14:15:00	15	100	625.75	0.012	13.24
07/03/96	14:30:00	30	100	625.75	0.012	13.24
07/03/96	14:45:00	45	100	625.75	0.012	13.24
07/03/96	15:00:00	60	100.005	625.745	0.017	13.24
07/03/96	15:15:00	75	100.005	625.745	0.017	13.24
07/03/96	15:30:00	90	100.005	625.745	0.017	13.24
07/03/96	15:45:00	105	100.005	625.745	0.017	13.23
07/03/96	16:00:00	120	100.005	625.745	0.017	13.23
07/03/96	16:15:00	135	100.005	625.745	0.017	13.23
07/03/96	16:30:00	150	100.005	625.745	0.017	13.23
07/03/96	16:45:00	165	100.009	625.741	0.021	13.24
07/03/96	17:00:00	180	100.005	625.745	0.017	13.23
07/03/96	17:15:00	195	100	625.75	0.012	13.23
07/03/96	17:30:00	210	99.995	625.755	0.007	13.22
07/03/96	17:45:00	225	100	625.75	0.012	13.21
07/03/96	18:00:00	240	100.005	625.745	0.017	13.22
07/03/96	18:15:00	255	100.005	625.745	0.017	13.22
07/03/96	18:30:00	270	100.005	625.745	0.017	13.23
07/03/96	18:45:00	285	100	625.75	0.012	13.22
07/03/96	19:00:00	300	100	625.75	0.012	13.22
07/03/96	19:15:00	315	100	625.75	0.012	13.22
07/03/96	19:30:00	330	99.995	625.755	0.007	13.21
07/03/96	19:45:00	345	99.995	625.755	0.007	13.21
07/03/96	20:00:00	360	99.995	625.755	0.007	13.21
07/03/96	20:15:00	375	99.995	625.755	0.007	13.21
07/03/96	20:30:00	390	99.995	625.755	0.007	13.22
07/03/96	20:45:00	405	99.995	625.755	0.007	13.22
07/03/96	21:00:00	420	99.995	625.755	0.007	13.22
07/03/96	21:15:00	435	99.995	625.755	0.007	13.23
07/03/96	21:30:00	450	99.995	625.755	0.007	13.23
07/03/96	21:45:00	465	99.995	625.755	0.007	13.23
07/03/96	22:00:00	480	99.995	625.755	0.007	13.23
07/03/96	22:15:00	495	99.991	625.759	0.003	13.23
07/03/96	22:30:00	510	99.991	625.759	0.003	13.23
07/03/96	22:45:00	525	99.988	625.762	0	13.23
07/03/96	23:00:00	540	99.991	625.759	0.003	13.23
07/03/96	23:15:00	555	99.993	625.757	0.005	13.23
07/03/96	23:30:00	570	99.988	625.762	0	13.23
07/03/96	23:45:00	585	99.993	625.757	0.005	13.23
07/04/96	0:00:00	600	99.993	625.757	0.005	13.23
07/04/96	0:15:00	615	99.988	625.762	0	13.23
07/04/96	0:30:00	630	99.993	625.757	0.005	13.23
07/04/96	0:45:00	645	99.988	625.762	0	13.24
07/04/96	1:00:00	660	99.993	625.757	0.005	13.24
07/04/96	1:15:00	675	99.993	625.757	0.005	13.24
07/04/96	1:30:00	690	99.995	625.755	0.007	13.24
07/04/96	1:45:00	705	99.993	625.757	0.005	13.24
07/04/96	2:00:00	720	99.993	625.757	0.005	13.24

Date	Time	ET (min)	Feet H2O	Elevation	Delta H	Celsius
07/04/96	2:15:00	735	99.993	625.757	0.005	13.24
07/04/96	2:30:00	750	99.993	625.757	0.005	13.24
07/04/96	2:45:00	765	99.998	625.752	0.01	13.24
07/04/96	3:00:00	780	99.993	625.757	0.005	13.24
07/04/96	3:15:00	795	99.993	625.757	0.005	13.24
07/04/96	3:30:00	810	99.993	625.757	0.005	13.24
07/04/96	3:45:00	825	99.993	625.757	0.005	13.24
07/04/96	4:00:00	840	99.998	625.752	0.01	13.24
07/04/96	4:15:00	855	99.998	625.752	0.01	13.24
07/04/96	4:30:00	870	99.998	625.752	0.01	13.24
07/04/96	4:45:00	885	99.998	625.752	0.01	13.25
07/04/96	5:00:00	900	99.998	625.752	0.01	13.25
07/04/96	5:15:00	915	99.998	625.752	0.01	13.25
07/04/96	5:30:00	930	99.998	625.752	0.01	13.25
07/04/96	5:45:00	945	99.998	625.752	0.01	13.26
07/04/96	6:00:00	960	100.002	625.748	0.014	13.26
07/04/96	6:15:00	975	100.002	625.748	0.014	13.26
07/04/96	6:30:00	990	100.002	625.748	0.014	13.26
07/04/96	6:45:00	1005	100.002	625.748	0.014	13.26
07/04/96	7:00:00	1020	100.002	625.748	0.014	13.26
07/04/96	7:15:00	1035	100.002	625.748	0.014	13.26
07/04/96	7:30:00	1050	100.007	625.743	0.019	13.26
07/04/96	7:45:00	1065	100.007	625.743	0.019	13.26
07/04/96	8:00:00	1080	100.007	625.743	0.019	13.26
07/04/96	8:15:00	1095	100.007	625.743	0.019	13.26
07/04/96	8:30:00	1110	100.007	625.743	0.019	13.26
07/04/96	8:45:00	1125	100.007	625.743	0.019	13.26
07/04/96	9:00:00	1140	100.007	625.743	0.019	13.26
07/04/96	9:15:00	1155	100.007	625.743	0.019	13.26
07/04/96	9:30:00	1170	100.007	625.743	0.019	13.26
07/04/96	9:45:00	1185	100.012	625.738	0.024	13.27
07/04/96	10:00:00	1200	100.012	625.738	0.024	13.27
07/04/96	10:15:00	1215	100.012	625.738	0.024	13.27
07/04/96	10:30:00	1230	100.012	625.738	0.024	13.27
07/04/96	10:45:00	1245	100.014	625.736	0.026	13.28
07/04/96	11:00:00	1260	100.014	625.736	0.026	13.27
07/04/96	11:15:00	1275	100.014	625.736	0.026	13.28
07/04/96	11:30:00	1290	100.014	625.736	0.026	13.28
07/04/96	11:45:00	1305	100.014	625.736	0.026	13.28
07/04/96	12:00:00	1320	100.018	625.732	0.03	13.28
07/04/96	12:15:00	1335	100.018	625.732	0.03	13.28
07/04/96	12:30:00	1350	100.014	625.736	0.026	13.28
07/04/96	12:45:00	1365	100.018	625.732	0.03	13.28
07/04/96	13:00:00	1380	100.018	625.732	0.03	13.28
07/04/96	13:15:00	1395	100.018	625.732	0.03	13.28
07/04/96	13:30:00	1410	100.018	625.732	0.03	13.28
07/04/96	13:45:00	1425	100.018	625.732	0.03	13.28
07/04/96	14:00:00	1440	100.018	625.732	0.03	13.28
07/04/96	14:15:00	1455	100.023	625.727	0.035	13.28
07/04/96	14:30:00	1470	100.018	625.732	0.03	13.28

Date	Time	ET (min)	Feet H2O	Elevation	Delta H	Celsius
07/04/96	14:45:00	1485	100.018	625.732	0.03	13.28
07/04/96	15:00:00	1500	100.018	625.732	0.03	13.28
07/04/96	15:15:00	1515	100.023	625.727	0.035	13.28
07/04/96	15:30:00	1530	100.023	625.727	0.035	13.28
07/04/96	15:45:00	1545	100.023	625.727	0.035	13.28
07/04/96	16:00:00	1560	100.023	625.727	0.035	13.28
07/04/96	16:15:00	1575	100.023	625.727	0.035	13.28
07/04/96	16:30:00	1590	100.023	625.727	0.035	13.28
07/04/96	16:45:00	1605	100.023	625.727	0.035	13.29
07/04/96	17:00:00	1620	100.028	625.722	0.04	13.29
07/04/96	17:15:00	1635	100.028	625.722	0.04	13.29
07/04/96	17:30:00	1650	100.028	625.722	0.04	13.29
07/04/96	17:45:00	1665	100.028	625.722	0.04	13.29
07/04/96	18:00:00	1680	100.028	625.722	0.04	13.29
07/04/96	18:15:00	1695	100.032	625.718	0.044	13.29
07/04/96	18:30:00	1710	100.032	625.718	0.044	13.29
07/04/96	18:45:00	1725	100.032	625.718	0.044	13.29
07/04/96	19:00:00	1740	100.032	625.718	0.044	13.29
07/04/96	19:15:00	1755	100.032	625.718	0.044	13.29
07/04/96	19:30:00	1770	100.032	625.718	0.044	13.29
07/04/96	19:45:00	1785	100.037	625.713	0.049	13.29
07/04/96	20:00:00	1800	100.037	625.713	0.049	13.29
07/04/96	20:15:00	1815	100.037	625.713	0.049	13.3
07/04/96	20:30:00	1830	100.037	625.713	0.049	13.3
07/04/96	20:45:00	1845	100.037	625.713	0.049	13.29
07/04/96	21:00:00	1860	100.037	625.713	0.049	13.29
07/04/96	21:15:00	1875	100.037	625.713	0.049	13.29
07/04/96	21:30:00	1890	100.037	625.713	0.049	13.3
07/04/96	21:45:00	1905	100.037	625.713	0.049	13.3
07/04/96	22:00:00	1920	100.037	625.713	0.049	13.3
07/04/96	22:15:00	1935	100.042	625.708	0.054	13.3
07/04/96	22:30:00	1950	100.042	625.708	0.054	13.3
07/04/96	22:45:00	1965	100.042	625.708	0.054	13.3
07/04/96	23:00:00	1980	100.042	625.708	0.054	13.3
07/04/96	23:15:00	1995	100.042	625.708	0.054	13.3
07/04/96	23:30:00	2010	100.042	625.708	0.054	13.3
07/04/96	23:45:00	2025	100.042	625.708	0.054	13.3
07/05/96	0:00:00	2040	100.042	625.708	0.054	13.3
07/05/96	0:15:00	2055	100.042	625.708	0.054	13.31
07/05/96	0:30:00	2070	100.042	625.708	0.054	13.31
07/05/96	0:45:00	2085	100.042	625.708	0.054	13.31
07/05/96	1:00:00	2100	100.042	625.708	0.054	13.3
07/05/96	1:15:00	2115	100.042	625.708	0.054	13.31
07/05/96	1:30:00	2130	100.042	625.708	0.054	13.31
07/05/96	1:45:00	2145	100.042	625.708	0.054	13.31
07/05/96	2:00:00	2160	100.046	625.704	0.058	13.31
07/05/96	2:15:00	2175	100.046	625.704	0.058	13.31
07/05/96	2:30:00	2190	100.046	625.704	0.058	13.31
07/05/96	2:45:00	2205	100.046	625.704	0.058	13.32
07/05/96	3:00:00	2220	100.046	625.704	0.058	13.32

Date	Time	ET (min)	Feet H2O	Elevation	Delta H	Celsius
07/05/96	3:15:00	2235	100.046	625.704	0.058	13.32
07/05/96	3:30:00	2250	100.046	625.704	0.058	13.32
07/05/96	3:45:00	2265	100.046	625.704	0.058	13.32
07/05/96	4:00:00	2280	100.046	625.704	0.058	13.32
07/05/96	4:15:00	2295	100.051	625.699	0.063	13.32
07/05/96	4:30:00	2310	100.051	625.699	0.063	13.32
07/05/96	4:45:00	2325	100.051	625.699	0.063	13.33
07/05/96	5:00:00	2340	100.051	625.699	0.063	13.33
07/05/96	5:15:00	2355	100.055	625.695	0.067	13.34
07/05/96	5:30:00	2370	100.051	625.699	0.063	13.34
07/05/96	5:45:00	2385	100.055	625.695	0.067	13.34
07/05/96	6:00:00	2400	100.055	625.695	0.067	13.34
07/05/96	6:15:00	2415	100.055	625.695	0.067	13.34
07/05/96	6:30:00	2430	100.06	625.69	0.072	13.34
07/05/96	6:45:00	2445	100.055	625.695	0.067	13.34
07/05/96	7:00:00	2460	100.06	625.69	0.072	13.34
07/05/96	7:15:00	2475	100.06	625.69	0.072	13.34
07/05/96	7:30:00	2490	100.06	625.69	0.072	13.34
07/05/96	7:45:00	2505	100.06	625.69	0.072	13.34
07/05/96	8:00:00	2520	100.06	625.69	0.072	13.34
07/05/96	8:15:00	2535	100.06	625.69	0.072	13.34
07/05/96	8:30:00	2550	100.06	625.69	0.072	13.34
07/05/96	8:45:00	2565	100.065	625.685	0.077	13.34
07/05/96	9:00:00	2580	100.06	625.69	0.072	13.34
07/05/96	9:15:00	2595	100.065	625.685	0.077	13.34
07/05/96	9:30:00	2610	100.065	625.685	0.077	13.34
07/05/96	9:45:00	2625	100.065	625.685	0.077	13.34
07/05/96	10:00:00	2640	100.069	625.681	0.081	13.34
07/05/96	10:15:00	2655	100.065	625.685	0.077	13.34
07/05/96	10:30:00	2670	100.065	625.685	0.077	13.34
07/05/96	10:45:00	2685	100.069	625.681	0.081	13.34
07/05/96	11:00:00	2700	100.069	625.681	0.081	13.34
07/05/96	11:15:00	2715	100.069	625.681	0.081	13.34
07/05/96	11:30:00	2730	100.069	625.681	0.081	13.34
07/05/96	11:45:00	2745	100.069	625.681	0.081	13.34
07/05/96	12:00:00	2760	100.069	625.681	0.081	13.34
07/05/96	12:15:00	2775	100.074	625.676	0.086	13.34
07/05/96	12:30:00	2790	100.069	625.681	0.081	13.34
07/05/96	12:45:00	2805	100.074	625.676	0.086	13.34
07/05/96	13:00:00	2820	100.069	625.681	0.081	13.34
07/05/96	13:15:00	2835	100.078	625.672	0.09	13.34
07/05/96	13:30:00	2850	100.083	625.667	0.095	13.34
07/05/96	13:45:00	2865	100.078	625.672	0.09	13.34
07/05/96	14:00:00	2880	100.083	625.667	0.095	13.32
07/05/96	14:15:00	2895		725.75		
07/05/96	14:30:00	2910		725.75		
07/05/96	14:45:00	2925		725.75		
07/05/96	15:00:00	2940		725.75		
07/05/96	15:15:00	2955		725.75		
07/05/96	15:30:00	2970		725.75		

Date	Time	ET (min)	Feet H2O	Elevation	Delta H	Celsius
07/05/96	15:45:00	2985		725.75		
07/05/96	16:00:00	3000	100.083	625.667	0.095	13.35
07/05/96	16:15:00	3015	100.078	625.672	0.09	13.37
07/05/96	16:30:00	3030	100.078	625.672	0.09	13.35
07/05/96	16:45:00	3045	100.078	625.672	0.09	13.35
07/05/96	17:00:00	3060	100.078	625.672	0.09	13.35
07/05/96	17:15:00	3075	100.078	625.672	0.09	13.34
07/05/96	17:30:00	3090	100.078	625.672	0.09	13.34
07/05/96	17:45:00	3105	100.078	625.672	0.09	13.34
07/05/96	18:00:00	3120	100.078	625.672	0.09	13.34
07/05/96	18:15:00	3135	100.078	625.672	0.09	13.33
07/05/96	18:30:00	3150	100.078	625.672	0.09	13.33
07/05/96	18:45:00	3165	100.078	625.672	0.09	13.32
07/05/96	19:00:00	3180	100.078	625.672	0.09	13.32
07/05/96	19:15:00	3195	100.078	625.672	0.09	13.32
07/05/96	19:30:00	3210	100.083	625.667	0.095	13.32
07/05/96	19:45:00	3225	100.083	625.667	0.095	13.32
07/05/96	20:00:00	3240	100.083	625.667	0.095	13.32
07/05/96	20:15:00	3255	100.083	625.667	0.095	13.33
07/05/96	20:30:00	3270	100.083	625.667	0.095	13.32
07/05/96	20:45:00	3285	100.083	625.667	0.095	13.32
07/05/96	21:00:00	3300	100.088	625.662	0.1	13.32
07/05/96	21:15:00	3315	100.083	625.667	0.095	13.32
07/05/96	21:30:00	3330	100.083	625.667	0.095	13.32
07/05/96	21:45:00	3345	100.083	625.667	0.095	13.32
07/05/96	22:00:00	3360	100.088	625.662	0.1	13.32
07/05/96	22:15:00	3375	100.083	625.667	0.095	13.32
07/05/96	22:30:00	3390	100.088	625.662	0.1	13.32
07/05/96	22:45:00	3405	100.083	625.667	0.095	13.32
07/05/96	23:00:00	3420	100.088	625.662	0.1	13.32
07/05/96	23:15:00	3435	100.083	625.667	0.095	13.32
07/05/96	23:30:00	3450	100.083	625.667	0.095	13.32
07/05/96	23:45:00	3465	100.088	625.662	0.1	13.32
07/06/96	0:00:00	3480	100.088	625.662	0.1	13.32
07/06/96	0:15:00	3495	100.088	625.662	0.1	13.32
07/06/96	0:30:00	3510	100.088	625.662	0.1	13.32
07/06/96	0:45:00	3525	100.088	625.662	0.1	13.32
07/06/96	1:00:00	3540	100.088	625.662	0.1	13.32
07/06/96	1:15:00	3555	100.088	625.662	0.1	13.33
07/06/96	1:30:00	3570	100.088	625.662	0.1	13.32
07/06/96	1:45:00	3585	100.088	625.662	0.1	13.32
07/06/96	2:00:00	3600	100.088	625.662	0.1	13.32
07/06/96	2:15:00	3615	100.088	625.662	0.1	13.32
07/06/96	2:30:00	3630	100.083	625.667	0.095	13.32
07/06/96	2:45:00	3645	100.083	625.667	0.095	13.32
07/06/96	3:00:00	3660	100.088	625.662	0.1	13.33
07/06/96	3:15:00	3675	100.088	625.662	0.1	13.33
07/06/96	3:30:00	3690	100.088	625.662	0.1	13.34
07/06/96	3:45:00	3705	100.083	625.667	0.095	13.33
07/06/96	4:00:00	3720	100.088	625.662	0.1	13.34

Date	Time	ET (min)	Feet H2O	Elevation	Delta H	Celsius
07/06/96	4:15:00	3735	100.088	625.662	0.1	13.34
07/06/96	4:30:00	3750	100.088	625.662	0.1	13.33
07/06/96	4:45:00	3765	100.088	625.662	0.1	13.34
07/06/96	5:00:00	3780	100.088	625.662	0.1	13.34
07/06/96	5:15:00	3795	100.088	625.662	0.1	13.34
07/06/96	5:30:00	3810	100.088	625.662	0.1	13.34
07/06/96	5:45:00	3825	100.088	625.662	0.1	13.34
07/06/96	6:00:00	3840	100.088	625.662	0.1	13.34
07/06/96	6:15:00	3855	100.088	625.662	0.1	13.34
07/06/96	6:30:00	3870	100.088	625.662	0.1	13.34
07/06/96	6:45:00	3885	100.092	625.658	0.104	13.34
07/06/96	7:00:00	3900	100.088	625.662	0.1	13.34
07/06/96	7:15:00	3915	100.088	625.662	0.1	13.34
07/06/96	7:30:00	3930	100.088	625.662	0.1	13.34
07/06/96	7:45:00	3945	100.088	625.662	0.1	13.34
07/06/96	8:00:00	3960	100.092	625.658	0.104	13.34
07/06/96	8:15:00	3975	100.088	625.662	0.1	13.35
07/06/96	8:30:00	3990	100.092	625.658	0.104	13.35
07/06/96	8:45:00	4005	100.088	625.662	0.1	13.35
07/06/96	9:00:00	4020	100.088	625.662	0.1	13.35
07/06/96	9:15:00	4035	100.092	625.658	0.104	13.35
07/06/96	9:30:00	4050	100.092	625.658	0.104	13.35
07/06/96	9:45:00	4065	100.092	625.658	0.104	13.35
07/06/96	10:00:00	4080	100.092	625.658	0.104	13.35
07/06/96	10:15:00	4095	100.092	625.658	0.104	13.34
07/06/96	10:30:00	4110	100.092	625.658	0.104	13.34
07/06/96	10:45:00	4125	100.092	625.658	0.104	13.34
07/06/96	11:00:00	4140	100.092	625.658	0.104	13.35
07/06/96	11:15:00	4155	100.092	625.658	0.104	13.35
07/06/96	11:30:00	4170	100.092	625.658	0.104	13.35
07/06/96	11:45:00	4185	100.097	625.653	0.109	13.35
07/06/96	12:00:00	4200	100.097	625.653	0.109	13.35
07/06/96	12:15:00	4215	100.097	625.653	0.109	13.35
07/06/96	12:30:00	4230	100.097	625.653	0.109	13.35
07/06/96	12:45:00	4245	100.101	625.649	0.113	13.34
07/06/96	13:00:00	4260	100.097	625.653	0.109	13.35
07/06/96	13:15:00	4275	100.101	625.649	0.113	13.35
07/06/96	13:30:00	4290	100.097	625.653	0.109	13.34
07/06/96	13:45:00	4305	100.097	625.653	0.109	13.34
07/06/96	14:00:00	4320	100.101	625.649	0.113	13.34
07/06/96	14:15:00	4335	100.101	625.649	0.113	13.34
07/06/96	14:30:00	4350	100.101	625.649	0.113	13.34
07/06/96	14:45:00	4365	100.101	625.649	0.113	13.34
07/06/96	15:00:00	4380	100.101	625.649	0.113	13.34
07/06/96	15:15:00	4395	100.101	625.649	0.113	13.34
07/06/96	15:30:00	4410	100.106	625.644	0.118	13.34
07/06/96	15:45:00	4425	100.101	625.649	0.113	13.34
07/06/96	16:00:00	4440	100.106	625.644	0.118	13.34
07/06/96	16:15:00	4455	100.106	625.644	0.118	13.35
07/06/96	16:30:00	4470	100.106	625.644	0.118	13.34

Date	Time	ET (min)	Feet H2O	Elevation	Delta H	Celsius
07/06/96	16:45:00	4485	100.106	625.644	0.118	13.34
07/06/96	17:00:00	4500	100.106	625.644	0.118	13.35
07/06/96	17:15:00	4515	100.106	625.644	0.118	13.35
07/06/96	17:30:00	4530	100.106	625.644	0.118	13.35
07/06/96	17:45:00	4545	100.111	625.639	0.123	13.35
07/06/96	18:00:00	4560	100.111	625.639	0.123	13.35
07/06/96	18:15:00	4575	100.115	625.635	0.127	13.35
07/06/96	18:30:00	4590	100.115	625.635	0.127	13.35
07/06/96	18:45:00	4605	100.115	625.635	0.127	13.35
07/06/96	19:00:00	4620	100.12	625.63	0.132	13.35
07/06/96	19:15:00	4635	100.12	625.63	0.132	13.35
07/06/96	19:30:00	4650	100.115	625.635	0.127	13.35
07/06/96	19:45:00	4665	100.12	625.63	0.132	13.35
07/06/96	20:00:00	4680	100.12	625.63	0.132	13.35
07/06/96	20:15:00	4695	100.12	625.63	0.132	13.35
07/06/96	20:30:00	4710	100.12	625.63	0.132	13.35
07/06/96	20:45:00	4725	100.12	625.63	0.132	13.35
07/06/96	21:00:00	4740	100.12	625.63	0.132	13.35
07/06/96	21:15:00	4755	100.12	625.63	0.132	13.35
07/06/96	21:30:00	4770	100.125	625.625	0.137	13.35
07/06/96	21:45:00	4785	100.12	625.63	0.132	13.35
07/06/96	22:00:00	4800	100.125	625.625	0.137	13.36
07/06/96	22:15:00	4815	100.125	625.625	0.137	13.36
07/06/96	22:30:00	4830	100.12	625.63	0.132	13.36
07/06/96	22:45:00	4845	100.12	625.63	0.132	13.36
07/06/96	23:00:00	4860	100.12	625.63	0.132	13.36
07/06/96	23:15:00	4875	100.125	625.625	0.137	13.36
07/06/96	23:30:00	4890	100.12	625.63	0.132	13.36
07/06/96	23:45:00	4905	100.12	625.63	0.132	13.36
07/07/96	0:00:00	4920	100.125	625.625	0.137	13.36
07/07/96	0:15:00	4935	100.125	625.625	0.137	13.36
07/07/96	0:30:00	4950	100.12	625.63	0.132	13.36
07/07/96	0:45:00	4965	100.125	625.625	0.137	13.36
07/07/96	1:00:00	4980	100.125	625.625	0.137	13.36
07/07/96	1:15:00	4995	100.125	625.625	0.137	13.36
07/07/96	1:30:00	5010	100.12	625.63	0.132	13.37
07/07/96	1:45:00	5025	100.125	625.625	0.137	13.37
07/07/96	2:00:00	5040	100.125	625.625	0.137	13.37
07/07/96	2:15:00	5055	100.125	625.625	0.137	13.37
07/07/96	2:30:00	5070	100.125	625.625	0.137	13.37
07/07/96	2:45:00	5085	100.12	625.63	0.132	13.37
07/07/96	3:00:00	5100	100.12	625.63	0.132	13.37
07/07/96	3:15:00	5115	100.12	625.63	0.132	13.37
07/07/96	3:30:00	5130	100.12	625.63	0.132	13.37
07/07/96	3:45:00	5145	100.12	625.63	0.132	13.37
07/07/96	4:00:00	5160	100.12	625.63	0.132	13.37
07/07/96	4:15:00	5175	100.125	625.625	0.137	13.37
07/07/96	4:30:00	5190	100.12	625.63	0.132	13.37
07/07/96	4:45:00	5205	100.125	625.625	0.137	13.38
07/07/96	5:00:00	5220	100.125	625.625	0.137	13.38

Date	Time	ET (min)	Feet H2O	Elevation	Delta H	Celsius
07/07/96	5:15:00	5235	100.125	625.625	0.137	13.38
07/07/96	5:30:00	5250	100.125	625.625	0.137	13.38
07/07/96	5:45:00	5265	100.125	625.625	0.137	13.38
07/07/96	6:00:00	5280	100.125	625.625	0.137	13.38
07/07/96	6:15:00	5295	100.125	625.625	0.137	13.38
07/07/96	6:30:00	5310	100.125	625.625	0.137	13.38
07/07/96	6:45:00	5325	100.125	625.625	0.137	13.38
07/07/96	7:00:00	5340	100.129	625.621	0.141	13.38
07/07/96	7:15:00	5355	100.129	625.621	0.141	13.39
07/07/96	7:30:00	5370	100.125	625.625	0.137	13.39
07/07/96	7:45:00	5385	100.125	625.625	0.137	13.39
07/07/96	8:00:00	5400	100.129	625.621	0.141	13.39
07/07/96	8:15:00	5415	100.125	625.625	0.137	13.39
07/07/96	8:30:00	5430	100.125	625.625	0.137	13.39
07/07/96	8:45:00	5445	100.129	625.621	0.141	13.39
07/07/96	9:00:00	5460	100.125	625.625	0.137	13.39
07/07/96	9:15:00	5475	100.125	625.625	0.137	13.39
07/07/96	9:30:00	5490	100.129	625.621	0.141	13.39
07/07/96	9:45:00	5505	100.129	625.621	0.141	13.39
07/07/96	10:00:00	5520	100.129	625.621	0.141	13.39
07/07/96	10:15:00	5535	100.129	625.621	0.141	13.39
07/07/96	10:30:00	5550	100.129	625.621	0.141	13.39
07/07/96	10:45:00	5565	100.129	625.621	0.141	13.39
07/07/96	11:00:00	5580	100.134	625.616	0.146	13.39
07/07/96	11:15:00	5595	100.129	625.621	0.141	13.39
07/07/96	11:30:00	5610	100.134	625.616	0.146	13.39
07/07/96	11:45:00	5625	100.134	625.616	0.146	13.39
07/07/96	12:00:00	5640	100.129	625.621	0.141	13.39
07/07/96	12:15:00	5655	100.134	625.616	0.146	13.39
07/07/96	12:30:00	5670	100.134	625.616	0.146	13.38
07/07/96	12:45:00	5685	100.134	625.616	0.146	13.39
07/07/96	13:00:00	5700	100.134	625.616	0.146	13.38
07/07/96	13:15:00	5715	100.134	625.616	0.146	13.38
07/07/96	13:30:00	5730	100.134	625.616	0.146	13.39
07/07/96	13:45:00	5745	100.138	625.612	0.15	13.39
07/07/96	14:00:00	5760	100.138	625.612	0.15	13.38
07/07/96	14:15:00	5775	100.134	625.616	0.146	13.38
07/07/96	14:30:00	5790	100.138	625.612	0.15	13.38
07/07/96	14:45:00	5805	100.138	625.612	0.15	13.38
07/07/96	15:00:00	5820	100.138	625.612	0.15	13.38
07/07/96	15:15:00	5835	100.138	625.612	0.15	13.39
07/07/96	15:30:00	5850	100.138	625.612	0.15	13.39
07/07/96	15:45:00	5865	100.143	625.607	0.155	13.39
07/07/96	16:00:00	5880	100.143	625.607	0.155	13.39
07/07/96	16:15:00	5895	100.143	625.607	0.155	13.39
07/07/96	16:30:00	5910	100.143	625.607	0.155	13.39
07/07/96	16:45:00	5925	100.143	625.607	0.155	13.39
07/07/96	17:00:00	5940	100.143	625.607	0.155	13.39
07/07/96	17:15:00	5955	100.143	625.607	0.155	13.39
07/07/96	17:30:00	5970	100.143	625.607	0.155	13.38

Date	Time	ET (min)	Feet H2O	Elevation	Delta H	Celsius
07/07/96	17:45:00	5985	100.143	625.607	0.155	13.39
07/07/96	18:00:00	6000	100.148	625.602	0.16	13.39
07/07/96	18:15:00	6015	100.143	625.607	0.155	13.39
07/07/96	18:30:00	6030	100.148	625.602	0.16	13.39
07/07/96	18:45:00	6045	100.143	625.607	0.155	13.39
07/07/96	19:00:00	6060	100.148	625.602	0.16	13.39
07/07/96	19:15:00	6075	100.148	625.602	0.16	13.4
07/07/96	19:30:00	6090	100.148	625.602	0.16	13.4
07/07/96	19:45:00	6105	100.152	625.598	0.164	13.4
07/07/96	20:00:00	6120	100.152	625.598	0.164	13.4
07/07/96	20:15:00	6135	100.152	625.598	0.164	13.4
07/07/96	20:30:00	6150	100.148	625.602	0.16	13.4
07/07/96	20:45:00	6165	100.152	625.598	0.164	13.4
07/07/96	21:00:00	6180	100.148	625.602	0.16	13.4
07/07/96	21:15:00	6195	100.152	625.598	0.164	13.4
07/07/96	21:30:00	6210	100.152	625.598	0.164	13.4
07/07/96	21:45:00	6225	100.152	625.598	0.164	13.4
07/07/96	22:00:00	6240	100.148	625.602	0.16	13.4
07/07/96	22:15:00	6255	100.157	625.593	0.169	13.4
07/07/96	22:30:00	6270	100.152	625.598	0.164	13.4
07/07/96	22:45:00	6285	100.152	625.598	0.164	13.4
07/07/96	23:00:00	6300	100.152	625.598	0.164	13.4
07/07/96	23:15:00	6315	100.148	625.602	0.16	13.4
07/07/96	23:30:00	6330	100.152	625.598	0.164	13.4
07/07/96	23:45:00	6345	100.152	625.598	0.164	13.4
07/08/96	0:00:00	6360	100.152	625.598	0.164	13.41
07/08/96	0:15:00	6375	100.152	625.598	0.164	13.41
07/08/96	0:30:00	6390	100.157	625.593	0.169	13.41
07/08/96	0:45:00	6405	100.152	625.598	0.164	13.41
07/08/96	1:00:00	6420	100.148	625.602	0.16	13.41
07/08/96	1:15:00	6435	100.148	625.602	0.16	13.41
07/08/96	1:30:00	6450	100.148	625.602	0.16	13.41
07/08/96	1:45:00	6465	100.148	625.602	0.16	13.41
07/08/96	2:00:00	6480	100.148	625.602	0.16	13.41
07/08/96	2:15:00	6495	100.152	625.598	0.164	13.41
07/08/96	2:30:00	6510	100.148	625.602	0.16	13.41
07/08/96	2:45:00	6525	100.143	625.607	0.155	13.41
07/08/96	3:00:00	6540	100.148	625.602	0.16	13.41
07/08/96	3:15:00	6555	100.148	625.602	0.16	13.41
07/08/96	3:30:00	6570	100.148	625.602	0.16	13.41
07/08/96	3:45:00	6585	100.148	625.602	0.16	13.41
07/08/96	4:00:00	6600	100.148	625.602	0.16	13.41
07/08/96	4:15:00	6615	100.148	625.602	0.16	13.42
07/08/96	4:30:00	6630	100.148	625.602	0.16	13.42
07/08/96	4:45:00	6645	100.152	625.598	0.164	13.42
07/08/96	5:00:00	6660	100.148	625.602	0.16	13.43
07/08/96	5:15:00	6675	100.157	625.593	0.169	13.43
07/08/96	5:30:00	6690	100.157	625.593	0.169	13.43
07/08/96	5:45:00	6705	100.157	625.593	0.169	13.43
07/08/96	6:00:00	6720	100.152	625.598	0.164	13.43

Date	Time	ET (min)	Feet H2O	Elevation	Delta H	Celsius
07/08/96	6:15:00	6735	100.161	625.589	0.173	13.43
07/08/96	6:30:00	6750	100.152	625.598	0.164	13.43
07/08/96	6:45:00	6765	100.152	625.598	0.164	13.43
07/08/96	7:00:00	6780	100.152	625.598	0.164	13.43
07/08/96	7:15:00	6795	100.152	625.598	0.164	13.43
07/08/96	7:30:00	6810	100.157	625.593	0.169	13.43
07/08/96	7:45:00	6825	100.157	625.593	0.169	13.43
07/08/96	8:00:00	6840	100.157	625.593	0.169	13.44
07/08/96	8:15:00	6855	100.157	625.593	0.169	13.43
07/08/96	8:30:00	6870	100.161	625.589	0.173	13.44
07/08/96	8:45:00	6885	100.161	625.589	0.173	13.45
07/08/96	9:00:00	6900	100.157	625.593	0.169	13.45



APPENDIX B

STEP-DRAWDOWN DATA

STOP INITIAL

		SE2000				
	Enviro	nmental L	gger			
		7/10 12:59				
	Unit# 6	54	T	est 1		
Setups:	INPUT 1	INPUT 2	INPUT 3	INPUT 4	INPUT 5	INPUT 6
	-----	-----	-----	-----	-----	-----
Type	Level (F)	Level (F)	Level (F)	Level (F)	Level (F)	Function
Mode	Surface	Surface	Surface	Surface	Surface	
I.D.	RW-2	MW-3	14S	14I	DC-P3	ATM
Reference	624.93	625.12	624.8	624.97	624.49	
PSI at Ref	8.71	8.807	3.684	6.337	0.492	
SG	1	1	1	1	1	
Linearity	0.118	0.092	0.121	0.062	0.138	0.024
Scale fact	19.926	20.218	20.069	20.002	19.99	8.028
Offset	0.02	-0.171	0.016	0.447	0.036	8.037
Delay ms	50	50	50	50	50	50
	Step 0	#####	50:01:00			
Elapsed Ti	INPUT 1	INPUT 2	INPUT 3	INPUT 4	INPUT 5	INPUT 6
	-----	-----	-----	-----	-----	-----
0	624.948	625.126	624.812	624.976	624.483	14.386
0.0083	624.948	625.126	624.812	624.976	624.483	14.387
0.0166	624.955	625.126	624.812	624.976	624.483	14.386
0.025	623.831	625.126	624.812	624.976	624.49	14.387
0.0333	625.081	625.126	624.812	624.976	624.49	14.386
0.0416	624.999	625.12	624.812	624.976	624.49	14.386
0.05	624.879	625.126	624.812	624.976	624.49	14.387
0.0583	624.892	625.126	624.812	624.976	624.49	14.387
0.0666	624.98	625.126	624.812	624.976	624.49	14.387
0.075	624.885	625.126	624.812	624.976	624.49	14.386
0.0833	624.816	625.126	624.812	624.976	624.49	14.387
0.0916	624.835	625.126	624.812	624.976	624.49	14.387
0.1	624.854	625.132	624.812	624.976	624.49	14.386
0.1083	624.904	625.12	624.812	624.976	624.49	14.386
0.1166	624.948	625.126	624.812	624.976	624.49	14.386
0.125	624.917	625.126	624.812	624.976	624.49	14.387
0.1333	624.828	625.126	624.812	624.976	624.49	14.386
0.1416	624.803	625.126	624.812	624.976	624.49	14.386
0.15	624.835	625.126	624.812	624.976	624.496	14.387
0.1583	624.917	625.12	624.812	624.976	624.49	14.387
0.1666	624.93	625.126	624.812	624.976	624.49	14.387
0.175	624.911	625.12	624.812	624.976	624.496	14.387
0.1833	624.847	625.12	624.812	624.976	624.49	14.386
0.1916	624.74	625.126	624.812	624.976	624.49	14.387
0.2	624.727	625.12	624.812	624.976	624.49	14.386
0.2083	624.753	625.12	624.812	624.976	624.49	14.386

I.D.	RW-2	MW-3	14S	14I	DC-P3	ATM
0.2166	624.803	625.126	624.812	624.976	624.49	14.386
0.225	624.791	625.12	624.812	624.976	624.49	14.387
0.2333	624.74	625.126	624.812	624.976	624.496	14.386
0.2416	624.652	625.12	624.812	624.976	624.49	14.386
0.25	624.652	625.126	624.812	624.976	624.49	14.387
0.2583	624.677	625.12	624.812	624.976	624.49	14.386
0.2666	624.709	625.12	624.812	624.976	624.49	14.387
0.275	624.784	625.12	624.812	624.976	624.49	14.386
0.2833	624.778	625.12	624.812	624.976	624.49	14.386
0.2916	624.709	625.12	624.812	624.976	624.49	14.386
0.3	624.62	625.126	624.812	624.976	624.49	14.387
0.3083	624.538	625.12	624.812	624.976	624.49	14.386
0.3166	624.551	625.12	624.812	624.976	624.49	14.386
0.325	624.626	625.12	624.812	624.976	624.49	14.387
0.3333	624.626	625.12	624.812	624.976	624.49	14.387
0.35	624.475	625.12	624.812	624.976	624.49	14.386
0.3666	624.507	625.12	624.812	624.97	624.49	14.387
0.3833	624.544	625.12	624.812	624.976	624.49	14.386
0.4	624.393	625.12	624.812	624.97	624.49	14.386
0.4166	624.481	625.12	624.812	624.97	624.49	14.387
0.4333	624.494	625.113	624.812	624.97	624.49	14.387
0.45	624.368	625.12	624.812	624.97	624.483	14.387
0.4666	624.349	625.12	624.812	624.97	624.49	14.386
0.4833	624.469	625.113	624.812	624.97	624.49	14.387
0.5	624.317	625.113	624.812	624.97	624.49	14.387
0.5166	624.406	625.113	624.812	624.97	624.49	14.387
0.5333	624.424	625.12	624.812	624.97	624.49	14.386
0.55	624.374	625.113	624.806	624.97	624.49	14.387
0.5666	624.298	625.113	624.812	624.97	624.49	14.386
0.5833	624.298	625.12	624.812	624.97	624.49	14.387
0.6	624.406	625.113	624.806	624.97	624.49	14.387
0.6166	624.38	625.113	624.806	624.97	624.49	14.386
0.6333	624.286	625.113	624.806	624.97	624.49	14.386
0.65	624.311	625.113	624.806	624.97	624.49	14.386
0.6666	624.424	625.113	624.806	624.97	624.49	14.386
0.6833	624.412	625.107	624.806	624.97	624.49	14.386
0.7	624.286	625.113	624.806	624.963	624.49	14.386
0.7166	624.342	625.113	624.806	624.963	624.49	14.387
0.7333	624.431	625.107	624.806	624.97	624.483	14.386
0.75	624.412	625.113	624.806	624.97	624.49	14.386
0.7666	624.361	625.107	624.806	624.963	624.49	14.386
0.7833	624.279	625.107	624.806	624.963	624.49	14.387
0.8	624.317	625.113	624.806	624.963	624.49	14.387
0.8166	624.399	625.107	624.806	624.963	624.49	14.386
0.8333	624.399	625.107	624.806	624.963	624.49	14.387
0.85	624.424	625.107	624.806	624.963	624.49	14.387
0.8666	624.412	625.107	624.806	624.963	624.49	14.387
0.8833	624.393	625.107	624.806	624.963	624.483	14.386
0.9	624.298	625.1	624.806	624.963	624.49	14.387
0.9166	624.273	625.107	624.806	624.963	624.49	14.387

I.D.	RW-2	MW-3	14S	14I	DC-P3	ATM
0.9333	624.374	625.1	624.806	624.963	624.49	14.387
0.95	624.406	625.107	624.806	624.963	624.49	14.387
0.9666	624.406	625.107	624.806	624.963	624.49	14.387
0.9833	624.399	625.1	624.806	624.963	624.49	14.387
1	624.399	625.1	624.806	624.963	624.49	14.387
1.2	624.273	625.1	624.8	624.957	624.483	14.388
1.4	624.361	625.094	624.793	624.957	624.483	14.388
1.6	624.26	625.094	624.8	624.957	624.483	14.388
1.8	624.292	625.094	624.793	624.957	624.483	14.388
2	624.279	625.094	624.793	624.951	624.483	14.387
2.2	624.109	625.088	624.793	624.951	624.483	14.388
2.4	624.153	625.081	624.793	624.951	624.477	14.388
2.6	624.216	625.081	624.793	624.951	624.477	14.388
2.8	624.21	625.075	624.787	624.944	624.483	14.388
3	624.185	625.081	624.787	624.951	624.483	14.386
3.2	624.058	625.081	624.793	624.944	624.483	14.387
3.4	624.065	625.075	624.787	624.944	624.483	14.387
3.6	624.172	625.075	624.787	624.944	624.483	14.387
3.8	624.153	625.075	624.787	624.944	624.483	14.387
4	624.197	625.075	624.787	624.944	624.483	14.388
4.2	624.077	625.068	624.787	624.944	624.483	14.387
4.4	624.166	625.068	624.787	624.938	624.483	14.388
4.6	624.185	625.062	624.78	624.938	624.483	14.387
4.8	624.147	625.068	624.78	624.938	624.49	14.387
5	624.197	625.068	624.78	624.938	624.483	14.388
5.2	624.197	625.068	624.787	624.938	624.477	14.387
5.4	624.039	625.062	624.78	624.938	624.483	14.387
5.6	624.046	625.062	624.787	624.938	624.483	14.386
5.8	624.09	625.062	624.78	624.938	624.477	14.387
6	624.185	625.062	624.78	624.938	624.477	14.387
6.2	624.185	625.056	624.78	624.938	624.477	14.387
6.4	624.077	625.056	624.78	624.938	624.477	14.386
6.6	624.033	625.056	624.78	624.938	624.483	14.387
6.8	624.058	625.056	624.78	624.938	624.483	14.387
7	624.052	625.056	624.78	624.938	624.477	14.387
7.2	624.172	625.056	624.78	624.938	624.483	14.386
7.4	624.134	625.056	624.78	624.932	624.483	14.386
7.6	624.084	625.056	624.78	624.938	624.483	14.387
7.8	624.058	625.056	624.78	624.938	624.483	14.386
8	624.09	625.056	624.78	624.932	624.483	14.386
8.2	624.147	625.056	624.78	624.932	624.483	14.386
8.4	624.071	625.056	624.78	624.932	624.477	14.386
8.6	624.103	625.049	624.78	624.932	624.483	14.387
8.8	624.039	625.056	624.78	624.932	624.483	14.387
9	624.115	625.049	624.78	624.932	624.483	14.388
9.2	624.147	625.049	624.774	624.932	624.483	14.387
9.4	624.159	625.049	624.78	624.932	624.483	14.387
9.6	624.096	625.049	624.774	624.932	624.483	14.388
9.8	624.033	625.049	624.774	624.932	624.483	14.388
10	624.153	625.049	624.774	624.932	624.483	14.389

I.D.	RW-2	MW-3	14S	14I	DC-P3	ATM
12	624.09	625.043	624.774	624.932	624.483	14.388
14	624.153	625.036	624.774	624.925	624.483	14.385
16	624.046	625.03	624.774	624.925	624.49	14.385
18	624.147	625.03	624.768	624.925	624.483	14.384
20	624.159	625.024	624.768	624.925	624.483	14.386
22	624.172	625.017	624.768	624.919	624.483	14.386
24	624.153	625.017	624.768	624.919	624.483	14.386
26	624.046	625.011	624.768	624.919	624.483	14.384
28	624.052	625.011	624.768	624.919	624.483	14.385
30	624.033	625.004	624.768	624.919	624.483	14.382
32	624.172	625.004	624.768	624.919	624.483	14.384
34	624.065	625.004	624.761	624.919	624.483	14.384
36	624.039	625.004	624.761	624.919	624.483	14.384
38	624.014	624.998	624.768	624.919	624.49	14.381
40	624.128	624.998	624.768	624.919	624.49	14.38
42	624.008	624.998	624.761	624.913	624.483	14.381
44	624.002	624.992	624.761	624.913	624.483	14.382
46	624.065	624.992	624.761	624.913	624.477	14.384
48	624.153	624.985	624.755	624.906	624.483	14.384
50	624.033	624.992	624.761	624.913	624.477	14.384
52	624.046	624.985	624.755	624.906	624.483	14.384
54	624.103	624.985	624.755	624.913	624.483	14.384
56	624.14	624.985	624.755	624.906	624.483	14.385
58	624.147	624.985	624.755	624.906	624.483	14.385
60	624.134	624.979	624.755	624.906	624.477	14.386
62	624.09	624.979	624.755	624.906	624.477	14.385
64	624.014	624.979	624.755	624.906	624.483	14.385
66	624.052	624.979	624.755	624.906	624.477	14.385
68	624.046	624.979	624.749	624.906	624.477	14.384
70	624.065	624.979	624.755	624.906	624.477	14.385
72	624.014	624.972	624.755	624.906	624.483	14.386
74	624.027	624.979	624.749	624.906	624.477	14.385
76	624.014	624.979	624.749	624.9	624.477	14.385
78	624.121	624.972	624.749	624.906	624.477	14.386
80	624.027	624.972	624.749	624.906	624.477	14.385
82	624.084	624.972	624.749	624.9	624.477	14.386
84	624.096	624.966	624.749	624.9	624.477	14.385
86	624.14	624.966	624.749	624.9	624.477	14.385
88	624.039	624.972	624.749	624.9	624.477	14.385
90	624.147	624.966	624.749	624.9	624.477	14.386
92	623.995	624.966	624.749	624.9	624.477	14.386
94	623.995	624.966	624.742	624.9	624.477	14.387
96	624.121	624.966	624.749	624.9	624.483	14.386
98	624.065	624.96	624.742	624.9	624.477	14.386
100	624.14	624.966	624.742	624.9	624.477	14.387

~~Step 2~~
TE ST 1

			SE2000			
	Enviro	nmental L	gger			
		7/10 13:06				
	Unit# 6	54	T est 1			
Setups:	INPUT 1	INPUT 2	INPUT 3	INPUT 4	INPUT 5	INPUT 6
Type	Level (F)	Level (F)	Level (F)	Level (F)	Level (F)	Function
Mode	Surface	Surface	Surface	Surface	Surface	
I.D.	RW-2	MW-3	14S	14I	DC-P3	ATM
Reference	624.93	625.12	624.8	624.97	624.49	
PSI at Ref	8.71	8.807	3.684	6.337	0.492	
SG	1	1	1	1	1	
Linearity	0.118	0.092	0.121	0.062	0.138	0.024
Scale fact	19.926	20.218	20.069	20.002	19.99	8.028
Offset	0.02	-0.171	0.016	0.447	0.036	8.037
Delay ms	50	50	50	50	50	50
	Step 1	#####	30:21:00			
Elapsed Ti	INPUT 1	INPUT 2	INPUT 3	INPUT 4	INPUT 5	INPUT 6
0	624.103	624.966	624.742	624.9	624.49	14.387
0.0083	624.14	624.966	624.749	624.9	624.49	14.386
0.0166	624.115	624.966	624.749	624.9	624.483	14.387
0.025	624.027	624.966	624.749	624.9	624.483	14.387
0.0333	623.995	624.966	624.749	624.9	624.483	14.387
0.0416	624.027	624.966	624.749	624.9	624.49	14.386
0.05	624.121	624.966	624.749	624.9	624.49	14.387
0.0583	624.084	624.966	624.749	624.9	624.483	14.387
0.0666	623.976	624.966	624.742	624.9	624.483	14.387
0.075	624.115	624.96	624.749	624.9	624.483	14.387
0.0833	623.976	624.966	624.749	624.9	624.483	14.387
0.0916	624.115	624.966	624.749	624.9	624.483	14.386
0.1	623.989	624.966	624.749	624.9	624.477	14.387
0.1083	624.058	624.966	624.742	624.9	624.483	14.386
0.1166	624.065	624.966	624.749	624.9	624.49	14.386
0.125	623.964	624.966	624.742	624.9	624.483	14.387
0.1333	624.096	624.966	624.749	624.9	624.483	14.386
0.1416	624.052	624.966	624.749	624.9	624.49	14.386
0.15	623.957	624.96	624.742	624.9	624.483	14.387
0.1583	624.033	624.966	624.749	624.9	624.483	14.386
0.1666	624.077	624.966	624.749	624.9	624.483	14.387
0.175	623.957	624.966	624.749	624.9	624.49	14.386
0.1833	624.033	624.966	624.742	624.9	624.483	14.386
0.1916	624.09	624.966	624.749	624.9	624.483	14.387
0.2	623.995	624.96	624.742	624.9	624.483	14.386
0.2083	623.976	624.966	624.749	624.9	624.483	14.386
0.2166	624.09	624.966	624.749	624.9	624.483	14.386

I.D.	RW-2	MW-3	14S	14I	DC-P3	ATM
0.225	624.014	624.966	624.749	624.9	624.483	14.386
0.2333	623.976	624.966	624.749	624.9	624.483	14.386
0.2416	624.09	624.966	624.749	624.9	624.483	14.385
0.25	623.964	624.966	624.749	624.9	624.49	14.387
0.2583	624.008	624.966	624.749	624.9	624.49	14.386
0.2666	624.065	624.966	624.749	624.9	624.483	14.386
0.275	623.938	624.966	624.749	624.9	624.483	14.387
0.2833	624.046	624.96	624.749	624.9	624.483	14.386
0.2916	624.065	624.966	624.749	624.9	624.49	14.385
0.3	623.957	624.966	624.749	624.9	624.483	14.385
0.3083	624.002	624.966	624.749	624.9	624.483	14.386
0.3166	624.065	624.966	624.749	624.9	624.483	14.386
0.325	623.938	624.966	624.749	624.9	624.49	14.386
0.3333	624.046	624.966	624.749	624.9	624.49	14.386
0.35	623.945	624.96	624.742	624.9	624.483	14.386
0.3666	623.964	624.96	624.742	624.9	624.483	14.386
0.3833	624.071	624.96	624.749	624.9	624.483	14.386
0.4	623.945	624.966	624.749	624.9	624.49	14.386
0.4166	623.957	624.96	624.749	624.9	624.483	14.387
0.4333	624.058	624.96	624.749	624.9	624.483	14.386
0.45	623.926	624.96	624.742	624.9	624.483	14.386
0.4666	623.919	624.96	624.749	624.9	624.483	14.386
0.4833	623.995	624.966	624.749	624.9	624.483	14.386
0.5	624.027	624.96	624.742	624.9	624.483	14.386
0.5166	624.039	624.966	624.749	624.9	624.483	14.387
0.5333	623.926	624.96	624.749	624.9	624.483	14.386
0.55	623.901	624.96	624.742	624.9	624.49	14.386
0.5666	623.926	624.96	624.742	624.9	624.483	14.387
0.5833	624.027	624.96	624.742	624.9	624.483	14.386
0.6	623.938	624.96	624.749	624.9	624.483	14.386
0.6166	623.888	624.96	624.749	624.9	624.483	14.386
0.6333	623.926	624.96	624.742	624.9	624.483	14.386
0.65	624.014	624.96	624.742	624.9	624.483	14.386
0.6666	623.907	624.96	624.749	624.9	624.483	14.387
0.6833	623.907	624.96	624.742	624.9	624.483	14.387
0.7	623.995	624.96	624.742	624.894	624.49	14.386
0.7166	623.938	624.96	624.749	624.9	624.483	14.387
0.7333	623.869	624.96	624.742	624.9	624.483	14.386
0.75	623.869	624.96	624.742	624.9	624.49	14.387
0.7666	623.957	624.953	624.749	624.894	624.483	14.387
0.7833	623.983	624.96	624.742	624.9	624.483	14.386
0.8	623.97	624.96	624.742	624.9	624.483	14.387
0.8166	623.964	624.96	624.742	624.9	624.483	14.386
0.8333	623.964	624.96	624.742	624.9	624.483	14.387
0.85	623.957	624.96	624.742	624.894	624.49	14.387
0.8666	623.957	624.96	624.742	624.9	624.483	14.387
0.8833	623.957	624.96	624.742	624.9	624.483	14.387
0.9	623.888	624.953	624.742	624.9	624.483	14.386
0.9166	623.882	624.96	624.742	624.894	624.483	14.387
0.9333	623.85	624.953	624.742	624.894	624.49	14.387

I.D.	RW-2	MW-3	14S	14I	DC-P3	ATM
0.95	623.869	624.953	624.749	624.894	624.483	14.387
0.9666	623.901	624.953	624.742	624.894	624.49	14.387
0.9833	623.831	624.953	624.742	624.894	624.483	14.387
1	623.926	624.953	624.742	624.894	624.483	14.386
1.2	623.762	624.953	624.742	624.894	624.49	14.386
1.4	623.831	624.947	624.742	624.887	624.483	14.387
1.6	623.825	624.947	624.736	624.887	624.477	14.388
1.8	623.781	624.947	624.736	624.887	624.483	14.386
2	623.642	624.947	624.736	624.887	624.477	14.386
2.2	623.755	624.94	624.736	624.887	624.477	14.386
2.4	623.616	624.94	624.736	624.887	624.477	14.387
2.6	623.724	624.934	624.73	624.881	624.483	14.388
2.8	623.673	624.934	624.73	624.881	624.477	14.388
3	623.598	624.934	624.736	624.881	624.483	14.387
3.2	623.699	624.934	624.73	624.881	624.477	14.387
3.4	623.616	624.934	624.73	624.875	624.483	14.388
3.6	623.616	624.928	624.73	624.875	624.477	14.387
3.8	623.68	624.928	624.723	624.875	624.477	14.388
4	623.61	624.928	624.723	624.875	624.477	14.388
4.2	623.61	624.928	624.723	624.875	624.477	14.387
4.4	623.547	624.928	624.723	624.875	624.477	14.387
4.6	623.686	624.921	624.723	624.875	624.477	14.387
4.8	623.661	624.921	624.723	624.868	624.477	14.387
5	623.667	624.921	624.717	624.868	624.477	14.387
5.2	623.553	624.921	624.723	624.868	624.477	14.387
5.4	623.528	624.921	624.723	624.875	624.477	14.387
5.6	623.623	624.921	624.723	624.868	624.477	14.387
5.8	623.629	624.915	624.723	624.868	624.477	14.387
6	623.629	624.915	624.717	624.868	624.477	14.387
6.2	623.661	624.915	624.723	624.868	624.477	14.387
6.4	623.648	624.915	624.723	624.868	624.477	14.387
6.6	623.623	624.915	624.717	624.868	624.477	14.387
6.8	623.585	624.915	624.717	624.868	624.477	14.387
7	623.648	624.915	624.723	624.868	624.477	14.387
7.2	623.541	624.915	624.717	624.868	624.477	14.387
7.4	623.553	624.915	624.717	624.862	624.477	14.387
7.6	623.522	624.908	624.717	624.862	624.477	14.387
7.8	623.591	624.908	624.717	624.862	624.483	14.387
8	623.522	624.908	624.717	624.862	624.477	14.387
8.2	623.528	624.908	624.717	624.862	624.477	14.387
8.4	623.61	624.908	624.717	624.862	624.477	14.387
8.6	623.522	624.908	624.717	624.862	624.477	14.387
8.8	623.654	624.908	624.717	624.862	624.477	14.387
9	623.654	624.908	624.717	624.862	624.477	14.387
9.2	623.547	624.908	624.711	624.862	624.477	14.387
9.4	623.534	624.908	624.717	624.862	624.483	14.387
9.6	623.534	624.902	624.717	624.862	624.477	14.386
9.8	623.553	624.902	624.717	624.862	624.477	14.386
10	623.667	624.902	624.717	624.862	624.49	14.387
12	623.528	624.896	624.717	624.862	624.49	14.385

I.D.	RW-2	MW-3	14S	14I	DC-P3	ATM
14	623.541	624.889	624.711	624.856	624.477	14.387
16	623.667	624.889	624.711	624.849	624.477	14.387
18	623.654	624.889	624.704	624.849	624.477	14.387
20	623.541	624.883	624.704	624.849	624.483	14.388
22	623.566	624.876	624.704	624.843	624.477	14.389
24	623.661	624.876	624.698	624.843	624.477	14.391
26	623.547	624.87	624.698	624.843	624.477	14.391
28	623.667	624.87	624.698	624.843	624.477	14.39
30	623.572	624.87	624.698	624.843	624.477	14.39
32	623.61	624.87	624.698	624.843	624.477	14.39
34	623.56	624.864	624.692	624.843	624.477	14.39
36	623.547	624.864	624.698	624.837	624.477	14.391
38	623.56	624.864	624.692	624.837	624.477	14.39
40	623.547	624.864	624.692	624.837	624.477	14.39
42	623.616	624.857	624.692	624.837	624.477	14.39
44	623.673	624.857	624.698	624.843	624.483	14.39
46	623.661	624.857	624.698	624.837	624.483	14.391
48	623.56	624.851	624.692	624.837	624.483	14.391
50	623.673	624.851	624.685	624.831	624.477	14.393
52	623.572	624.851	624.692	624.837	624.483	14.393
54	623.692	624.851	624.685	624.831	624.477	14.395
56	623.686	624.844	624.685	624.824	624.471	14.396
58	623.661	624.844	624.685	624.824	624.471	14.398
60	623.686	624.844	624.679	624.824	624.471	14.398
62	623.616	624.838	624.679	624.824	624.471	14.398
64	623.68	624.838	624.679	624.824	624.477	14.398
66	623.692	624.838	624.679	624.824	624.471	14.4
68	623.692	624.838	624.679	624.824	624.471	14.401
70	623.667	624.832	624.679	624.818	624.471	14.401
72	623.699	624.832	624.673	624.818	624.471	14.401
74	623.667	624.832	624.679	624.818	624.471	14.402
76	623.623	624.832	624.679	624.818	624.471	14.402
78	623.572	624.832	624.679	624.824	624.471	14.401
80	623.667	624.832	624.679	624.818	624.471	14.402
82	623.604	624.832	624.679	624.818	624.471	14.403
84	623.616	624.825	624.673	624.818	624.471	14.405
86	623.56	624.832	624.679	624.818	624.464	14.403
88	623.661	624.832	624.679	624.818	624.471	14.402
90	623.591	624.825	624.673	624.818	624.471	14.403
92	623.56	624.825	624.673	624.818	624.471	14.405
94	623.699	624.825	624.673	624.818	624.471	14.403
96	623.68	624.825	624.679	624.824	624.483	14.401
98	623.623	624.825	624.673	624.818	624.471	14.403

Step 2

			SE2000			
	Enviro	nmental L	gger			
		7/10 14:22				
	Unit# 6	54	T est 1			
Setups:	INPUT 1	INPUT 2	INPUT 3	INPUT 4	INPUT 5	INPUT 6
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Type	Level (F)	Function				
Mode	Surface	Surface	Surface	Surface	Surface	
I.D.	RW-2	MW-3	14S	14I	DC-P3	ATM
Reference	624.93	625.12	624.8	624.97	624.49	
PSI at Ref	8.71	8.807	3.684	6.337	0.492	
SG	1	1	1	1	1	
Linearity	0.118	0.092	0.121	0.062	0.138	0.024
Scale fact	19.926	20.218	20.069	20.002	19.99	8.028
Offset	0.02	-0.171	0.016	0.447	0.036	8.037
Delay mS	50	50	50	50	50	50
		Step 2	#####	10:08		
Elapsed Ti	INPUT 1	INPUT 2	INPUT 3	INPUT 4	INPUT 5	INPUT 6
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0	623.56	624.825	624.679	624.824	624.483	14.403
0.0083	623.591	624.825	624.679	624.818	624.483	14.403
0.0166	623.471	624.825	624.673	624.818	624.483	14.403
0.025	623.503	624.825	624.679	624.818	624.483	14.403
0.0333	623.604	624.825	624.679	624.818	624.477	14.403
0.0416	623.522	624.825	624.679	624.818	624.483	14.403
0.05	623.471	624.825	624.679	624.818	624.477	14.403
0.0583	623.604	624.825	624.679	624.818	624.477	14.402
0.0666	623.49	624.825	624.673	624.818	624.483	14.402
0.075	623.534	624.825	624.679	624.818	624.477	14.403
0.0833	623.579	624.825	624.673	624.818	624.483	14.402
0.0916	623.459	624.825	624.673	624.818	624.477	14.402
0.1	623.534	624.819	624.673	624.818	624.477	14.402
0.1083	623.585	624.825	624.679	624.818	624.483	14.402
0.1166	623.484	624.825	624.679	624.818	624.477	14.402
0.125	623.465	624.819	624.673	624.818	624.477	14.402
0.1333	623.566	624.825	624.679	624.818	624.483	14.403
0.1416	623.572	624.825	624.679	624.818	624.483	14.402
0.15	623.49	624.819	624.673	624.818	624.477	14.403
0.1583	623.446	624.819	624.673	624.818	624.477	14.403
0.1666	623.534	624.819	624.679	624.818	624.477	14.403
0.175	623.553	624.819	624.679	624.818	624.483	14.403
0.1833	623.44	624.819	624.679	624.818	624.477	14.402
0.1916	623.509	624.825	624.679	624.818	624.477	14.402
0.2	623.547	624.819	624.673	624.818	624.477	14.402
0.2083	623.427	624.825	624.679	624.818	624.477	14.402

I.D.	RW-2	MW-3	14S	14I	DC-P3	ATM
0.2166	623.49	624.819	624.673	624.818	624.477	14.402
0.225	623.553	624.819	624.673	624.818	624.477	14.403
0.2333	623.44	624.819	624.673	624.818	624.483	14.403
0.2416	623.44	624.819	624.679	624.818	624.477	14.403
0.25	623.553	624.825	624.673	624.818	624.477	14.402
0.2583	623.503	624.819	624.679	624.818	624.477	14.403
0.2666	623.415	624.825	624.673	624.818	624.483	14.403
0.275	623.465	624.819	624.673	624.818	624.477	14.403
0.2833	623.553	624.819	624.679	624.818	624.477	14.403
0.2916	623.471	624.819	624.673	624.818	624.483	14.403
0.3	623.433	624.819	624.679	624.818	624.477	14.403
0.3083	623.547	624.819	624.673	624.818	624.483	14.403
0.3166	623.459	624.825	624.673	624.818	624.477	14.403
0.325	623.427	624.819	624.673	624.818	624.477	14.403
0.3333	623.534	624.819	624.673	624.818	624.477	14.402
0.35	623.408	624.819	624.679	624.818	624.477	14.402
0.3666	623.515	624.819	624.673	624.818	624.477	14.403
0.3833	623.522	624.819	624.673	624.818	624.477	14.402
0.4	623.408	624.819	624.673	624.818	624.477	14.402
0.4166	623.459	624.819	624.673	624.818	624.477	14.402
0.4333	623.534	624.819	624.673	624.812	624.477	14.403
0.45	623.534	624.819	624.673	624.818	624.477	14.402
0.4666	623.465	624.819	624.673	624.818	624.483	14.403
0.4833	623.396	624.819	624.673	624.812	624.477	14.402
0.5	623.452	624.819	624.673	624.812	624.477	14.402
0.5166	623.522	624.819	624.673	624.812	624.477	14.402
0.5333	623.402	624.812	624.673	624.812	624.483	14.403
0.55	623.484	624.819	624.673	624.812	624.477	14.402
0.5666	623.503	624.819	624.673	624.812	624.477	14.402
0.5833	623.389	624.812	624.673	624.812	624.483	14.402
0.6	623.433	624.819	624.673	624.812	624.477	14.403
0.6166	623.503	624.819	624.673	624.812	624.483	14.402
0.6333	623.515	624.812	624.673	624.812	624.477	14.402
0.65	623.396	624.819	624.673	624.812	624.477	14.402
0.6666	623.446	624.819	624.673	624.812	624.477	14.402
0.6833	623.509	624.812	624.673	624.812	624.483	14.402
0.7	623.446	624.812	624.673	624.812	624.483	14.402
0.7166	623.37	624.812	624.673	624.812	624.477	14.403
0.7333	623.433	624.819	624.673	624.812	624.483	14.402
0.75	623.503	624.812	624.673	624.812	624.483	14.402
0.7666	623.396	624.812	624.673	624.812	624.477	14.402
0.7833	623.364	624.812	624.673	624.812	624.477	14.403
0.8	623.465	624.812	624.673	624.812	624.477	14.403
0.8166	623.459	624.812	624.673	624.812	624.477	14.403
0.8333	623.389	624.812	624.673	624.812	624.477	14.403
0.85	623.37	624.812	624.673	624.812	624.483	14.402
0.8666	623.478	624.812	624.673	624.812	624.483	14.403
0.8833	623.402	624.812	624.673	624.812	624.483	14.402
0.9	623.351	624.812	624.673	624.812	624.477	14.403
0.9166	623.452	624.812	624.673	624.812	624.477	14.402

I.D.	RW-2	MW-3	14S	14I	DC-P3	ATM
0.9333	623.37	624.812	624.673	624.812	624.483	14.402
0.95	623.351	624.812	624.673	624.812	624.477	14.402
0.9666	623.452	624.812	624.673	624.812	624.483	14.403
0.9833	623.421	624.806	624.673	624.812	624.477	14.402
1	623.332	624.812	624.673	624.812	624.483	14.402
1.2	623.402	624.806	624.673	624.812	624.477	14.403
1.4	623.276	624.8	624.673	624.805	624.477	14.402
1.6	623.225	624.8	624.673	624.805	624.483	14.402
1.8	623.25	624.793	624.666	624.799	624.477	14.402
2	623.225	624.793	624.666	624.799	624.477	14.401
2.2	623.187	624.787	624.66	624.793	624.483	14.402
2.4	623.156	624.78	624.66	624.793	624.483	14.402
2.6	623.08	624.774	624.66	624.793	624.477	14.402
2.8	622.992	624.774	624.654	624.786	624.483	14.402
3	623.048	624.78	624.654	624.786	624.477	14.401
3.2	622.998	624.774	624.654	624.78	624.477	14.402
3.4	622.916	624.774	624.647	624.78	624.477	14.401
3.6	623.03	624.774	624.647	624.774	624.477	14.403
3.8	622.884	624.774	624.647	624.774	624.483	14.402
4	622.884	624.768	624.641	624.774	624.483	14.402
4.2	622.922	624.768	624.641	624.774	624.477	14.402
4.4	622.973	624.768	624.641	624.767	624.477	14.401
4.6	622.847	624.761	624.641	624.767	624.483	14.402
4.8	622.922	624.768	624.641	624.767	624.477	14.402
5	622.948	624.761	624.641	624.761	624.477	14.402
5.2	622.922	624.755	624.635	624.761	624.483	14.402
5.4	622.897	624.755	624.628	624.755	624.477	14.402
5.6	622.847	624.755	624.628	624.755	624.483	14.401
5.8	622.815	624.761	624.628	624.755	624.477	14.402
6	622.884	624.755	624.628	624.755	624.477	14.403
6.2	622.922	624.755	624.628	624.748	624.477	14.403
6.4	622.815	624.755	624.628	624.748	624.477	14.403
6.6	622.922	624.755	624.622	624.748	624.477	14.402
6.8	622.91	624.748	624.622	624.748	624.477	14.402
7	622.783	624.748	624.622	624.748	624.483	14.402
7.2	622.878	624.748	624.622	624.742	624.483	14.401
7.4	622.796	624.755	624.622	624.742	624.477	14.402
7.6	622.79	624.748	624.622	624.742	624.477	14.403
7.8	622.916	624.748	624.616	624.742	624.477	14.403
8	622.878	624.748	624.616	624.742	624.477	14.402
8.2	622.916	624.748	624.616	624.736	624.477	14.402
8.4	622.859	624.748	624.616	624.736	624.477	14.403
8.6	622.828	624.742	624.616	624.736	624.477	14.402
8.8	622.815	624.742	624.616	624.736	624.477	14.402
9	622.872	624.742	624.616	624.736	624.483	14.402
9.2	622.903	624.742	624.609	624.729	624.477	14.402
9.4	622.79	624.742	624.609	624.729	624.477	14.402
9.6	622.884	624.742	624.616	624.729	624.477	14.401
9.8	622.847	624.742	624.616	624.736	624.477	14.401
10	622.884	624.742	624.616	624.729	624.477	14.402

I.D.	RW-2	MW-3	14S	14I	DC-P3	ATM
12	622.922	624.729	624.597	624.717	624.464	14.405
14	622.935	624.723	624.597	624.711	624.464	14.402
16	622.903	624.723	624.603	624.723	624.477	14.403
18	622.878	624.71	624.584	624.704	624.464	14.402
20	622.91	624.704	624.584	624.698	624.464	14.403
22	622.966	624.704	624.597	624.711	624.471	14.401
24	622.966	624.697	624.597	624.704	624.471	14.403
26	622.828	624.691	624.578	624.692	624.464	14.401
28	622.859	624.704	624.578	624.692	624.464	14.402
30	622.973	624.697	624.584	624.692	624.477	14.402
32	622.84	624.691	624.578	624.692	624.464	14.401
34	622.884	624.684	624.578	624.692	624.471	14.4
36	622.954	624.678	624.571	624.685	624.464	14.402
38	622.878	624.678	624.571	624.685	624.464	14.402
40	622.891	624.672	624.578	624.692	624.471	14.4
42	622.903	624.672	624.578	624.685	624.477	14.398
44	622.941	624.665	624.584	624.692	624.483	14.4
46	622.853	624.652	624.571	624.679	624.464	14.399
48	622.872	624.652	624.565	624.673	624.464	14.401
50	622.903	624.652	624.571	624.679	624.471	14.4
52	622.878	624.646	624.571	624.679	624.471	14.4
54	622.929	624.646	624.571	624.679	624.477	14.403
56	622.872	624.64	624.571	624.679	624.477	14.402
58	622.853	624.64	624.571	624.679	624.477	14.403
60	622.979	624.633	624.571	624.673	624.471	14.401
62	622.979	624.627	624.565	624.673	624.471	14.403
64	622.891	624.627	624.565	624.673	624.471	14.402
66	622.903	624.62	624.565	624.673	624.471	14.403
68	622.865	624.62	624.559	624.666	624.464	14.406
70	622.992	624.614	624.559	624.666	624.464	14.407
72	622.985	624.614	624.571	624.673	624.471	14.407
74	622.998	624.608	624.565	624.673	624.471	14.406
76	622.872	624.608	624.565	624.673	624.464	14.406
78	622.91	624.608	624.546	624.66	624.458	14.407
80	622.91	624.601	624.552	624.66	624.464	14.408
82	622.865	624.601	624.565	624.673	624.471	14.409
84	622.859	624.595	624.559	624.66	624.464	14.408
86	622.998	624.595	624.559	624.666	624.471	14.408
88	622.954	624.595	624.546	624.654	624.458	14.408
90	622.884	624.588	624.559	624.666	624.464	14.408
92	622.973	624.588	624.559	624.666	624.471	14.409
94	622.865	624.588	624.559	624.666	624.464	14.41
96	622.966	624.582	624.54	624.647	624.458	14.41
98	622.979	624.582	624.559	624.666	624.471	14.409
100	622.859	624.582	624.552	624.66	624.471	14.407

STEP 3 (RECOVERY OF STEP TEST)

		SE2000				
Enviro	nmental L	gger				
	7/10 14:28					
	Unit# 6	54	T	est 1		
Setups:	INPUT 1	INPUT 2	INPUT 3	INPUT 4	INPUT 5	INPUT 6
-----	-----	-----	-----	-----	-----	-----
Type	Level (F)	Level (F)	Level (F)	Level (F)	Level (F)	Function
Mode	Surface	Surface	Surface	Surface	Surface	
I.D.	RW-2	MW-3	14S	14I	DC-P3	ATM
Reference	624.93	625.12	624.8	624.97	624.49	
PSI at Ref	8.71	8.807	3.684	6.337	0.492	
SG	1	1	1	1	1	
Linearity	0.118	0.092	0.121	0.062	0.138	0.024
Scale fact	19.926	20.218	20.069	20.002	19.99	8.028
Offset	0.02	-0.171	0.016	0.447	0.036	8.037
Delay mS	50	50	50	50	50	50
	Step 3	#####	50:19:00			
Elapsed Ti	INPUT 1	INPUT 2	INPUT 3	INPUT 4	INPUT 5	INPUT 6
-----	-----	-----	-----	-----	-----	-----
0	622.998	624.582	624.546	624.66	624.471	14.408
0.0083	622.948	624.582	624.552	624.654	624.471	14.408
0.0166	622.865	624.582	624.546	624.66	624.471	14.407
0.025	622.897	624.582	624.552	624.66	624.471	14.408
0.0333	623.415	624.582	624.546	624.654	624.471	14.407
0.0416	623.162	624.582	624.552	624.66	624.477	14.407
0.05	623.112	624.582	624.552	624.66	624.471	14.407
0.0583	623.112	624.582	624.552	624.66	624.471	14.407
0.0666	623.099	624.582	624.552	624.66	624.471	14.406
0.075	623.105	624.582	624.552	624.66	624.464	14.407
0.0833	623.105	624.582	624.552	624.66	624.471	14.407
0.0916	623.105	624.582	624.552	624.66	624.471	14.407
0.1	623.105	624.582	624.552	624.66	624.471	14.407
0.1083	623.099	624.582	624.552	624.66	624.471	14.407
0.1166	623.099	624.582	624.552	624.66	624.471	14.406
0.125	623.099	624.582	624.552	624.66	624.471	14.406
0.1333	623.099	624.582	624.552	624.66	624.471	14.407
0.1416	623.105	624.582	624.552	624.66	624.477	14.407
0.15	623.099	624.582	624.552	624.66	624.471	14.407
0.1583	623.105	624.582	624.552	624.66	624.471	14.407
0.1666	623.105	624.582	624.552	624.66	624.477	14.406
0.175	623.105	624.582	624.552	624.66	624.471	14.407
0.1833	623.105	624.582	624.552	624.66	624.477	14.407
0.1916	623.105	624.582	624.552	624.66	624.477	14.407
0.2	623.112	624.588	624.552	624.66	624.471	14.407
0.2083	623.118	624.588	624.559	624.666	624.471	14.407

I.D.	RW-2	MW-3	14S	14I	DC-P3	ATM
0.2166	623.118	624.588	624.559	624.666	624.471	14.407
0.225	623.131	624.582	624.559	624.666	624.477	14.406
0.2333	623.131	624.588	624.559	624.666	624.471	14.406
0.2416	623.131	624.588	624.559	624.666	624.477	14.407
0.25	623.124	624.588	624.559	624.666	624.471	14.407
0.2583	623.131	624.588	624.559	624.666	624.471	14.407
0.2666	623.137	624.582	624.559	624.666	624.471	14.406
0.275	623.137	624.588	624.559	624.666	624.471	14.407
0.2833	623.143	624.588	624.559	624.666	624.471	14.407
0.2916	623.149	624.588	624.559	624.666	624.471	14.407
0.3	623.149	624.588	624.559	624.666	624.471	14.407
0.3083	623.158	624.588	624.559	624.666	624.471	14.406
0.3166	623.149	624.588	624.559	624.666	624.471	14.407
0.325	623.156	624.588	624.559	624.666	624.471	14.407
0.3333	623.156	624.588	624.552	624.66	624.471	14.407
0.35	623.156	624.588	624.552	624.666	624.471	14.407
0.3666	623.156	624.588	624.559	624.666	624.471	14.408
0.3833	623.162	624.588	624.559	624.666	624.471	14.407
0.4	623.162	624.588	624.559	624.666	624.471	14.407
0.4166	623.168	624.588	624.559	624.666	624.477	14.407
0.4333	623.168	624.588	624.559	624.666	624.477	14.407
0.45	623.168	624.595	624.559	624.666	624.471	14.407
0.4666	623.168	624.588	624.565	624.666	624.471	14.407
0.4833	623.168	624.588	624.559	624.673	624.471	14.407
0.5	623.175	624.588	624.565	624.673	624.477	14.407
0.5166	623.175	624.588	624.565	624.673	624.477	14.407
0.5333	623.181	624.595	624.565	624.673	624.477	14.408
0.55	623.181	624.588	624.565	624.673	624.477	14.407
0.5666	623.181	624.595	624.565	624.673	624.477	14.407
0.5833	623.187	624.595	624.565	624.673	624.477	14.407
0.6	623.187	624.595	624.565	624.679	624.477	14.407
0.6166	623.2	624.595	624.565	624.679	624.477	14.407
0.6333	623.194	624.595	624.571	624.679	624.477	14.407
0.65	623.2	624.595	624.571	624.679	624.477	14.407
0.6666	623.2	624.595	624.571	624.679	624.477	14.407
0.6833	623.206	624.595	624.571	624.679	624.477	14.408
0.7	623.206	624.595	624.571	624.679	624.477	14.408
0.7166	623.206	624.595	624.571	624.679	624.477	14.407
0.7333	623.213	624.595	624.571	624.679	624.477	14.408
0.75	623.219	624.595	624.571	624.679	624.477	14.408
0.7666	623.219	624.595	624.571	624.679	624.477	14.407
0.7833	623.225	624.595	624.571	624.679	624.477	14.408
0.8	623.225	624.595	624.571	624.679	624.477	14.407
0.8166	623.225	624.595	624.578	624.685	624.477	14.408
0.8333	623.231	624.601	624.578	624.685	624.477	14.408
0.85	623.238	624.595	624.571	624.685	624.477	14.408
0.8666	623.238	624.601	624.578	624.685	624.477	14.408
0.8833	623.263	624.601	624.578	624.685	624.477	14.408
0.9	623.32	624.595	624.578	624.685	624.477	14.408
0.9166	623.351	624.601	624.578	624.685	624.477	14.408

I.D.	RW-2	MW-3	14S	14I	DC-P3	ATM
12	624.709	624.729	624.685	624.837	624.464	14.407
14	624.721	624.748	624.685	624.843	624.464	14.408
16	624.734	624.761	624.685	624.843	624.458	14.408
18	624.746	624.774	624.704	624.862	624.464	14.41
20	624.753	624.78	624.698	624.856	624.458	14.41
22	624.759	624.793	624.704	624.862	624.458	14.411
24	624.772	624.812	624.711	624.875	624.471	14.409

STEP Drawdown

IN_SITU INC.	TROLL			
Serial number:	755			
Unit name:	SP4000			
Report generated:	7/12/96	11:07:35		
Report from file:	TMP1.\$\$\$			
Test name:	17sStep1			
Test defined on:	7/10/96	7:11:47		
Test scheduled for:	7/10/96	7:30:00		
Test started on:	7/10/96	7:30:00		
Test stopped on:	7/12/96	11:06:38		
Test extracted on:	7/12/96	11:07:01		
Data gathered using Linear testing				
Time between data points:	10.0000	Minutes		
Number of data samples:	310			
Channel number [2]				
Measurement type:	Pressure/Level			
Channel name:	OnBoard Pressure			
Specific gravity:	1			
Mode:	Surface			
User-defined reference:	625.76	Feet H2O		
Referenced on:	test start			
Pressure head at reference:	5.04	Feet H2O		
Channel number [1]				
Measurement type:	Temperature			
Channel name:	OnBoard Temp			
Date	Time	ET (min)	Channel[2] Feet H2O	Channel[1] Celsius
-----	-----	-----	-----	-----
7/10/96	7:30:00	0	625.76	13.89
7/10/96	7:40:00	10	625.765	13.85
7/10/96	7:50:00	20	625.76	13.84
7/10/96	8:00:00	30	625.76	13.84
7/10/96	8:10:00	40	625.76	13.84
7/10/96	8:20:00	50	625.76	13.84
7/10/96	8:30:00	60	625.76	13.84
7/10/96	8:40:00	70	625.76	13.84
7/10/96	8:50:00	80	625.755	13.84
7/10/96	9:00:00	90	625.755	13.84
7/10/96	9:10:00	100	625.755	13.84
7/10/96	9:20:00	110	625.755	13.84
7/10/96	9:30:00	120	625.751	13.84
7/10/96	9:40:00	130	625.746	13.85
7/10/96	9:50:00	140	625.746	13.85

Date	Time	ET (min)	Feet H2O	Celsius
7/10/96	10:00:00	150	625.746	13.85
7/10/96	10:10:00	160	625.742	13.85
7/10/96	10:20:00	170	625.737	13.86
7/10/96	10:30:00	180	625.737	13.86
7/10/96	10:40:00	190	625.732	13.85
7/10/96	10:50:00	200	625.728	13.86
7/10/96	11:00:00	210	625.728	13.86
7/10/96	11:10:00	220	625.723	13.86
7/10/96	11:20:00	230	625.718	13.86
7/10/96	11:30:00	240	625.714	13.86
7/10/96	11:40:00	250	625.709	13.87
7/10/96	11:50:00	260	625.709	13.87
7/10/96	12:00:00	270	625.709	13.87
7/10/96	12:10:00	280	625.707	13.87
7/10/96	12:20:00	290	625.702	13.87
7/10/96	12:30:00	300	625.693	13.87
7/10/96	12:40:00	310	625.688	13.87
7/10/96	12:50:00	320	625.684	13.88
7/10/96	13:00:00	330	625.679	13.88
7/10/96	13:10:00	340	625.675	13.88
7/10/96	13:20:00	350	625.67	13.89
7/10/96	13:30:00	360	625.665	13.88
7/10/96	13:40:00	370	625.661	13.88
7/10/96	13:50:00	380	625.656	13.89
7/10/96	14:00:00	390	625.656	13.88
7/10/96	14:10:00	400	625.665	13.88
7/10/96	14:20:00	410	625.67	13.88
7/10/96	14:30:00	420	625.675	13.87
7/10/96	14:40:00	430	625.675	13.86
7/10/96	14:50:00	440	625.679	13.86
7/10/96	15:00:00	450	625.679	13.85
7/10/96	15:10:00	460	625.679	13.84
7/10/96	15:20:00	470	625.679	13.84
7/10/96	15:30:00	480	625.684	13.84
7/10/96	15:40:00	490	625.684	13.83
7/10/96	15:50:00	500	625.679	13.83
7/10/96	16:00:00	510	625.679	13.83
7/10/96	16:10:00	520	625.684	13.83
7/10/96	16:20:00	530	625.679	13.83
7/10/96	16:30:00	540	625.679	13.83
7/10/96	16:40:00	550	625.679	13.83
7/10/96	16:50:00	560	625.679	13.83
7/10/96	17:00:00	570	625.679	13.83
7/10/96	17:10:00	580	625.679	13.83
7/10/96	17:20:00	590	625.679	13.83
7/10/96	17:30:00	600	625.675	13.83
7/10/96	17:40:00	610	625.675	13.83
7/10/96	17:50:00	620	625.675	13.83
7/10/96	18:00:00	630	625.675	13.83
7/10/96	18:10:00	640	625.675	13.83

Date	Time	ET (min)	Feet H2O	Celsius
7/10/96	18:20:00	650	625.675	13.83
7/10/96	18:30:00	660	625.67	13.83
7/10/96	18:40:00	670	625.67	13.83
7/10/96	18:50:00	680	625.67	13.83
7/10/96	19:00:00	690	625.67	13.83
7/10/96	19:10:00	700	625.665	13.83
7/10/96	19:20:00	710	625.67	13.83
7/10/96	19:30:00	720	625.665	13.83
7/10/96	19:40:00	730	625.665	13.83
7/10/96	19:50:00	740	625.661	13.83
7/10/96	20:00:00	750	625.661	13.83
7/10/96	20:10:00	760	625.661	13.83
7/10/96	20:20:00	770	625.661	13.83
7/10/96	20:30:00	780	625.661	13.83
7/10/96	20:40:00	790	625.661	13.83
7/10/96	20:50:00	800	625.656	13.83
7/10/96	21:00:00	810	625.656	13.83
7/10/96	21:10:00	820	625.656	13.83
7/10/96	21:20:00	830	625.656	13.83
7/10/96	21:30:00	840	625.656	13.83
7/10/96	21:40:00	850	625.656	13.83
7/10/96	21:50:00	860	625.656	13.83
7/10/96	22:00:00	870	625.656	13.83
7/10/96	22:10:00	880	625.656	13.83
7/10/96	22:20:00	890	625.656	13.83
7/10/96	22:30:00	900	625.652	13.83
7/10/96	22:40:00	910	625.652	13.83
7/10/96	22:50:00	920	625.652	13.83
7/10/96	23:00:00	930	625.652	13.83
7/10/96	23:10:00	940	625.652	13.83
7/10/96	23:20:00	950	625.652	13.83
7/10/96	23:30:00	960	625.652	13.83
7/10/96	23:40:00	970	625.652	13.83
7/10/96	23:50:00	980	625.652	13.83
7/11/96	0:00:00	990	625.652	13.83
7/11/96	0:10:00	1000	625.652	13.83
7/11/96	0:20:00	1010	625.652	13.83
7/11/96	0:30:00	1020	625.647	13.83
7/11/96	0:40:00	1030	625.647	13.83
7/11/96	0:50:00	1040	625.647	13.83
7/11/96	1:00:00	1050	625.647	13.83
7/11/96	1:10:00	1060	625.652	13.83
7/11/96	1:20:00	1070	625.647	13.83
7/11/96	1:30:00	1080	625.647	13.83
7/11/96	1:40:00	1090	625.652	13.84
7/11/96	1:50:00	1100	625.647	13.84
7/11/96	2:00:00	1110	625.647	13.83
7/11/96	2:10:00	1120	625.647	13.84
7/11/96	2:20:00	1130	625.647	13.84
7/11/96	2:30:00	1140	625.647	13.84

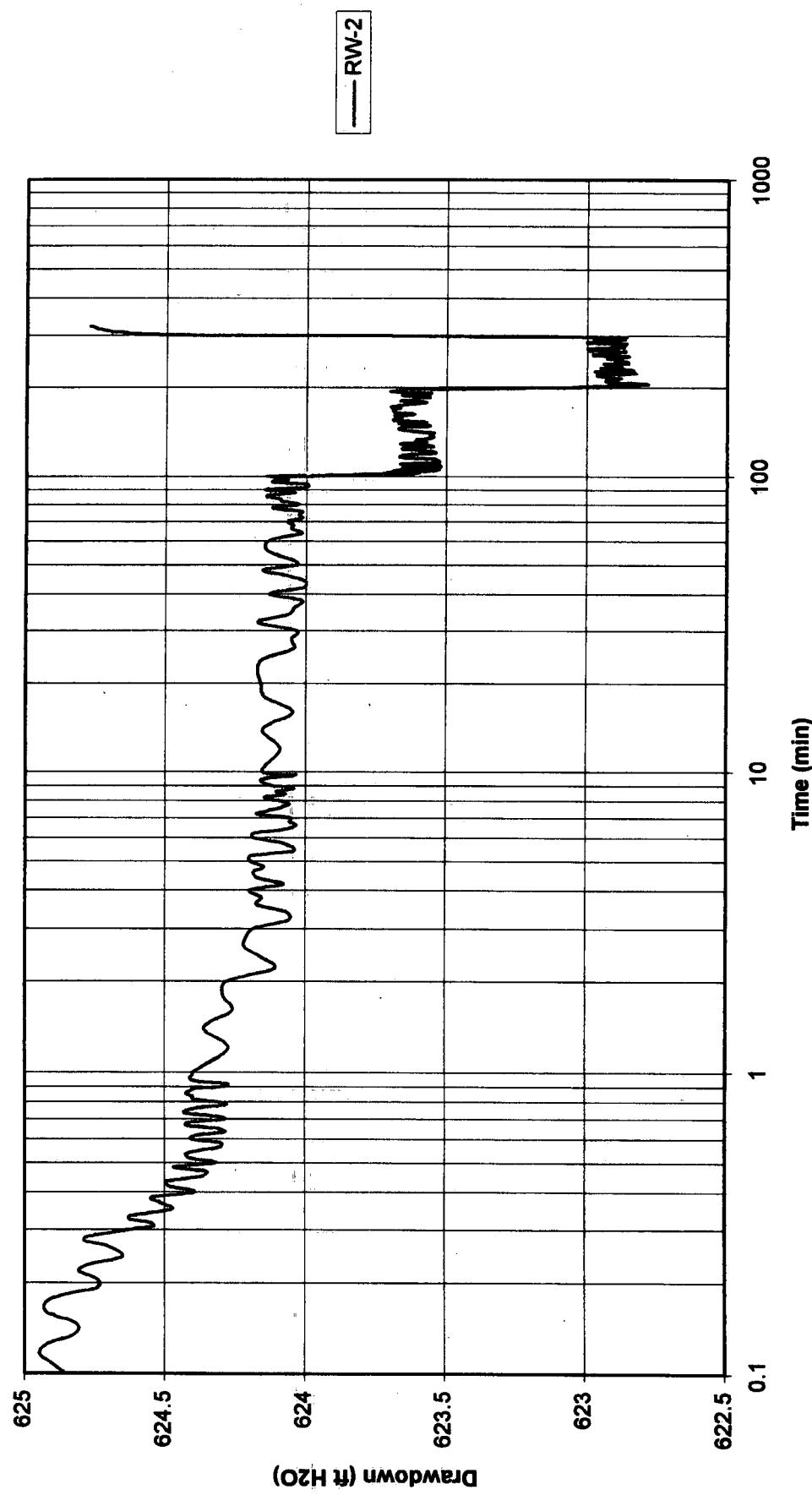
Date	Time	ET (min)	Feet H2O	Celsius
7/11/96	2:40:00	1150	625.647	13.83
7/11/96	2:50:00	1160	625.647	13.84
7/11/96	3:00:00	1170	625.647	13.83
7/11/96	3:10:00	1180	625.647	13.84
7/11/96	3:20:00	1190	625.647	13.84
7/11/96	3:30:00	1200	625.647	13.84
7/11/96	3:40:00	1210	625.647	13.84
7/11/96	3:50:00	1220	625.647	13.84
7/11/96	4:00:00	1230	625.647	13.84
7/11/96	4:10:00	1240	625.647	13.84
7/11/96	4:20:00	1250	625.647	13.84
7/11/96	4:30:00	1260	625.645	13.84
7/11/96	4:40:00	1270	625.645	13.84
7/11/96	4:50:00	1280	625.647	13.84
7/11/96	5:00:00	1290	625.645	13.84
7/11/96	5:10:00	1300	625.642	13.84
7/11/96	5:20:00	1310	625.645	13.84
7/11/96	5:30:00	1320	625.645	13.84
7/11/96	5:40:00	1330	625.64	13.84
7/11/96	5:50:00	1340	625.642	13.84
7/11/96	6:00:00	1350	625.64	13.84
7/11/96	6:10:00	1360	625.642	13.84
7/11/96	6:20:00	1370	625.64	13.84
7/11/96	6:30:00	1380	625.638	13.85
7/11/96	6:40:00	1390	625.64	13.84
7/11/96	6:50:00	1400	625.64	13.84
7/11/96	7:00:00	1410	625.638	13.85
7/11/96	7:10:00	1420	625.638	13.85
7/11/96	7:20:00	1430	625.64	13.84
7/11/96	7:30:00	1440	625.638	13.85
7/11/96	7:40:00	1450	625.638	13.85
7/11/96	7:50:00	1460	625.638	13.85
7/11/96	8:00:00	1470	625.635	13.85
7/11/96	8:10:00	1480	625.635	13.85
7/11/96	8:20:00	1490	625.635	13.85
7/11/96	8:30:00	1500	625.635	13.85
7/11/96	8:40:00	1510	625.635	13.86
7/11/96	8:50:00	1520	625.631	13.85
7/11/96	9:00:00	1530	625.635	13.86
7/11/96	9:10:00	1540	625.635	13.86
7/11/96	9:20:00	1550	625.631	13.86
7/11/96	9:30:00	1560	625.631	13.86
7/11/96	9:40:00	1570	625.631	13.86
7/11/96	9:50:00	1580	625.631	13.85
7/11/96	10:00:00	1590	625.626	13.86
7/11/96	10:10:00	1600	625.631	13.86
7/11/96	10:20:00	1610	625.626	13.86
7/11/96	10:30:00	1620	625.626	13.86
7/11/96	10:40:00	1630	625.626	13.86
7/11/96	10:50:00	1640	625.626	13.86

Date	Time	ET (min)	Feet H2O	Celsius
7/11/96	11:00:00	1650	625.626	13.86
7/11/96	11:10:00	1660	625.626	13.86
7/11/96	11:20:00	1670	625.622	13.85
7/11/96	11:30:00	1680	625.622	13.86
7/11/96	11:40:00	1690	625.622	13.86
7/11/96	11:50:00	1700	625.622	13.85
7/11/96	12:00:00	1710	625.622	13.86
7/11/96	12:10:00	1720	625.622	13.86
7/11/96	12:20:00	1730	625.622	13.85
7/11/96	12:30:00	1740	625.622	13.86
7/11/96	12:40:00	1750	625.622	13.85
7/11/96	12:50:00	1760	625.617	13.85
7/11/96	13:00:00	1770	625.622	13.85
7/11/96	13:10:00	1780	625.617	13.85
7/11/96	13:20:00	1790	625.622	13.85
7/11/96	13:30:00	1800	625.622	13.85
7/11/96	13:40:00	1810	625.622	13.84
7/11/96	13:50:00	1820	625.617	13.84
7/11/96	14:00:00	1830	625.617	13.84
7/11/96	14:10:00	1840	625.617	13.84
7/11/96	14:20:00	1850	625.617	13.84
7/11/96	14:30:00	1860	625.617	13.84
7/11/96	14:40:00	1870	625.612	13.84
7/11/96	14:50:00	1880	625.617	13.84
7/11/96	15:00:00	1890	625.612	13.84
7/11/96	15:10:00	1900	625.612	13.84
7/11/96	15:20:00	1910	625.612	13.84
7/11/96	15:30:00	1920	625.612	13.84
7/11/96	15:40:00	1930	625.612	13.84
7/11/96	15:50:00	1940	625.612	13.84
7/11/96	16:00:00	1950	625.612	13.84
7/11/96	16:10:00	1960	625.612	13.84
7/11/96	16:20:00	1970	625.612	13.84
7/11/96	16:30:00	1980	625.612	13.84
7/11/96	16:40:00	1990	625.612	13.84
7/11/96	16:50:00	2000	625.612	13.84
7/11/96	17:00:00	2010	625.608	13.84
7/11/96	17:10:00	2020	625.612	13.84
7/11/96	17:20:00	2030	625.608	13.84
7/11/96	17:30:00	2040	625.608	13.84
7/11/96	17:40:00	2050	625.608	13.84
7/11/96	17:50:00	2060	625.608	13.84
7/11/96	18:00:00	2070	625.603	13.84
7/11/96	18:10:00	2080	625.608	13.84
7/11/96	18:20:00	2090	625.608	13.84
7/11/96	18:30:00	2100	625.603	13.84
7/11/96	18:40:00	2110	625.603	13.84
7/11/96	18:50:00	2120	625.603	13.84
7/11/96	19:00:00	2130	625.603	13.84
7/11/96	19:10:00	2140	625.603	13.84

Date	Time	ET (min)	Feet H2O	Celsius
7/11/96	19:20:00	2150	625.603	13.84
7/11/96	19:30:00	2160	625.603	13.84
7/11/96	19:40:00	2170	625.603	13.84
7/11/96	19:50:00	2180	625.603	13.85
7/11/96	20:00:00	2190	625.603	13.85
7/11/96	20:10:00	2200	625.599	13.85
7/11/96	20:20:00	2210	625.599	13.84
7/11/96	20:30:00	2220	625.599	13.84
7/11/96	20:40:00	2230	625.599	13.85
7/11/96	20:50:00	2240	625.599	13.85
7/11/96	21:00:00	2250	625.599	13.85
7/11/96	21:10:00	2260	625.594	13.85
7/11/96	21:20:00	2270	625.599	13.85
7/11/96	21:30:00	2280	625.589	13.85
7/11/96	21:40:00	2290	625.594	13.85
7/11/96	21:50:00	2300	625.589	13.85
7/11/96	22:00:00	2310	625.589	13.86
7/11/96	22:10:00	2320	625.594	13.86
7/11/96	22:20:00	2330	625.594	13.85
7/11/96	22:30:00	2340	625.589	13.86
7/11/96	22:40:00	2350	625.589	13.85
7/11/96	22:50:00	2360	625.589	13.85
7/11/96	23:00:00	2370	625.589	13.85
7/11/96	23:10:00	2380	625.585	13.85
7/11/96	23:20:00	2390	625.585	13.86
7/11/96	23:30:00	2400	625.589	13.86
7/11/96	23:40:00	2410	625.585	13.86
7/11/96	23:50:00	2420	625.589	13.86
7/12/96	0:00:00	2430	625.589	13.85
7/12/96	0:10:00	2440	625.589	13.86
7/12/96	0:20:00	2450	625.589	13.85
7/12/96	0:30:00	2460	625.585	13.86
7/12/96	0:40:00	2470	625.585	13.86
7/12/96	0:50:00	2480	625.585	13.85
7/12/96	1:00:00	2490	625.585	13.86
7/12/96	1:10:00	2500	625.589	13.86
7/12/96	1:20:00	2510	625.594	13.85
7/12/96	1:30:00	2520	625.589	13.85
7/12/96	1:40:00	2530	625.589	13.86
7/12/96	1:50:00	2540	625.585	13.86
7/12/96	2:00:00	2550	625.585	13.85
7/12/96	2:10:00	2560	625.589	13.85
7/12/96	2:20:00	2570	625.589	13.86
7/12/96	2:30:00	2580	625.589	13.86
7/12/96	2:40:00	2590	625.585	13.86
7/12/96	2:50:00	2600	625.589	13.85
7/12/96	3:00:00	2610	625.589	13.86
7/12/96	3:10:00	2620	625.589	13.86
7/12/96	3:20:00	2630	625.585	13.86
7/12/96	3:30:00	2640	625.589	13.86

Date	Time	ET (min)	Feet H2O	Celsius
7/12/96	3:40:00	2650	625.585	13.86
7/12/96	3:50:00	2660	625.585	13.86
7/12/96	4:00:00	2670	625.585	13.86
7/12/96	4:10:00	2680	625.585	13.86
7/12/96	4:20:00	2690	625.585	13.86
7/12/96	4:30:00	2700	625.585	13.86
7/12/96	4:40:00	2710	625.585	13.86
7/12/96	4:50:00	2720	625.585	13.86
7/12/96	5:00:00	2730	625.585	13.87
7/12/96	5:10:00	2740	625.585	13.87
7/12/96	5:20:00	2750	625.585	13.87
7/12/96	5:30:00	2760	625.585	13.87
7/12/96	5:40:00	2770	625.585	13.87
7/12/96	5:50:00	2780	625.585	13.87
7/12/96	6:00:00	2790	625.585	13.87
7/12/96	6:10:00	2800	625.585	13.87
7/12/96	6:20:00	2810	625.58	13.87
7/12/96	6:30:00	2820	625.58	13.87
7/12/96	6:40:00	2830	625.58	13.87
7/12/96	6:50:00	2840	625.58	13.87
7/12/96	7:00:00	2850	625.58	13.88
7/12/96	7:10:00	2860	625.58	13.87
7/12/96	7:20:00	2870	625.58	13.87
7/12/96	7:30:00	2880	625.58	13.87
7/12/96	7:40:00	2890	625.58	13.87
7/12/96	7:50:00	2900	625.58	13.87
7/12/96	8:00:00	2910	625.575	13.87
7/12/96	8:10:00	2920	625.575	13.88
7/12/96	8:20:00	2930	625.575	13.87
7/12/96	8:30:00	2940	625.58	13.88
7/12/96	8:40:00	2950	625.58	13.88
7/12/96	8:50:00	2960	625.575	13.87
7/12/96	9:00:00	2970	625.575	13.88
7/12/96	9:10:00	2980	625.575	13.87
7/12/96	9:20:00	2990	625.575	13.88
7/12/96	9:30:00	3000	625.58	13.87
7/12/96	9:40:00	3010	625.575	13.87
7/12/96	9:50:00	3020	625.575	13.88
7/12/96	10:00:00	3030	625.575	13.87
7/12/96	10:10:00	3040	625.575	13.88
7/12/96	10:20:00	3050	625.575	13.88
7/12/96	10:30:00	3060	625.575	13.87
7/12/96	10:40:00	3070	625.571	13.88
7/12/96	10:50:00	3080	625.575	13.88
7/12/96	11:00:00	3090	625.571	13.88

L.E. Carpenter Aquifer Test
Wharton, New Jersey
Step Drawdown Test
Well: RW-2



CLIENT/SUBJECT _____ W.O. NO. _____

TASK DESCRIPTION EVALUATION OF STEP DRAWDOWN DATA TASK NO. _____

PREPARED BY _____ DEPT _____ DATE _____

APPROVED BY _____

MATH CHECK BY _____ DEPT _____ DATE _____

METHOD REV. BY _____ DEPT _____ DATE _____

DEPT _____ DATE _____

STEP - DRAWDOWN TEST - RW-2
DISCHARGE AND DRAWDOWN DATA
L.F. CARPENTER SITE

YIELD

DRAWDOWN

Δ DRAWDOWN

Δ DRAWDOWN/Q

15 gpm

0.808 ft

0.808 ft

0.0539

30 gpm

1.288 ft

0.480 ft

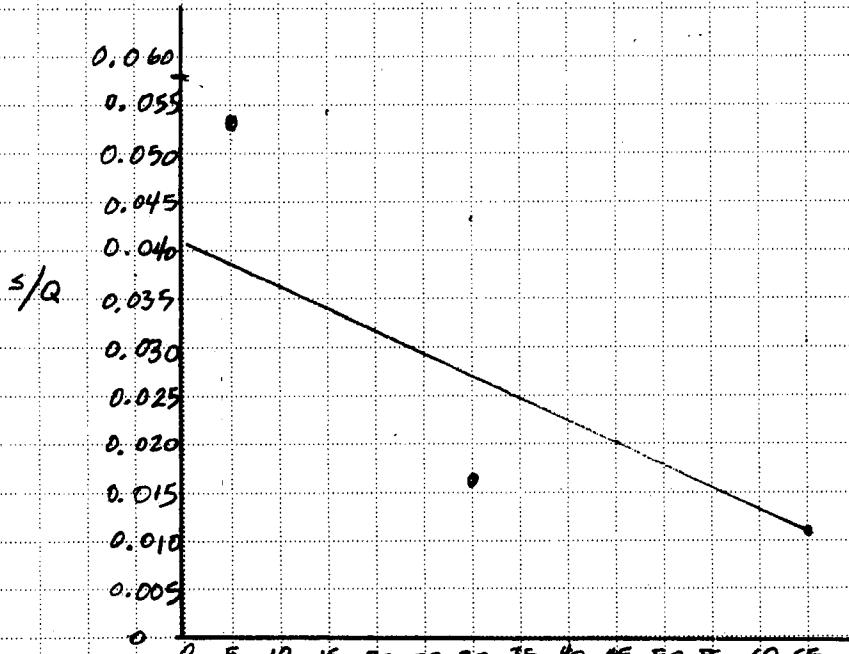
0.0160

65 gpm

1.989 ft

0.701 ft

0.0108



$$B = \frac{0.040}{\Delta Q} = \frac{0.020}{45}$$

$$= 4 \times 10^{-4}$$

Q, gpm

CLIENT/SUBJECT _____ W.O. NO. _____

TASK DESCRIPTION EVALUATION OF STEP DRAWDOWN DATA TASK NO. _____

PREPARED BY _____ DEPT _____ DATE _____

APPROVED BY _____

MATH CHECK BY _____ DEPT _____ DATE _____

METHOD REV. BY _____ DEPT _____ DATE _____

DEPT _____ DATE _____

$$\frac{Q}{S} = \frac{1}{4 \times 10^{-4} (2) - 0.040}$$

$Q = 150 \text{ gpm}$ (Pumping rate during aquifer test)

$$\frac{Q}{S} = \frac{1}{0.1}$$

$$\frac{Q}{S} = 10 \text{ gpm/ft}$$

$$L_p = \text{head loss to laminar flow} = \frac{BQ}{BQ + CQ^2} \cdot 100$$

$$= \frac{(0.040)(150)}{(0.040)(150) + 4 \times 10^{-4} (150)^2} \cdot 100$$

$$= \frac{6}{6+9} \cdot 100$$

$$= \frac{6}{15} \cdot 100 = 40\%$$

$$\frac{Q}{S} = \frac{T}{264 \log \frac{0.3 T t}{r^2 S}}$$

s = drawdown in the well, in ft

Q = well yield, in gpm

T = Transmissivity, in gpd/ft

t = time of pumping, in days, 24 hours or 0.25 days

r = radius of well, in ft, $Rw-2 = 0.33$ feet

S = Storage coefficient of the aquifer, assumed: 7.5×10^{-2}

CLIENT/SUBJECT _____ W.O. NO. _____

TASK DESCRIPTION EVALUATION OF STEP DRAWDOWN DATA TASK NO. _____

PREPARED BY _____ DEPT _____ DATE _____

APPROVED BY _____

MATH CHECK BY _____ DEPT _____ DATE _____

METHOD REV. BY _____ DEPT _____ DATE _____

DEPT _____ DATE _____

$$\frac{Q}{S} = \frac{T}{264 \log \frac{0.3Tt}{r^2 S}}$$

$$10 \text{ gpm/ft} = \frac{T}{264 \log \frac{0.3T(0.25 \text{ days})}{(0.11 \text{ ft}^2)(7.5 \times 10^{-2})}}$$

$$10 \text{ gpm} = \frac{T}{264 \log \frac{(9.036)(T)}{(8.3 \times 10^{-3})}}$$

$$10 \text{ gpm} = \frac{T}{264 \log \frac{(9.036)(30,000)}{(8.3 \times 10^{-3})}}$$

$$(10 \text{ gpm}) [264 \log (271,080)] = T$$

$$(10) [264(5.43)] = 14,335.2 \text{ gpd/ft}$$

Linear Regression to determine T.

$$\frac{T_i + T_{i+1}}{2} = T_j; \quad \frac{T_j + T_{j+1}}{2} = T_k; \dots$$

* 30,000 gpd/ft = T, Groundwater & Wells p. 1021

CLIENT/SUBJECT _____ W.O. NO. _____

TASK DESCRIPTION EVALUATION OF STEP-DRAWDOWN DATA TASK NO. _____

PREPARED BY _____ DEPT _____ DATE _____

APPROVED BY _____

MATH CHECK BY _____ DEPT _____ DATE _____

METHOD REV. BY _____ DEPT _____ DATE _____

DEPT _____ DATE _____

T_i (gpd/ft)

T_{i+1} (gpd/ft)

T_f (gpd/ft)

30,000

14,335.2

22,167.6

22,167.6

13,996.5

18,082.0

18,082.0

13,762.9

15,922.5

15,922.5

13,617.1

14,169.2

14,169.2

13,483.3

13,826.3

13,826.3

13,455.1

13,640.8

13,640.8

13,439.8

13,540.3

13,540.3

13,431.3

13,405.8

13,429.8

13,426.7

13,426.2

13,426.2

13,424.1

13,440.2

13,440.2

13,422.8

13,431.5

13,431.5

13,422.0

13,426.7

13,426.7

13,421.6

13,424.2

13,424.2

$$T = 13,421.4 \text{ gpd/ft} \\ = 19.3 \text{ cm}^2/\text{sec}$$

$$\tau = K b$$

$$T/b = K$$

$$(13,421.4 \text{ gpd/ft}) / (70 \text{ ft}) = 191.73 \text{ gpd/ft}^2 \\ 191.73 \text{ gpd/ft}^2 = 9.04 \times 10^{-3} \text{ cm/sec}$$



APPENDIX C

CONSTANT RATE PUMPING TEST DATA

TABLE 1
WATER LEVEL/PRODUCT THICKNESS MEASUREMENT DATA
PRIOR TO TEST - JULY 16, 1996
L.E. CARPENTER SITE
WHARTON, NEW JERSEY

MONITORING POINT DESIGNATION	MEASURING POINT ELEVATION (FT. MSL)	DEPTH TO PRODUCT (FT)	APPARENT PRODUCT THICKNESS (FT)	STATIC DEPTH TO WATER (FT)	CORRECTED DEPTH TO WATER (FT)	CORRECTED WATER LEVEL ELEVATION (FT MSL)
MW-1	ABANDONED	ABANDONED	ABANDONED	ABANDONED	ABANDONED	ABANDONED
MW-1(R)	NOT SURVEYED	8.52	0.93	9.45	8.81	NOT SURVEYED
MW-2	633.57	ABANDONED	ABANDONED	ABANDONED	ABANDONED	ABANDONED
MW-2(R)	NOT SURVEYED	NONE	NONE	5.97	5.97	NOT SURVEYED
MW-3	632.56	6.15	0.10	6.25	6.16	626.40
MW-4	632.50	NONE	NONE	5.94	5.94	626.56
MW-5	632.42	NONE	NONE	5.54	5.54	626.88
MW-6	632.77	ABANDONED	ABANDONED	ABANDONED	ABANDONED	ABANDONED
MW-6(R)	NOT SURVEYED	5.08	0.04	5.04	5.06	NOT SURVEYED
MW-7	630.68	NONE	NONE	4.26	4.26	626.42
MW-8	630.56	NONE	NONE	4.06	4.06	626.50
MW-9	631.69	NONE	NONE	4.55	4.55	627.14
MW-10	631.52	6.58	SHEEN	6.58	6.58	624.94
MW-11S	632.96	6.30	6.17	12.47	6.73	626.23
MW-11I	632.82	NONE	NONE	6.39	6.39	626.43
MW-11D	632.42	NONE	NONE	3.53	3.53	628.89
MW-12S	633.18	ABANDONED	ABANDONED	ABANDONED	ABANDONED	ABANDONED
MW-12I	633.06	ABANDONED	ABANDONED	ABANDONED	ABANDONED	ABANDONED
MW-12R	NOT SURVEYED	NONE	NONE	7.79	7.79	NOT SURVEYED
MW-13S	631.23	NONE	NONE	3.65	3.65	627.58
MW-13(R)	NOT SURVEYED	NONE	NONE	4.55	4.55	NOT SURVEYED
MW-13I	630.66	NONE	NONE	4.59	4.59	626.07
MW-14S	628.41	NONE	NONE	2.74	2.74	625.67
MW-14I	628.23	NONE	NONE	2.25	2.25	625.98
MW-14D	628.53	NONE	NONE	ARTESIAN	ARTESIAN	ARTESIAN
MW-15S	636.77	NONE	NONE	9.99	9.99	626.78
MW-15I	636.66	NONE	NONE	9.87	9.87	626.79
MW-16S	634.47	NONE	NONE	5.81	5.81	628.66
MW-16I	634.96	NONE	NONE	7.70	7.70	627.26
MW-17S	634.79	NONE	NONE	7.46	7.46	627.33
MW-17D	634.86	NONE	NONE	7.83	7.83	627.03
MW-18S	631.26	NONE	NONE	6.17	6.17	625.09
MW-18I	631.04	NONE	NONE	4.61	4.61	626.43
MW-18D	630.77	NONE	NONE	2.59	2.59	628.18
MW-19	638.88	NONE	NONE	11.06	11.06	627.82
MW-20	636.77	NONE	NONE	6.26	6.26	630.51
MW-21	628.80	NONE	NONE	3.21	3.21	625.59
MW-22	628.74	CASING	IS	OBSTRUCTED	CASING	#VALUE!
MW-23	630.64	NONE	NONE	2.29	2.29	628.35
MW-24	629.03	CASING	IS	OBSTRUCTED	CASING	#VALUE!
MW-25	627.33	CASING	IS	OBSTRUCTED	CASING	#VALUE!
MW-26	NOT SURVEYED	NONE	NONE	6.99	6.99	NOT SURVEYED
RW-1	637.38	10.30	0.27	10.57	10.34	627.04
RW-2	631.68	5.52	SHEEN	5.52	5.52	626.16
RW-3	631.99	NONE	NONE	5.76	5.76	626.23
CW-1	NOT SURVEYED	7.37	0.01	7.38	7.37	NOT SURVEYED

TABLE 1
 WATER LEVEL/PRODUCT THICKNESS MEASUREMENT DATA
 PRIOR TO TEST - JULY 16,1996
 L.E. CARPENTER SITE
 WHARTON, NEW JERSEY

MONITORING POINT DESIGNATION	MEASURING POINT ELEVATION (FT. MSL)	DEPTH TO PRODUCT (FT)	APPARENT PRODUCT THICKNESS (FT)	STATIC DEPTH TO WATER (FT)	CORRECTED DEPTH TO WATER (FT)	CORRECTED WATER LEVEL ELEVATION (FT MSL)
CW-2	ABANDONED	ABANDONED	ABANDONED	ABANDONED	ABANDONED	NOT SURVEYED
CW-3	NOT SURVEYED	NONE	NONE	6.63	6.63	NOT SURVEYED
GEI-1I	630.78	NONE	NONE	4.26	4.26	626.52
GEI-2S	637.67	NONE	NONE	9.96	9.96	627.71
GEI-2I	638.20	NO	ACCESS	NO	ACCESS	#VALUE!
GEI-3I	639.85	NONE	NONE	13.23	13.23	626.62
WP-A1	635.81	8.60	2.10	10.70	8.89	626.92
WP-A2	BENT CASING	CASING	IS	BENT	BENT CASING	BENT CASING
WP-A3	635.56	NONE	NONE	8.30	8.30	627.26
WP-A4	NO ACCESS	NO ACCESS	NO ACCESS	NO ACCESS	NO ACCESS	NO ACCESS
WP-A5	637.85	10.35	SHEEN	10.35	10.35	627.50
WP-A6	637.28	10.35	4.05	14.40	10.59	626.69
WP-A7	634.88	7.83	0.51	8.44	7.96	626.92
WP-A8	637.56	10.75	5.85	16.60	11.10	626.46
WP-A9	639.45	11.78	0.32	12.10	11.79	627.66
WP-B1	633.65	NONE	NONE	4.70	4.70	628.95
WP-B2	632.25	NONE	NONE	5.81	5.81	626.44
WP-B3	633.33	NONE	NONE	5.42	5.42	627.81
WP-B4	NEW STICKUP	5.95	2.44	8.39	8.17	NOT SURVEYED
WP-B5	632.11	5.83	SHEEN	5.83	5.83	626.28
WP-B6	631.86	NONE	NONE	4.40	4.40	627.46
WP-B7	629.49	3.40	0.20	3.60	3.43	626.06
WP-B8	629.29	NOT	MEASURED	NOT	MEASURED	#VALUE!
WP-B9	ABANDONED	ABANDONED	ABANDONED	ABANDONED	ABANDONED	ABANDONED
WP-B10	NEW STICKUP	NONE	NONE	6.32	6.32	NOT SURVEYED
WP-C1	NEW STICKUP	NONE	NONE	6.24	6.24	NOT SURVEYED
WP-C2	634.46	NOT	MEASURED	NOT	MEASURED	#VALUE!
WP-C3	632.64	NONE	NONE	5.45	5.45	627.19
WP-C4	NEW STICKUP	NONE	NONE	6.24	6.24	NOT SURVEYED
DC-P0	625.73	NONE	NONE	0.63	0.63	625.10
DC-P1	625.26	NONE	NONE	1.16	NO ACCESS	NO ACCESS
DC-P2	626.79	NONE	NONE	0.65	0.65	626.14
DC-P3	625.22	NONE	NONE	0.53	0.53	624.69
DC-P4	625.10	NONE	NONE	0.61	0.61	624.48
DC-P5	625.16	NO ACCESS	NO ACCESS	NO ACCESS	NO ACCESS	NO ACCESS
RP-01	629.65	NONE	NONE	2.30	2.30	627.35
RP-02	627.75	NONE	NONE	1.48	1.48	626.27
RP-03	627.11	NONE	NONE	2.04	2.04	625.07
RP-04	NOT SURVEYED	NONE	NONE	2.15	2.15	NOT SURVEYED

NOTE:

WHERE SPECIFIC GRAVITY WAS NOT BE MEASURED, ASSUME A PRODUCT SPECIFIC GRAVITY OF 0.86.

TABLE 2
WATER LEVEL/PRODUCT THICKNESS MEASUREMENT DATA
DURING TEST - JULY 16 1996
L.E. CARPENTER SITE
WHARTON, NEW JERSEY

MONITORING POINT DESIGNATION	MEASURING POINT ELEVATION (FT. MSL)	DEPTH TO PRODUCT (FT)	APPARENT PRODUCT THICKNESS (FT)	STATIC DEPTH TO WATER (FT)	CORRECTED DEPTH TO WATER (FT)	CORRECTED WATER LEVEL ELEVATION (FT MSL)
MW-1	ABANDONED	ABANDONED	ABANDONED	ABANDONED	ABANDONED	ABANDONED
MW-1(R)	NOT SURVEYED	8.87	0.69	9.56	8.94	NOT SURVEYED
MW-2	633.57	ABANDONED	ABANDONED	ABANDONED	ABANDONED	ABANDONED
MW-2(R)	NOT SURVEYED	NONE	NONE	7.12	7.12	NOT SURVEYED
MW-3	632.56	7.39	0.08	7.47	7.40	625.16
MW-4	632.50	NONE	NONE	6.46	6.46	626.04
MW-5	632.42	NONE	NONE	5.80	5.80	626.62
MW-6	632.77	ABANDONED	ABANDONED	ABANDONED	ABANDONED	ABANDONED
MW-6(R)	NOT SURVEYED	5.50	SHEEN	5.50	5.50	NOT SURVEYED
MW-7	630.68	NOT	MEASURED	NOT	#VALUE!	#VALUE!
MW-8	630.56	NONE	NONE	4.25	4.25	626.31
MW-9	631.69	NONE	NONE	4.68	4.68	627.01
MW-10	631.52	7.23	SHEEN	7.23	7.23	624.29
MW-11S	632.96	6.88	6.13	13.01	7.31	625.65
MW-11I	632.82	NONE	NONE	6.89	6.89	625.93
MW-11D	632.42	NONE	NONE	3.52	3.52	628.90
MW-12S	633.18	ABANDONED	ABANDONED	ABANDONED	ABANDONED	ABANDONED
MW-12I	633.06	ABANDONED	ABANDONED	ABANDONED	ABANDONED	ABANDONED
MW-12R	NOT SURVEYED	NONE	NONE	8.19	8.19	NOT SURVEYED
MW-13S	631.23	NONE	NONE	3.92	3.92	627.31
MW-13(R)	NOT SURVEYED	NONE	NONE	5.28	5.28	NOT SURVEYED
MW-13I	630.66	NONE	NONE	5.18	5.18	625.48
MW-14S	628.41	DATA	LOGGER	MONITORED	DATA	#VALUE!
MW-14I	628.23	DATA	LOGGER	MONITORED	DATA	#VALUE!
MW-14D	628.53	NONE	NONE	ARTESIAN	ARTESIAN	ARTESIAN
MW-15S	636.77	NONE	NONE	10.30	10.30	626.47
MW-15I	636.66	NONE	NONE	10.21	10.21	626.45
MW-16S	634.47	NONE	NONE	6.03	6.03	628.44
MW-16I	634.96	NONE	NONE	7.89	7.89	627.07
MW-17S	634.79	DATA	LOGGER	MONITORED	DATA	#VALUE!
MW-17D	634.86	NONE	NONE	8.09	8.09	626.77
MW-18S	631.26	NONE	NONE	5.33	5.33	625.93
MW-18I	631.04	NONE	NONE	4.79	4.79	626.25
MW-18D	630.77	NONE	NONE	2.55	2.55	628.22
MW-19	638.88	NONE	NONE	11.02	11.02	627.86
MW-20	636.77	NOT	MEASURED	NOT	MEASURED	#VALUE!
MW-21	628.80	NOT	MEASURED	NOT	MEASURED	#VALUE!
MW-22	626.74	CASING	IS	OBSTRUCTED	CASING	#VALUE!
MW-23	630.64	NOT	MEASURED	NOT	MEASURED	#VALUE!
MW-24	629.03	CASING	IS	OBSTRUCTED	CASING	#VALUE!
MW-25	627.33	CASING	IS	OBSTRUCTED	CASING	#VALUE!
MW-26	NOT SURVEYED	NONE	NONE	7.52	7.52	NOT SURVEYED
RW-1	637.38	10.57	0.25	10.82	10.82	626.56
RW-2	631.68	DATA	LOGGER	MONITORED	#VALUE!	#VALUE!
RW-3	631.99	NONE	NONE	3.93	3.93	628.06
CW-1	NOT SURVEYED	7.81	SHEEN	7.81	7.81	NOT SURVEYED

TABLE 2
WATER LEVEL/PRODUCT THICKNESS MEASUREMENT DATA
DURING TEST - JULY 16 1996
L.E. CARPENTER SITE
WHARTON, NEW JERSEY

MONITORING POINT DESIGNATION	MEASURING POINT ELEVATION (FT. MSL)	DEPTH TO PRODUCT (FT)	APPARENT PRODUCT THICKNESS (FT)	STATIC DEPTH TO WATER (FT)	CORRECTED DEPTH TO WATER (FT)	CORRECTED WATER LEVEL ELEVATION (FT MSL)
CW-2	ABANDONED	ABANDONED	ABANDONED	ABANDONED	ABANDONED	NOT SURVEYED
CW-3	NOT SURVEYED	NONE	NONE	7.33	7.33	NOT SURVEYED
GEI-1I	630.78	NONE	NONE	4.43	4.43	626.35
GEI-2S	637.67	NONE	NONE	9.98	9.98	627.69
GEI-2I	638.20	NOT	MEASURED	NOT	MEASURED	#VALUE!
GEI-3I	639.85	NONE	NONE	12.42	12.42	627.43
WP-A1	635.81	9.05	2.05	11.10	9.34	626.47
WP-A2	BENT CASING	CASING	IS	BENT	BENT CASING	BENT CASING
WP-A3	635.56	NONE	NONE	8.52	8.52	627.04
WP-A4	NO ACCESS	NO ACCESS	NO ACCESS	NO ACCESS	NO ACCESS	NO ACCESS
WP-A5	637.85	NONE	NONE	10.57	10.57	627.28
WP-A6	637.28	NONE	NONE	10.66	10.66	626.62
WP-A7	634.88	8.31	0.32	8.63	8.33	626.55
WP-A8	637.56	11.19	5.27	16.46	11.51	626.05
WP-A9	639.45	11.95	0.49	12.44	11.96	627.49
WP-B1	633.65	NONE	NONE	4.71	4.71	628.94
WP-B2	632.25	NONE	NONE	6.24	6.24	626.01
WP-B3	633.33	NONE	NONE	5.61	5.61	627.72
WP-B4	NEW STICKUP	6.58	2.10	8.68	6.77	NOT SURVEYED
WP-B5	632.11	6.47	SHEEN	6.47	6.47	625.64
WP-B6	631.86	NONE	NONE	4.60	4.60	627.26
WP-B7	629.49	3.69	0.23	3.92	3.72	625.77
WP-B8	629.29	NONE	NONE	2.78	2.78	626.51
WP-B9	ABANDONED	ABANDONED	ABANDONED	ABANDONED	ABANDONED	ABANDONED
WP-B10	NEW STICKUP	NONE	NONE	6.81	6.81	NOT SURVEYED
WP-C1	NEW STICKUP	NONE	NONE	6.39	6.39	NOT SURVEYED
WP-C2	634.48	NOT	MEASURED	NOT	MEASURED	#VALUE!
WP-C3	632.64	NONE	NONE	7.56	7.56	625.08
WP-C4	NEW STICKUP	NONE	NONE	8.43	8.43	NOT SURVEYED
DC-P0	625.73	NOT	MEASURED	NOT	MEASURED	#VALUE!
DC-P1	625.26	NOT	MEASURED	NOT	MEASURED	NO ACCESS
DC-P2	626.79	NOT	MEASURED	NOT	MEASURED	#VALUE!
DC-P3	625.22	DATA	LOGGER	MONITORED	DATA	#VALUE!
DC-P4	625.10	NOT	MEASURED	NOT	MEASURED	#VALUE!
DC-P5	625.16	NOT	MEASURED	NOT	MEASURED	NOT MEASURED
RP-01	629.65	NONE	NO ACCESS	2.42	2.42	627.23
RP-02	627.75	NONE	NONE	1.52	1.52	626.23
RP-03	627.11	NONE	NONE	2.14	2.64	624.47
RP-04	NOT SURVEYED	NONE	NONE	2.15	2.15	NOT SURVEYED

NOTE:

WHERE SPECIFIC GRAVITY WAS NOT BE MEASURED, ASSUME A PRODUCT SPECIFIC GRAVITY OF 0.86.

TABLE 3
RW-2 PUMPING TEST
SUMMARY OF RESULTS

MONITORING POINT DESIGNATION	DISTANCE FROM RW-2 (Feet)	METHOD OF ANALYSIS	TRANSMISSIVITY (Square Centimeters Per Second)	HYDRAULIC CONDUCTIVITY (Centimeters Per Second)	SPECIFIC YIELD OF AQUIFER	STORAGE COEFFICIENT OF AQUIFER
RW-2	0	Theis	55.61	2.61E-02		1.28E-01
MW-3	22.56	Theis Neuman - Partially Penetrating Cooper - Jacob	77.23 175.89 88.83	3.62E-02 8.24E-02 4.16E-02	1.68E-02	1.90E-02 4.63E-02 1.45E-02
MW-14S	134.2	Theis Neuman - Partially Penetrating	199.9 330.3	9.37E-02 1.55E-01	7.58E-03	1.36E-03 2.32E-03
MW-14I	119.8	Theis Neuman - Partially Penetrating Cooper - Jacob	175.20 137.4 185.8	8.21E-02 6.44E-02 8.71E-02	2.41E-03	1.08E-03 1.34E-03 8.65E-04
GEOMETRIC MEAN			139.35	6.53E-02	6.72E-03	4.50E-03
ARITHMETIC MEAN			158.46	7.43E-02	8.88E-03	2.67E-02

Note:

For calculation of hydraulic conductivity, assume an aquifer thickness of 70 feet.

TABLE 4
CHANGE IN WATER LEVELS DURING THE
CONSTANT RATE AQUIFER TEST - JULY 16, 1996
L.E. CARPENTER SITE
WHARTON, NEW JERSEY

MONITORING POINT DESIGNATION	CHANGE IN WATER LEVEL (FEET)
MW-1(R)	-0.33
MW-2(R)	-1.09
MW-3	-1.22
MW-4	-0.52
MW-5	-0.26
MW-6(R)	-0.31
MW-8	-0.62
MW-9	-0.13
MW-10	-0.65
MW-11S	-0.58
MW-11I	-0.50
MW-11D	-0.01
MW-12R	-0.40
MW-13S	-0.27
MW-13(R)	-0.73
MW-13I	-0.59
MW-14S	-0.55
MW-14I	-0.66
MW-15S	-0.31
MW-15I	-0.34
MW-16S	-0.22
MW-16I	-0.19
MW-17D	-0.26
MW-18S	+0.84
MW-18I	-0.18
MW-18D	+0.04
MW-19	+0.04
MW-26	-0.53
RW-1	-0.46
RW-2	-3.44
RW-3	+1.83
CW-1	-0.44
CW-3	-0.70
GEI-11	-0.17
GEI-2S	-0.02
GEI-3I	+0.81
WP-A1	-0.45
WP-A3	-0.22
WP-A5	-0.22
WP-A6	-0.07
WP-A7	-0.37
WP-A8	-0.41
WP-A9	-0.17
WP-B1	-0.01
WP-B2	-0.43
WP-B3	-0.19
WP-B4	-0.60
WP-B5	-0.64
WP-B6	-0.20
WP-B7	-0.29
WP-B10	-0.49
WP-C1	-0.15
WP-C3	-2.11
WP-C4	-2.19
RP-01	-0.12
RP-02	-0.04
RP-03	-0.60
RP-04	0

NOTES:

+ Denotes an increase in corrected water level elevation.

- Denotes a decrease in corrected water level elevation.

Change in water level (feet) denotes difference of corrected water level during the test to corrected water level prior to test.

SHEET 1 of 1

CLIENT/SUBJECT _____ W.O. NO. _____

TASK DESCRIPTION PRODUCT THICKNESS TASK NO. _____

PREPARED BY _____ DEPT _____ DATE _____

APPROVED BY _____

MATH CHECK BY _____ DEPT _____ DATE _____

METHOD REV. BY _____ DEPT _____ DATE _____

DEPT _____ DATE _____

Apparent Product Thickness = RW-2, July 16, 1996

<u>TIME</u>	<u>DEPTH TO PRODUCT</u>	<u>DEPTH TO WATER</u>	<u>PRODUCT THICKNESS</u>
0759	5.52 ft	5.52 ft	0.00 ft
1243	-	9.57 ft *	0.00 ft
1325	-	10.00 ft *	0.00 ft
1352	-	10.00 ft *	0.00 ft
1454	-	10.01 ft *	0.00 ft
1528	-	10.02 ft *	0.00 ft
1629	-	10.05 ft *	0.00 ft
July 17, 1996			
1210	-	9.69	0.00ft
July 18, 1996			
0918	-	5.74	0.00ft

NOTE:

1240: Pump on.

* Measurements beginning at 1243 to conclusion of test were collected from a temporary dmp-line.

SHEET 1 of 1

CLIENT/SUBJECT _____ W.O. NO. _____

TASK DESCRIPTION Product Thickness TASK NO. _____

PREPARED BY _____ DEPT _____ DATE _____

APPROVED BY _____

MATH CHECK BY _____ DEPT _____ DATE _____

METHOD REV. BY _____ DEPT _____ DATE _____

DEPT _____ DATE _____

Apparent Product Thickness: MW-3, July 16, 1996

<u>TIME</u>	<u>DEPTH TO PRODUCT</u>	<u>DEPTH TO WATER</u>	<u>PRODUCT THICKNESS</u>
0757	6.15 ft	6.25 ft	0.10 ft
1242	6.52 ft	6.59 ft	0.07 ft
1323	7.15 ft	7.25 ft	0.10 ft
1350	7.23 ft	7.30 ft	0.07 ft
1501	7.33 ft	7.40 ft	0.07 ft
1528	7.34 ft	7.42 ft	0.08 ft
1634	7.39 ft	7.47 ft	0.08 ft
July 17, 1996			
1130	6.31	6.34	0.03 ft
July 18, 1996			
0747	6.37	6.43	0.06 ft

NOTE:

1240: Pump on.

A Q T E S O L V R E S U L T S
Version 2.01

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08/30/96

12:27:31

TEST DESCRIPTION

Data set..... PRW-2.DAT
Output file..... PRW-2.OUT

Units of Measurement

Length..... ft
Time..... min
Pumping rate.... gal/min .

Pumping Well Data

Well No. 1	
Well identification.....	RW-2
X location.....	227.1
Y location.....	336.6
Casing radius.....	0.3333
Wellbore radius.....	0.5
Depth to top of well screen.....	3
Depth to bottom of well screen...	30
Number of pumping periods.....	1
Period	Pumping Rate

150

Observation Well/Piezometer Data

Well identification.....	RW-2
X location.....	227.1
Y location.....	336.6
Distance from pumping well #1....	0
Well penetration.....	Full
No. of observations.....	171

Aquifer Data

Saturated thickness..... 70

ANALYTICAL METHOD

Theis (Unconfined Aquifer)

RESULTS FROM VISUAL CURVE MATCHING

VISUAL MATCH PARAMETER ESTIMATES

Estimate
T = 5.5607E+001 cm²/sec

S = 1.2769E-001

10.

DATA SET:
PRM-2.DAT

08/30/96

AQUIFER MODEL:
Unconfined

SOLUTION METHOD:
Theis

TEST DATA:

$Q = 150 \text{ gal/min}$

$r = 0 \text{ ft}$

$r_c = 0.3333 \text{ ft}$

$r_u = 0.5 \text{ ft}$

$b = 70 \text{ ft}$

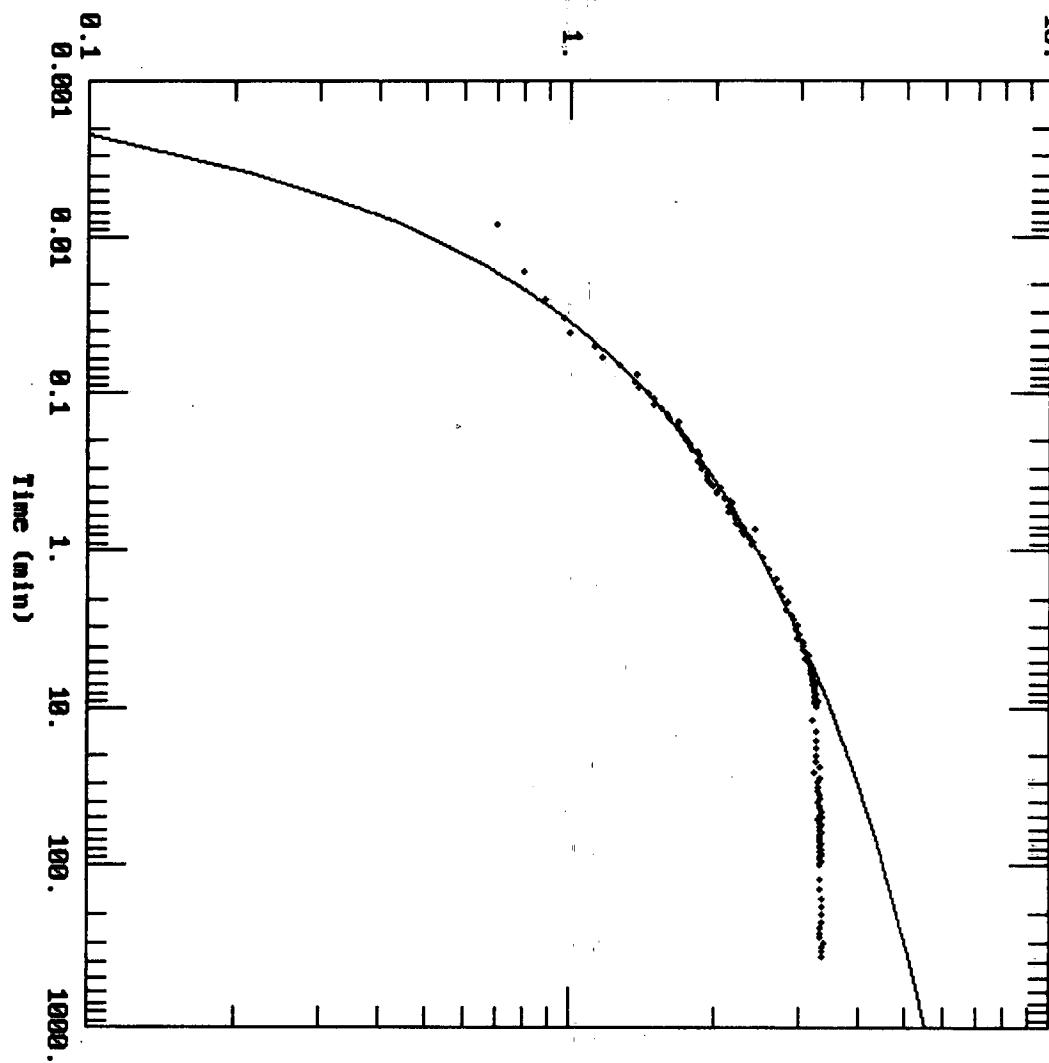
PARAMETER ESTIMATES:

$T = 55.61 \text{ cm}^2/\text{sec}$

$S = 0.1277$

Corrected Drawdown (ft)

1.



A Q T E S O L V R E S U L T S
Version 2.01

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08/30/96

10:29:24

TEST DESCRIPTION

Data set..... PMW-3.DAT
Output file..... PMW-3.OUT

Units of Measurement

Length..... ft
Time..... min
Pumping rate.... gal/min

Jumping Well Data

Well No. 1	
Well identification.....	RW-2
X location.....	227.1
Y location.....	336.6
Depth to top of well screen.....	3
Depth to bottom of well screen...	30
Number of pumping periods.....	1
Period Pumping Rate	-----
1	150

Well No. 2	
X location.....	0
Y location.....	0
Well penetration.....	Full
Number of pumping periods.....	1
Period	Pumping Rate
-----	-----

Observation Well/Piezometer Data

Well identification.....	MW-3
X location.....	216.2
Y location.....	356.4
Distance from pumping well #1....	22.56
Well penetration.....	Full
No. of observations.....	171

Aquifer Data

Saturated thickness..... 70

ANALYTICAL METHOD

Theis (Unconfined Aquifer)

RESULTS FROM VISUAL CURVE MATCHING

VISUAL MATCH PARAMETER ESTIMATES

Estimate
T = 7.7234E+001 cm²/sec
S = 1.8997E-002

A Q T E S O L V R E S U L T S Version 2.01

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08/30/96

12:03:26

TEST DESCRIPTION

Data set..... PMW-3.DAT
Output file..... PMW-3.OUT

Units of Measurement

Length..... ft
Time..... min
Pumping rate.... gal/min

Pumping Well Data

Well No. 1
Well identification..... RW-2
X location..... 227.1
Y location..... 336.6
Casing radius..... 0.3333
Wellbore radius..... 0.5
Depth to top of well screen..... 3
Depth to bottom of well screen... 30
Number of pumping periods..... 1
Period Pumping Rate

1 150

Observation Well/Piezometer Data

Well identification..... MW-3
X location..... 216.2
Y location..... 356.4
Distance from pumping well #1.... 22.56
Depth to top of well screen..... 1.5
Depth to bottom of well screen... 27
No. of observations..... 171

Aquifer Data

Saturated thickness..... 70

ANALYTICAL METHOD

Neuman (Unconfined Aquifer)
Partially Penetrating Well(s)

RESULTS FROM VISUAL CURVE MATCHING

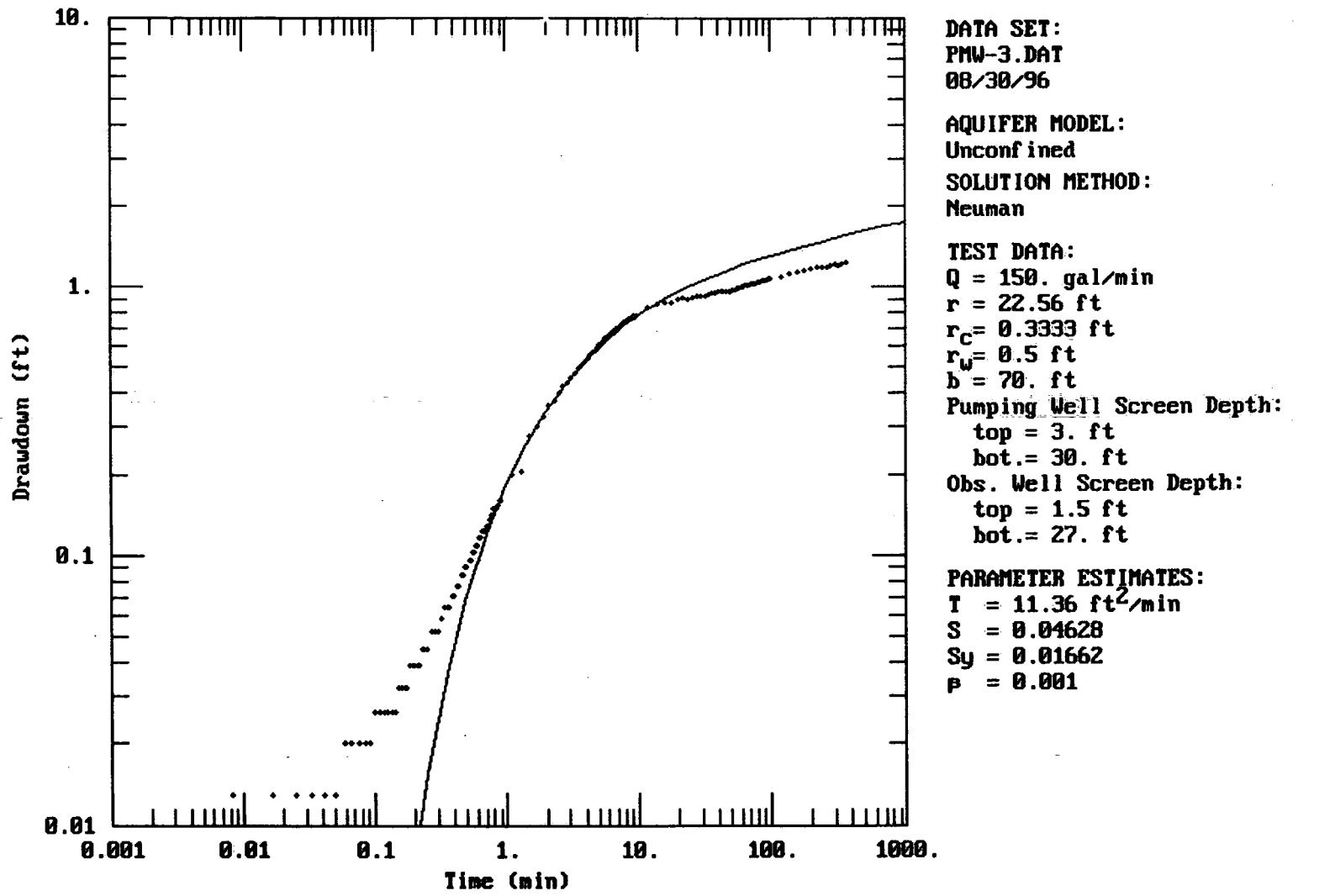
VISUAL MATCH PARAMETER ESTIMATES

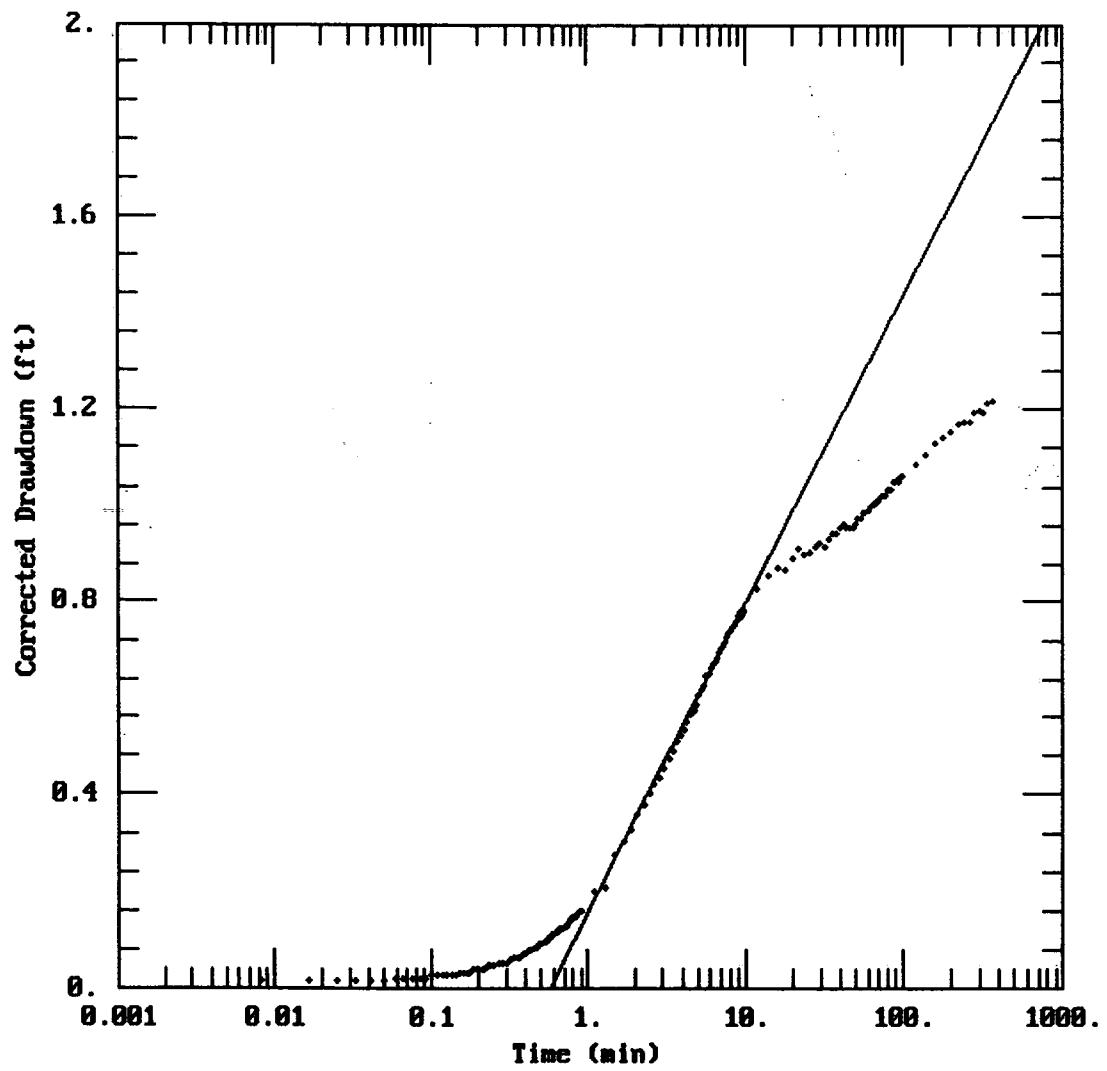
Estimate

T = 1.5245E+002 cm²/sec
S = 6.1163E-003
Sy = 1.0000E-001
B = 1.0000E-001

Derived Parameters

Kr = 2.178 cm/sec
Kz/Kr = 0.9629



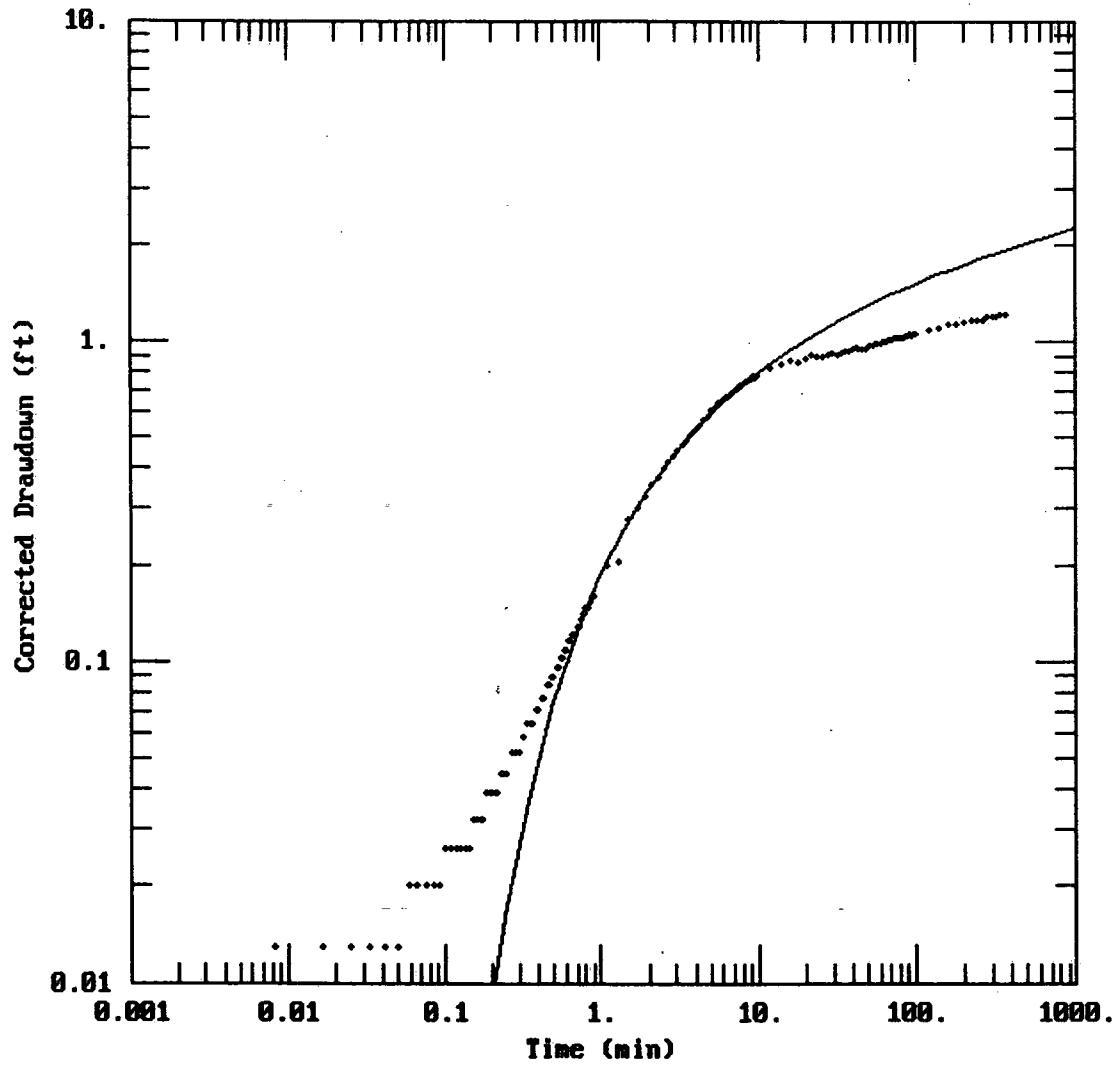


DATA SET:
PMW-3.DAT
08/30/96

AQUIFER MODEL:
Unconfined
SOLUTION METHOD:
Cooper-Jacob

TEST DATA:
 $Q = 150.$ gal/min
 $r = 22.56$ ft
 $r_c = 0.3333$ ft
 $r_w = 0.5$ ft
 $b = 70.$ ft

PARAMETER ESTIMATES:
 $T = 88.83 \text{ cm}^2/\text{sec}$
 $S = 0.01447$



DATA SET:
PMU-3.DAT
08/30/96

AQUIFER MODEL:
Unconfined
SOLUTION METHOD:
Theis

TEST DATA:
 $Q = 150.$ gal/min
 $r = 22.56$ ft
 $r_c = 0.3333$ ft
 $r_w = 0.5$ ft
 $b = 70.$ ft

PARAMETER ESTIMATES:
 $T = 77.23 \text{ cm}^2/\text{sec}$
 $S = 0.019$

A Q T E S O L V R E S U L T S
Version 2.01

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08/30/96

12:12:17

TEST DESCRIPTION

Data set..... PMW-14S.DAT
Output file..... PMW-14S.OUT

Units of Measurement

Length..... ft
Time..... min
Pumping rate.... gal/min

Pumping Well Data

Well No. 1	
Well identification.....	RW-2
X location.....	227.1
Y location.....	336.6
Casing radius.....	0.3333
Wellbore radius.....	0.5
Depth to top of well screen.....	3
Depth to bottom of well screen...	30
Number of pumping periods.....	1
Period Pumping Rate	

150

Observation Well/Piezometer Data

Well identification.....	MW-14s
X location.....	294.9
Y location.....	452.4
Distance from pumping well #1....	134.2
Well penetration.....	Full
No. of observations.....	165

Aquifer Data

Saturated thickness..... 70

ANALYTICAL METHOD

Theis (Unconfined Aquifer)

RESULTS FROM VISUAL CURVE MATCHING

VISUAL MATCH PARAMETER ESTIMATES

Estimate

T = 1.9994E+002 cm⁻²/sec

S = 1.3575E-003

A Q T E S O L V R E S U L T S
Version 2.01

(c) Developed by Glenn M. Duffield
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08/30/96

12:15:22

TEST DESCRIPTION

Data set..... PMW-14S.DAT
Output file..... PMW-14S.OUT

Units of Measurement

Length..... ft
Time..... min
Pumping rate.... gal/min

Pumping Well Data

Well No. 1	
Well identification.....	RW-2
X location.....	227.1
Y location.....	336.6
Casing radius.....	0.3333
Wellbore radius.....	0.5
Depth to top of well screen.....	3
Depth to bottom of well screen...	30
Number of pumping periods.....	1
Period	Pumping Rate
-----	-----
1	150

Observation Well/Piezometer Data

Well identification.....	MW-14s
X location.....	294.9
Y location.....	452.4
Distance from pumping well #1....	134.2
Depth to top of well screen.....	0.79
Depth to bottom of well screen...	10.83
No. of observations.....	165

Aquifer Data

Saturated thickness..... 70

ANALYTICAL METHOD

**Neuman (Unconfined Aquifer)
Partially Penetrating Well(s)**

RESULTS FROM VISUAL CURVE MATCHING

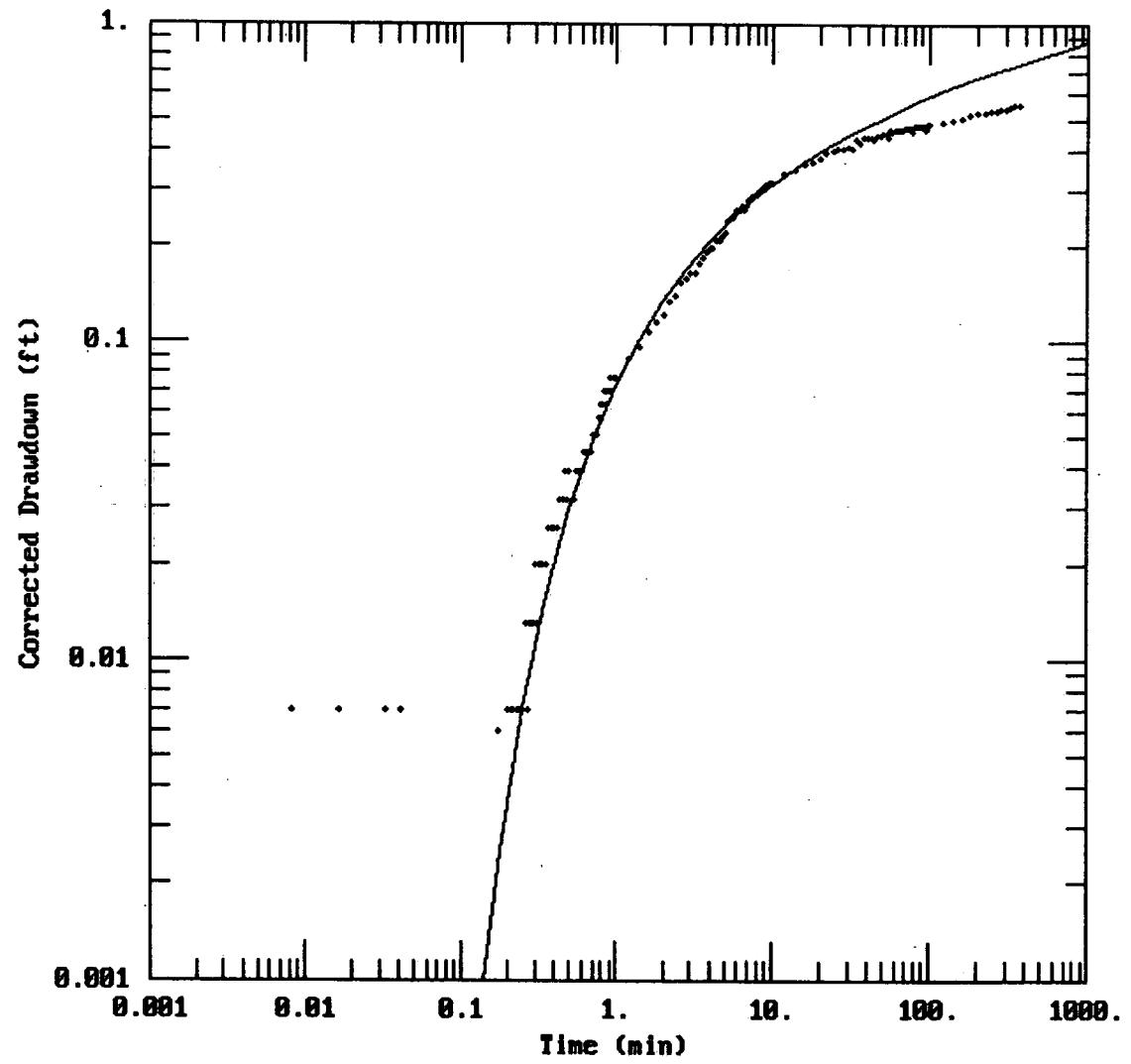
VISUAL MATCH PARAMETER ESTIMATES

Estimate

T = 3.3026E+002 cm²/sec
 S = 2.3162E-003
 Sy = 7.5803E-003
 B = 1.0000E-003

Derived Parameters

$$\text{Kz/Kr} = 0.0002722$$

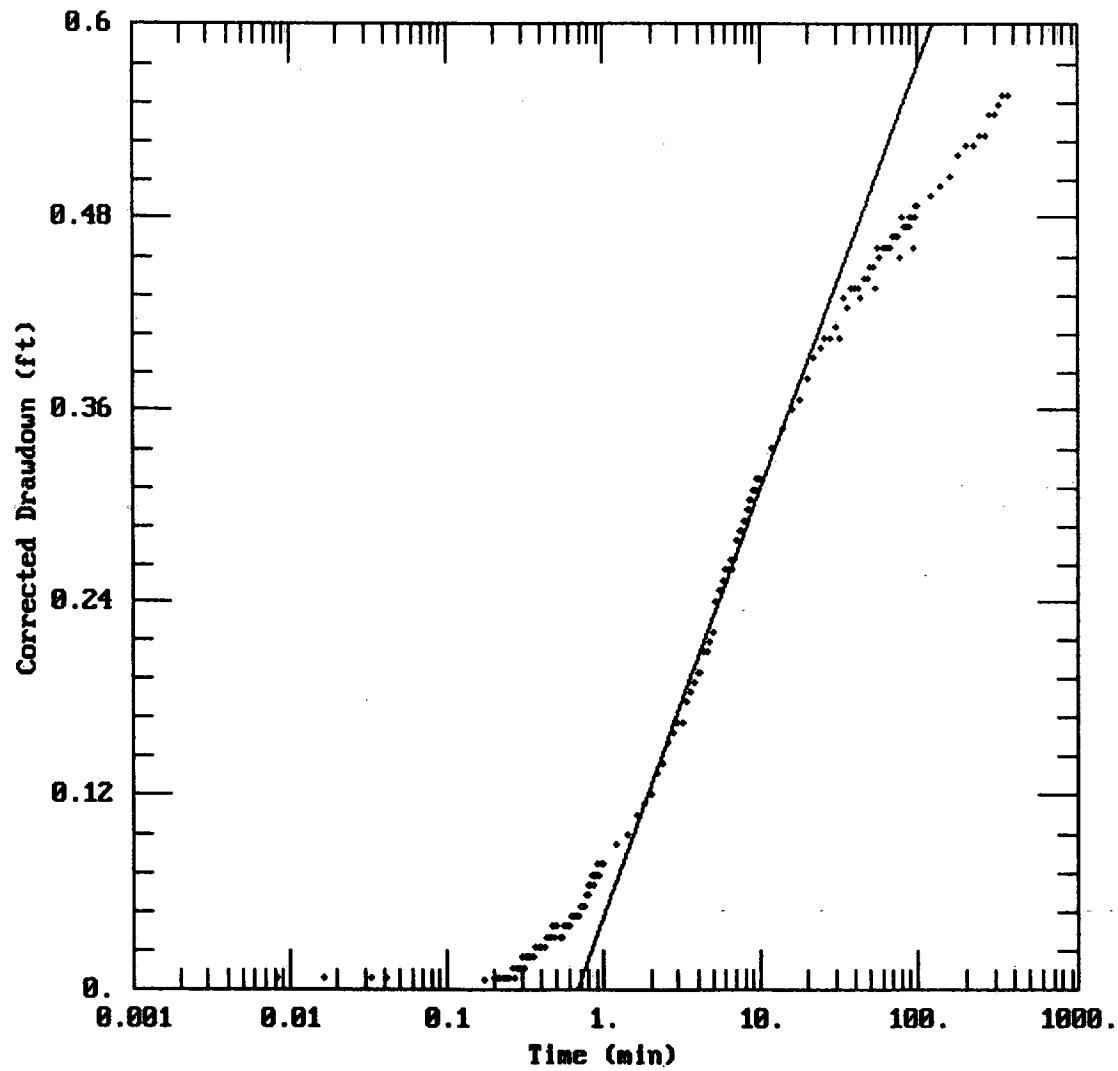


DATA SET:
PMW-14S.DAT
08/30/96

AQUIFER MODEL:
Unconfined
SOLUTION METHOD:
Theis

TEST DATA:
 $Q = 150.$ gal/min
 $r = 134.2$ ft
 $r_c = 0.3333$ ft
 $r_w = 0.5$ ft
 $b = 70.$ ft

PARAMETER ESTIMATES:
 $T = 199.9 \text{ cm}^2/\text{sec}$
 $S = 0.001358$

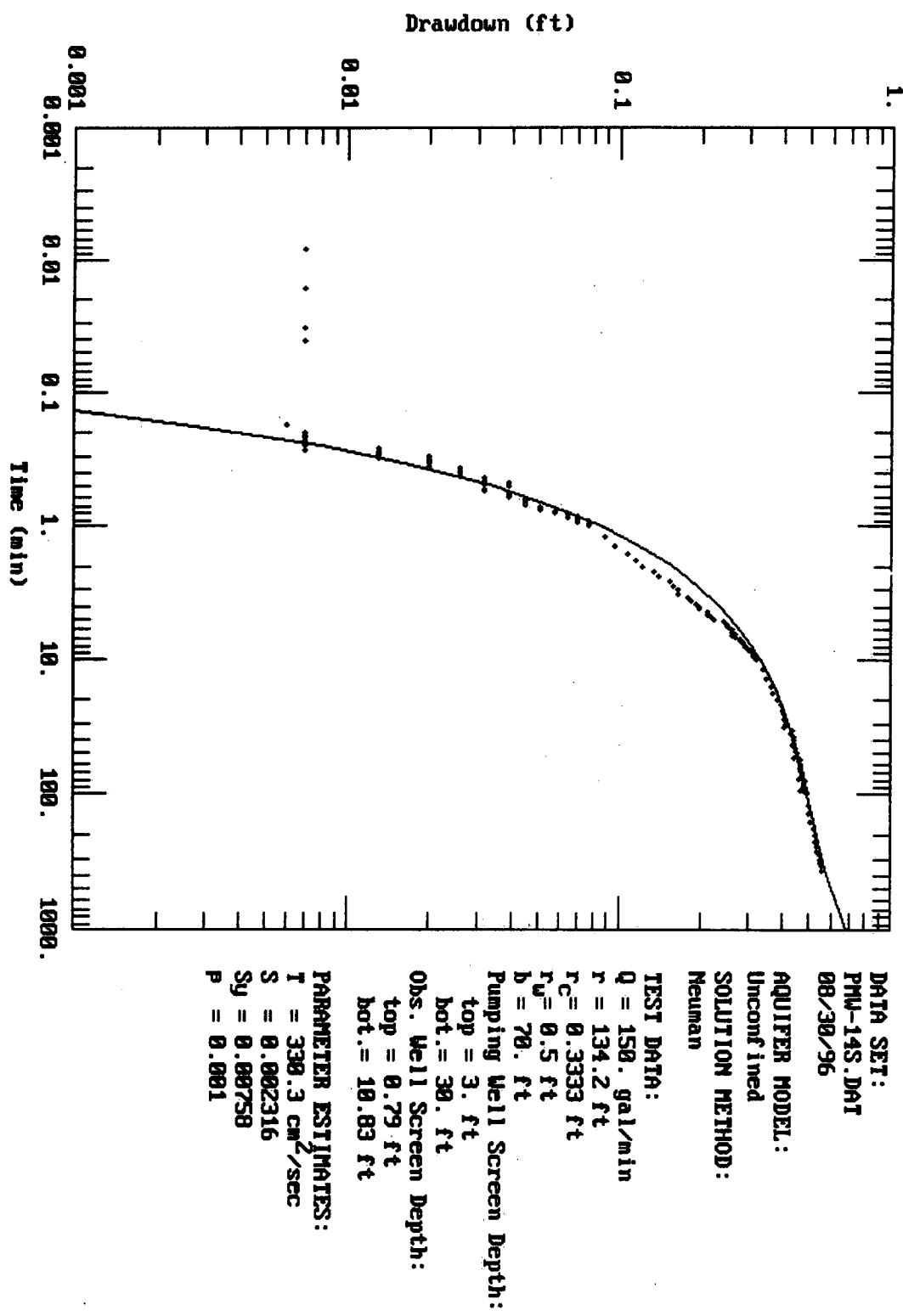


DATA SET:
PMW-14S.DAT
08/30/96

AQUIFER MODEL:
Unconfined
SOLUTION METHOD:
Cooper-Jacob

TEST DATA:
 $Q = 150.$ gal/min
 $r = 134.2$ ft
 $r_c = 0.3333$ ft
 $r_w = 0.5$ ft
 $b = 70.$ ft

PARAMETER ESTIMATES:
 $T = 214.3 \text{ cm}^2/\text{sec}$
 $S = 0.001173$



A Q T E S O L V R E S U L T S
Version 2.01

(c) Developed by Glenn M. Duffield
1988-1995 Geraghty & Miller, Inc.

8/30/96

12:07:52

TEST DESCRIPTION

Data set..... PMW-14I.DAT
Output file..... PMW-14I.OUT

Units of Measurement

Length..... ft
Time..... min
Pumping rate.... gal/min

Pumping Well Data

Well No. 1	
Well identification.....	RW-2
X location.....	227.1
Y location.....	336.6
Casing radius.....	0.3333
Wellbore radius.....	0.5
Depth to top of well screen.....	3
Depth to bottom of well screen...	30
Number of pumping periods.....	1
Period Pumping Rate	

1 150

Observation Well/Piezometer Data

Well identification.....	MW-14i
X location.....	284.3
Y location.....	441.9
Distance from pumping well #1....	119.8
Well penetration.....	Full
No. of observations.....	183

Aquifer Data

Saturated thickness..... 70

ANALYTICAL METHOD

heis (Unconfined Aquifer)

RESULTS FROM VISUAL CURVE MATCHING

VISUAL MATCH PARAMETER ESTIMATES

Estimate
T = 1.7520E+002 cm²/sec

S = 1.0787E-003

A Q T E S O L V R E S U L T S
Version 2.01

(c) Developed by Glenn M. Duffield
1988-1995 Geraghty & Miller, Inc.

08/30/96

12:10:30

TEST DESCRIPTION

Data set..... PMW-14I.DAT
Output file..... PMW-14I.OUT

Units of Measurement

Length..... ft
Time..... min
Pumping rate.... gal/min

Pumping Well Data

Well No. 1	
Well identification..... RW-2	
X location.....	227.1
Y location.....	336.6
Casing radius.....	0.3333
Wellbore radius.....	0.5
Depth to top of well screen.....	3
Depth to bottom of well screen...	30
Number of pumping periods.....	1
Period	Pumping Rate
-----	-----
1	150

Observation Well/Piezometer Data

Well identification.....	MW-14i
X location.....	284.3
Y location.....	441.9
Distance from pumping well #1....	119.8
Depth to top of well screen.....	30.92
Depth to bottom of well screen...	40.96
No. of observations.....	183

Aquifer Data

Saturated thickness..... 70

ANALYTICAL METHOD

Neuman (Unconfined Aquifer) Partially Penetrating Well(s)

RESULTS FROM VISUAL CURVE MATCHING

VISUAL MATCH PARAMETER ESTIMATES

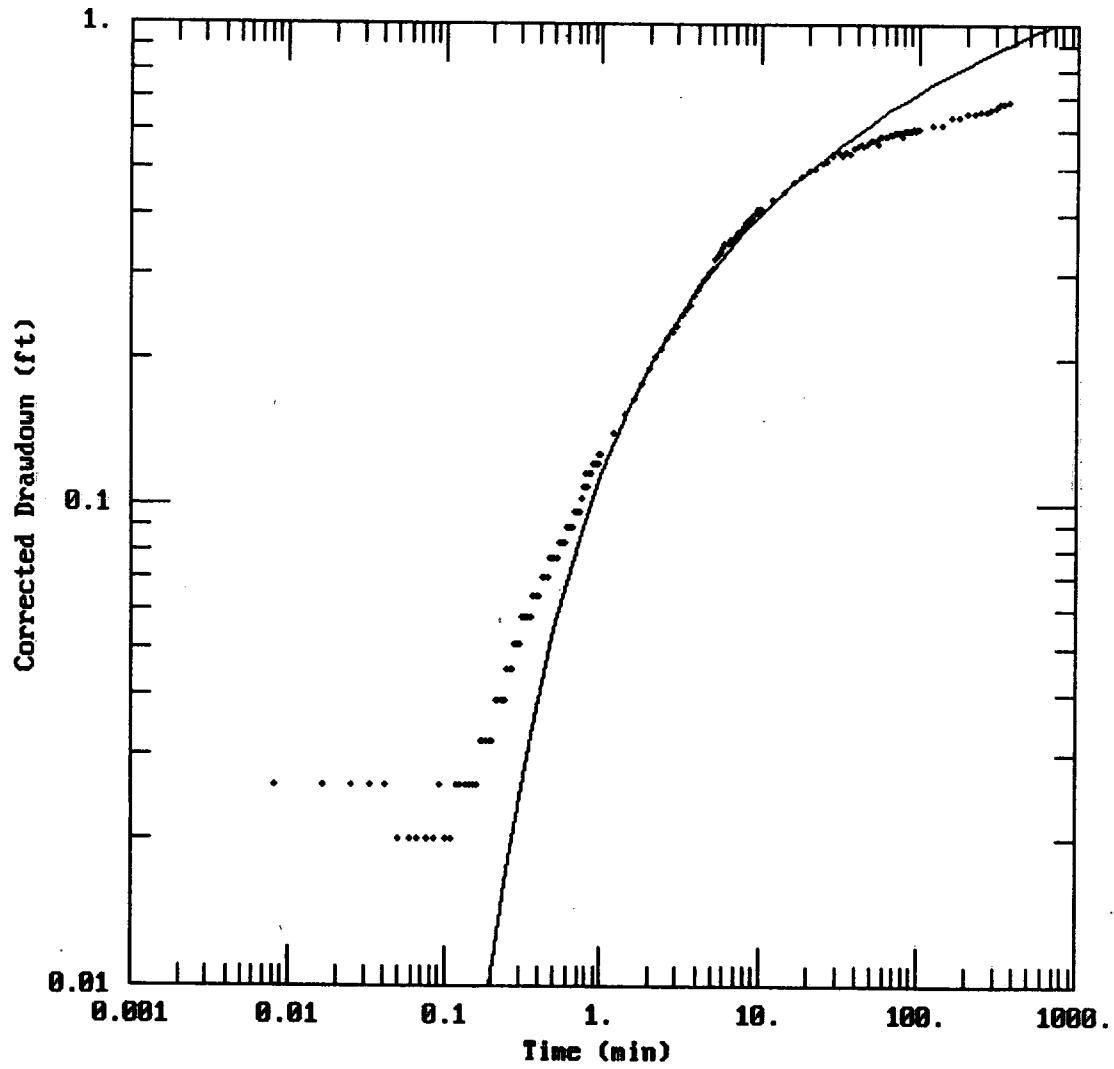
Estimate

T = 1.3743E+002 cm²/sec
 S = 1.3410E-004
 Sy = 2.4057E-003
 B = 1.0000E-003

Derived Parameters

$$K_r = 1.963 \quad \text{cm/sec}$$

~~~~~

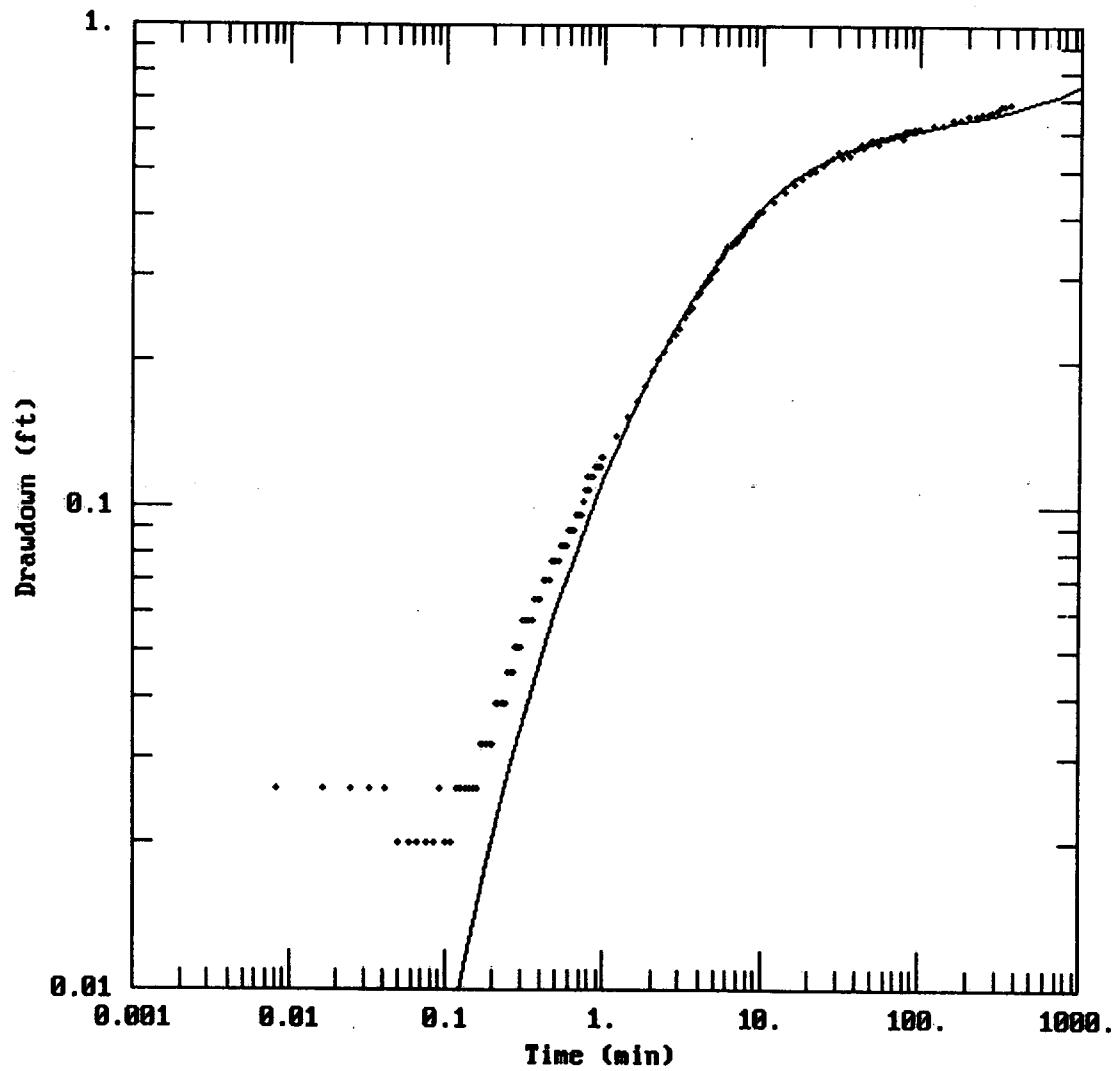


DATA SET:  
PMU-141.DAT  
08/30/96

AQUIFER MODEL:  
Unconfined  
SOLUTION METHOD:  
Theis

TEST DATA:  
 $Q = 150.$  gal/min  
 $r = 119.8$  ft  
 $r_c = 0.3333$  ft  
 $r_w = 0.5$  ft  
 $b = 70.$  ft

PARAMETER ESTIMATES:  
 $T = 175.2 \text{ cm}^2/\text{sec}$   
 $S = 0.001079$



DATA SET:  
PMW-14I.DAT  
08/30/96

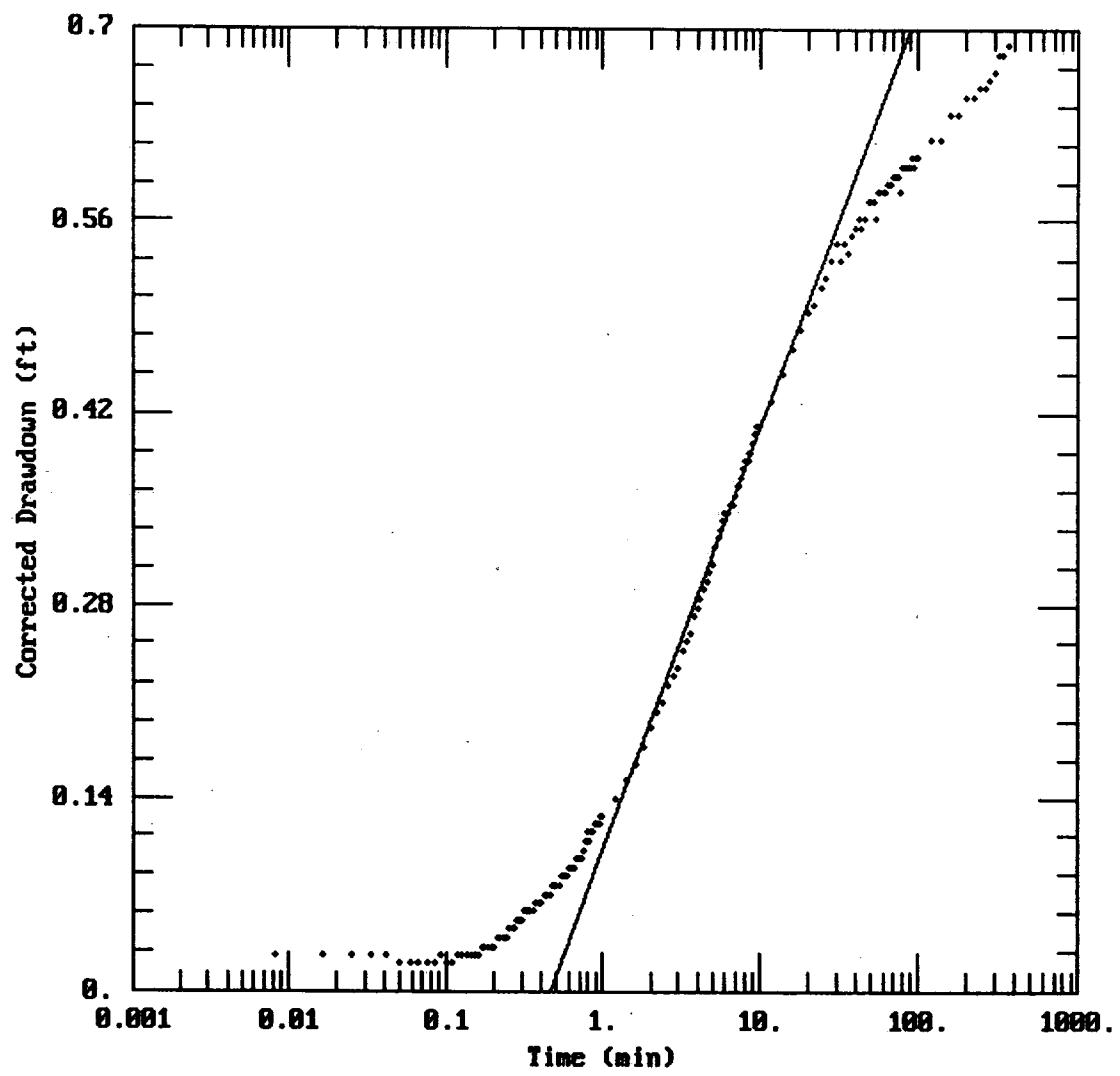
AQUIFER MODEL:  
Unconfined  
SOLUTION METHOD:  
Neuman

TEST DATA:  
 $Q = 150.$  gal/min  
 $r = 119.8$  ft  
 $r_c = 0.3333$  ft  
 $r_w = 0.5$  ft  
 $b = 70.$  ft

Pumping Well Screen Depth:  
top = 3. ft  
bot. = 30. ft

Obs. Well Screen Depth:  
top = 30.92 ft  
bot. = 40.96 ft

PARAMETER ESTIMATES:  
 $T = 137.4 \text{ cm}^2/\text{sec}$   
 $S = 0.0001341$   
 $S_y = 0.002406$   
 $P = 0.001$



DATA SET:  
PMW-14I.DAT  
08/30/96

AQUIFER MODEL:  
Unconfined  
SOLUTION METHOD:  
Cooper-Jacob

TEST DATA:  
 $Q = 150.$  gal/min  
 $r = 119.8$  ft  
 $r_c = 0.3333$  ft  
 $r_w = 0.5$  ft  
 $b = 70.$  ft

PARAMETER ESTIMATES:  
 $T = 185.8 \text{ cm}^2/\text{sec}$   
 $S = 0.0008648$

|                        |                       |                       |
|------------------------|-----------------------|-----------------------|
| CLIENT/SUBJECT _____   | W.O. NO. _____        |                       |
| TASK DESCRIPTION _____ | TASK NO. _____        |                       |
| PREPARED BY _____      | DEPT _____ DATE _____ | APPROVED BY _____     |
| MATH CHECK BY _____    | DEPT _____ DATE _____ |                       |
| METHOD REV. BY _____   | DEPT _____ DATE _____ | DEPT _____ DATE _____ |

**CALCULATION OF THE RADIUS OF THE CONE OF DEPRESSION:**

Source: Groundwater and Wells, Second Edition, p. 213 and 214

$$Q = \frac{K (H^2 - h^2)}{1,055 \log R/r}$$

where:  $Q$  = pumping rate in gpm (150 gpm)

$K$  = hydraulic conductivity, in  
gpd/ft<sup>2</sup> (1575.46)

$H$  = static head measured  
from bottom of aquifer,  
in ft (assume 70 ft)

$h$  = depth of water in the  
well while pumping, in  
ft (assume full penetration  
 $70 - 3.44 = 66.56$  ft)

$R$  = radius of the cone of  
depression, in ft

$r$  = radius of the well, in  
ft: (0.33 ft)

$$150 \text{ gpm} = \frac{(1575.46)(70^2 - 66.56^2)}{1,055 \log R/0.33}$$

$$1,055 \log R/0.33$$

$$(150)(1,055 \log R/0.33) = (1,575.46)(4,900 - 4,430.2)$$

$$(1,055 \log R/0.33) = \frac{(1,575.46)(469.8)}{150}$$

$$(1,055)(\log R/0.33) = 4,934.34$$

\* Arithmetic Mean of  $K$  determined during the pumping test.



SHEET \_\_\_\_ of \_\_\_\_

CLIENT/SUBJECT \_\_\_\_\_ W.O. NO. \_\_\_\_\_

TASK DESCRIPTION \_\_\_\_\_ TASK NO. \_\_\_\_\_

PREPARED BY \_\_\_\_\_ DEPT \_\_\_\_\_ DATE \_\_\_\_\_

APPROVED BY \_\_\_\_\_

MATH CHECK BY \_\_\_\_\_ DEPT \_\_\_\_\_ DATE \_\_\_\_\_

METHOD REV. BY \_\_\_\_\_ DEPT \_\_\_\_\_ DATE \_\_\_\_\_

DEPT \_\_\_\_\_ DATE \_\_\_\_\_

$$(\log R / 10.33) = 4.68$$

$$\log R = 1.34$$

$R = 34.67 \text{ ft} \therefore$  radius of the cone of depression.

| Elapsed Time | INPUT 1 |        | INPUT 2 |        | INPUT 3 |        | INPUT 4 |        | INPUT 5 |        | INPUT 6 |  | INPUT 7 |        | INPUT 8 |        |
|--------------|---------|--------|---------|--------|---------|--------|---------|--------|---------|--------|---------|--|---------|--------|---------|--------|
|              | RW-2    |        | MW-3    |        | 14S     |        | 14I     |        | DC-P3   |        | ATM     |  | MW-2R   |        | MW-6R   |        |
| 0            | 626.166 | 0.008  | 626.297 | -0.013 | 625.623 | -0.007 | 625.924 | -0.026 | 624.583 | -0.007 | 14.454  |  | 99.987  | -0.013 | 99.988  | -0.032 |
| 0.0083       | 626.172 | 0.012  | 626.297 | -0.013 | 625.623 | -0.007 | 625.924 | -0.026 | 624.583 | -0.007 | 14.453  |  | 99.987  | -0.013 | 99.988  | -0.032 |
| 0.0166       | 626.172 | 0.012  | 626.297 | -0.013 | 625.623 | -0.007 | 625.924 | -0.026 | 624.59  | 0      | 14.453  |  | 99.983  | -0.007 | 99.988  | -0.032 |
| 0.025        | 626.172 | 0.012  | 626.297 | -0.013 | 625.63  | 0      | 625.924 | -0.026 | 624.59  | 0      | 14.453  |  | 99.983  | -0.007 | 99.988  | -0.032 |
| 0.0333       | 626.166 | 0.008  | 626.297 | -0.013 | 625.623 | -0.007 | 625.924 | -0.026 | 624.583 | -0.007 | 14.453  |  | 99.987  | -0.013 | 99.974  | -0.026 |
| 0.0416       | 626.172 | 0.012  | 626.297 | -0.013 | 625.623 | -0.007 | 625.924 | -0.026 | 624.583 | -0.007 | 14.453  |  | 99.987  | -0.013 | 99.974  | -0.026 |
| 0.05         | 626.172 | 0.012  | 626.297 | -0.013 | 625.63  | 0      | 625.93  | -0.02  | 624.59  | 0      | 14.452  |  | 99.993  | -0.007 | 99.974  | -0.026 |
| 0.0583       | 626.172 | 0.012  | 626.297 | -0.013 | 625.63  | 0      | 625.93  | -0.02  | 624.59  | 0      | 14.453  |  | 99.993  | -0.007 | 99.974  | -0.026 |
| 0.0666       | 626.172 | 0.012  | 626.297 | -0.013 | 625.63  | 0      | 625.93  | -0.02  | 624.59  | 0      | 14.452  |  | 99.993  | -0.007 | 99.974  | -0.026 |
| 0.075        | 623.167 | -2.993 | 626.297 | -0.013 | 625.63  | 0      | 625.93  | -0.02  | 624.59  | 0      | 14.452  |  | 99.993  | -0.007 | 99.974  | -0.026 |
| 0.0833       | 628.232 | 2.072  | 626.303 | -0.007 | 625.63  | 0      | 625.93  | -0.02  | 624.583 | -0.007 | 14.452  |  | 99.987  | -0.013 | 99.974  | -0.026 |
| 0.0916       | 625.629 | -0.531 | 626.297 | -0.013 | 625.63  | 0      | 625.924 | -0.026 | 624.59  | 0      | 14.452  |  | 99.993  | -0.007 | 99.974  | -0.026 |
| 0.1          | 625.842 | -0.518 | 626.297 | -0.013 | 625.63  | 0      | 625.93  | -0.02  | 624.59  | 0      | 14.452  |  | 99.981  | -0.019 | 99.974  | -0.026 |
| 0.1083       | 625.458 | -0.702 | 626.297 | -0.013 | 625.63  | 0      | 625.93  | -0.02  | 624.59  | 0      | 14.453  |  | 99.981  | -0.019 | 99.974  | -0.026 |
| 0.1166       | 625.357 | -0.803 | 626.297 | -0.013 | 625.63  | 0      | 625.924 | -0.026 | 624.59  | 0      | 14.453  |  | 99.981  | -0.019 | 99.974  | -0.026 |
| 0.125        | 625.275 | -0.885 | 626.297 | -0.013 | 625.63  | 0      | 625.924 | -0.026 | 624.59  | 0      | 14.453  |  | 99.981  | -0.019 | 99.974  | -0.026 |
| 0.1333       | 625.181 | -0.979 | 626.297 | -0.013 | 625.63  | 0      | 625.924 | -0.026 | 624.59  | 0      | 14.452  |  | 99.974  | -0.026 | 99.98   | -0.02  |
| 0.1416       | 625.155 | -1.005 | 626.297 | -0.013 | 625.63  | 0      | 625.924 | -0.026 | 624.583 | -0.007 | 14.452  |  | 99.974  | -0.026 | 99.98   | -0.02  |
| 0.15         | 625.029 | -1.131 | 626.297 | -0.013 | 625.63  | 0      | 625.924 | -0.026 | 624.583 | -0.007 | 14.453  |  | 99.974  | -0.026 | 99.98   | -0.02  |
| 0.1583       | 624.985 | -1.175 | 626.29  | -0.02  | 625.63  | 0      | 625.924 | -0.026 | 624.59  | 0      | 14.453  |  | 99.962  | -0.038 | 99.974  | -0.026 |
| 0.1666       | 624.878 | -1.282 | 626.29  | -0.02  | 625.63  | 0      | 625.918 | -0.032 | 624.59  | 0      | 14.453  |  | 99.962  | -0.038 | 99.98   | -0.02  |
| 0.175        | 624.777 | -1.383 | 626.29  | -0.02  | 625.636 | 0.006  | 625.918 | -0.032 | 624.59  | 0      | 14.453  |  | 99.962  | -0.038 | 99.98   | -0.02  |
| 0.1833       | 624.789 | -1.371 | 626.29  | -0.02  | 625.63  | 0      | 625.918 | -0.032 | 624.583 | -0.007 | 14.452  |  | 99.949  | -0.051 | 99.98   | -0.02  |
| 0.1916       | 624.764 | -1.396 | 626.29  | -0.02  | 625.63  | 0      | 625.918 | -0.032 | 624.59  | 0      | 14.452  |  | 99.949  | -0.051 | 99.98   | -0.02  |
| 0.2          | 624.688 | -1.472 | 626.284 | -0.026 | 625.623 | -0.007 | 625.918 | -0.032 | 624.583 | -0.007 | 14.453  |  | 99.943  | -0.057 | 99.98   | -0.02  |
| 0.2083       | 624.65  | -1.51  | 626.284 | -0.026 | 625.623 | -0.007 | 625.911 | -0.039 | 624.59  | 0      | 14.453  |  | 99.943  | -0.057 | 99.98   | -0.02  |
| 0.2166       | 624.657 | -1.503 | 626.284 | -0.026 | 625.623 | -0.007 | 625.911 | -0.039 | 624.59  | 0      | 14.453  |  | 99.93   | -0.07  | 99.98   | -0.02  |
| 0.225        | 624.6   | -1.56  | 626.284 | -0.026 | 625.623 | -0.007 | 625.911 | -0.039 | 624.59  | 0      | 14.453  |  | 99.936  | -0.064 | 99.98   | -0.02  |
| 0.2333       | 624.556 | -1.604 | 626.284 | -0.026 | 625.623 | -0.007 | 625.911 | -0.039 | 624.583 | -0.007 | 14.453  |  | 99.93   | -0.07  | 99.98   | -0.02  |
| 0.2416       | 624.53  | -1.63  | 626.284 | -0.026 | 625.623 | -0.007 | 625.911 | -0.039 | 624.59  | 0      | 14.453  |  | 99.924  | -0.076 | 99.987  | -0.013 |
| 0.25         | 624.455 | -1.705 | 626.278 | -0.032 | 625.623 | -0.007 | 625.905 | -0.045 | 624.59  | 0      | 14.452  |  | 99.924  | -0.076 | 99.98   | -0.02  |
| 0.2583       | 624.467 | -1.693 | 626.278 | -0.032 | 625.617 | -0.013 | 625.905 | -0.045 | 624.583 | -0.007 | 14.453  |  | 99.911  | -0.069 | 99.98   | -0.02  |
| 0.2666       | 624.461 | -1.699 | 626.278 | -0.032 | 625.623 | -0.007 | 625.905 | -0.045 | 624.583 | -0.007 | 14.454  |  | 99.911  | -0.069 | 99.987  | -0.013 |
| 0.275        | 624.442 | -1.718 | 626.278 | -0.032 | 625.617 | -0.013 | 625.899 | -0.051 | 624.59  | 0      | 14.453  |  | 99.905  | -0.095 | 99.987  | -0.013 |
| 0.2833       | 624.429 | -1.731 | 626.271 | -0.039 | 625.617 | -0.013 | 625.899 | -0.051 | 624.59  | 0      | 14.453  |  | 99.905  | -0.095 | 99.987  | -0.013 |
| 0.2916       | 624.391 | -1.769 | 626.271 | -0.039 | 625.617 | -0.013 | 625.899 | -0.051 | 624.583 | -0.007 | 14.454  |  | 99.898  | -0.102 | 99.987  | -0.013 |
| 0.3          | 624.391 | -1.769 | 626.271 | -0.039 | 625.61  | -0.02  | 625.899 | -0.051 | 624.59  | 0      | 14.453  |  | 99.886  | -0.114 | 99.987  | -0.013 |
| 0.3083       | 624.366 | -1.794 | 626.271 | -0.039 | 625.617 | -0.013 | 625.892 | -0.058 | 624.59  | 0      | 14.453  |  | 99.886  | -0.114 | 99.987  | -0.013 |
| 0.3166       | 624.354 | -1.806 | 626.271 | -0.039 | 625.61  | -0.02  | 625.892 | -0.058 | 624.583 | -0.007 | 14.453  |  | 99.886  | -0.114 | 99.987  | -0.013 |
| 0.325        | 624.335 | -1.825 | 626.265 | -0.045 | 625.61  | -0.02  | 625.892 | -0.058 | 624.583 | -0.007 | 14.453  |  | 99.879  | -0.121 | 99.987  | -0.013 |
| 0.3333       | 624.284 | -1.876 | 626.265 | -0.045 | 625.61  | -0.02  | 625.892 | -0.058 | 624.59  | 0      | 14.454  |  | 99.879  | -0.121 | 99.987  | -0.013 |
| 0.35         | 624.271 | -1.869 | 626.265 | -0.045 | 625.61  | -0.02  | 625.892 | -0.058 | 624.583 | -0.007 | 14.453  |  | 99.867  | -0.133 | 99.993  | -0.007 |
| 0.3666       | 624.29  | -1.87  | 626.258 | -0.052 | 625.604 | -0.026 | 625.886 | -0.064 | 624.583 | -0.007 | 14.453  |  | 99.86   | -0.14  | 99.993  | -0.007 |
| 0.3833       | 624.246 | -1.914 | 626.258 | -0.052 | 625.604 | -0.026 | 625.886 | -0.064 | 624.59  | 0      | 14.454  |  | 99.854  | -0.146 | 99.993  | -0.007 |
| 0.4          | 624.246 | -1.914 | 626.258 | -0.052 | 625.604 | -0.026 | 625.886 | -0.064 | 624.583 | -0.007 | 14.453  |  | 99.848  | -0.152 | 99.993  | -0.007 |
| 0.4166       | 624.202 | -1.958 | 626.252 | -0.058 | 625.604 | -0.026 | 625.88  | -0.07  | 624.583 | -0.007 | 14.454  |  | 99.841  | -0.158 | 99.993  | -0.007 |

| Elapsed Time | INPUT 1 |        | INPUT 2 |        | INPUT 3 |        | INPUT 4 |        | INPUT 5 |        | INPUT 6 |       | INPUT 7 |        | INPUT 8 |       |
|--------------|---------|--------|---------|--------|---------|--------|---------|--------|---------|--------|---------|-------|---------|--------|---------|-------|
|              | RW-2    | MW-3   | 14S     | 14I    |         | DC-P3  |         | ATM    |         | MW-2R  |         | MW-6R |         |        |         |       |
| 0.4333       | 624.198 | -1.964 | 626.246 | -0.064 | 625.598 | -0.032 | 625.88  | -0.07  | 624.583 | -0.007 | 14.453  |       | 99.841  | -0.159 | 100     | 0     |
| 0.45         | 624.208 | -1.952 | 626.246 | -0.064 | 625.598 | -0.032 | 625.88  | -0.07  | 624.583 | -0.007 | 14.454  |       | 99.835  | -0.165 | 100     | 0     |
| 0.4666       | 624.183 | -1.977 | 626.246 | -0.064 | 625.591 | -0.039 | 625.873 | -0.077 | 624.583 | -0.007 | 14.454  |       | 99.822  | -0.178 | 100     | 0     |
| 0.4833       | 624.139 | -2.021 | 626.239 | -0.071 | 625.598 | -0.032 | 625.873 | -0.077 | 624.59  | 0      | 14.454  |       | 99.822  | -0.178 | 100     | 0     |
| 0.5          | 624.063 | -2.097 | 626.239 | -0.071 | 625.591 | -0.039 | 625.873 | -0.077 | 624.583 | -0.007 | 14.454  |       | 99.81   | -0.19  | 100.006 | 0.006 |
| 0.5166       | 624.114 | -2.046 | 626.233 | -0.077 | 625.598 | -0.032 | 625.873 | -0.077 | 624.59  | 0      | 14.454  |       | 99.816  | -0.184 | 100.006 | 0.006 |
| 0.5333       | 624.101 | -2.059 | 626.233 | -0.077 | 625.598 | -0.032 | 625.867 | -0.083 | 624.59  | 0      | 14.454  |       | 99.81   | -0.19  | 100.006 | 0.006 |
| 0.55         | 624.038 | -2.122 | 626.226 | -0.084 | 625.591 | -0.039 | 625.867 | -0.083 | 624.59  | 0      | 14.454  |       | 99.803  | -0.197 | 100.006 | 0.006 |
| 0.5666       | 624.032 | -2.128 | 626.226 | -0.084 | 625.591 | -0.039 | 625.867 | -0.083 | 624.59  | 0      | 14.454  |       | 99.797  | -0.203 | 100.006 | 0.006 |
| 0.5833       | 623.975 | -2.185 | 626.22  | -0.09  | 625.591 | -0.039 | 625.867 | -0.083 | 624.59  | 0      | 14.454  |       | 99.791  | -0.209 | 100.006 | 0.006 |
| 0.6          | 623.956 | -2.204 | 626.22  | -0.09  | 625.591 | -0.039 | 625.861 | -0.089 | 624.59  | 0      | 14.453  |       | 99.784  | -0.216 | 100.006 | 0.006 |
| 0.6166       | 623.994 | -2.166 | 626.214 | -0.096 | 625.585 | -0.045 | 625.861 | -0.089 | 624.59  | 0      | 14.453  |       | 99.778  | -0.222 | 100.012 | 0.012 |
| 0.6333       | 623.937 | -2.223 | 626.214 | -0.096 | 625.585 | -0.045 | 625.861 | -0.089 | 624.59  | 0      | 14.454  |       | 99.772  | -0.228 | 100.012 | 0.012 |
| 0.65         | 623.937 | -2.223 | 626.207 | -0.103 | 625.585 | -0.045 | 625.861 | -0.089 | 624.59  | 0      | 14.453  |       | 99.778  | -0.222 | 100.012 | 0.012 |
| 0.6666       | 623.981 | -2.179 | 626.207 | -0.103 | 625.585 | -0.045 | 625.854 | -0.096 | 624.59  | 0      | 14.453  |       | 99.772  | -0.228 | 100.012 | 0.012 |
| 0.6833       | 623.918 | -2.242 | 626.201 | -0.109 | 625.585 | -0.045 | 625.854 | -0.096 | 624.59  | 0      | 14.454  |       | 99.765  | -0.235 | 100.012 | 0.012 |
| 0.7          | 623.912 | -2.248 | 626.201 | -0.109 | 625.579 | -0.051 | 625.854 | -0.096 | 624.59  | 0      | 14.454  |       | 99.753  | -0.247 | 100.012 | 0.012 |
| 0.7166       | 623.912 | -2.248 | 626.194 | -0.118 | 625.579 | -0.051 | 625.854 | -0.096 | 624.59  | 0      | 14.454  |       | 99.753  | -0.247 | 100.012 | 0.012 |
| 0.7333       | 623.899 | -2.261 | 626.194 | -0.116 | 625.579 | -0.051 | 625.854 | -0.096 | 624.59  | 0      | 14.454  |       | 99.759  | -0.241 | 100.012 | 0.012 |
| 0.75         | 623.88  | -2.28  | 626.188 | -0.122 | 625.579 | -0.051 | 625.848 | -0.102 | 624.59  | 0      | 14.454  |       | 99.753  | -0.247 | 100.006 | 0.006 |
| 0.7666       | 623.805 | -2.255 | 626.188 | -0.122 | 625.572 | -0.058 | 625.842 | -0.108 | 624.59  | 0      | 14.454  |       | 99.74   | -0.28  | 100.012 | 0.012 |
| 0.7833       | 623.881 | -2.289 | 626.188 | -0.122 | 625.572 | -0.058 | 625.842 | -0.108 | 624.59  | 0      | 14.454  |       | 99.734  | -0.268 | 100.006 | 0.006 |
| 0.8          | 623.838 | -2.324 | 626.182 | -0.128 | 625.566 | -0.064 | 625.835 | -0.115 | 624.583 | -0.007 | 14.454  |       | 99.734  | -0.268 | 100.012 | 0.012 |
| 0.8166       | 623.83  | -2.33  | 626.182 | -0.128 | 625.566 | -0.064 | 625.842 | -0.108 | 624.583 | -0.007 | 14.453  |       | 99.721  | -0.279 | 100.012 | 0.012 |
| 0.8333       | 623.691 | -2.469 | 626.182 | -0.128 | 625.56  | -0.07  | 625.835 | -0.115 | 624.59  | 0      | 14.454  |       | 99.721  | -0.279 | 100.006 | 0.006 |
| 0.85         | 623.842 | -2.318 | 626.175 | -0.135 | 625.566 | -0.064 | 625.835 | -0.115 | 624.583 | -0.007 | 14.453  |       | 99.715  | -0.285 | 100.006 | 0.006 |
| 0.8666       | 623.811 | -2.349 | 626.169 | -0.141 | 625.56  | -0.07  | 625.835 | -0.115 | 624.583 | -0.007 | 14.453  |       | 99.715  | -0.285 | 100.012 | 0.012 |
| 0.8833       | 623.811 | -2.349 | 626.169 | -0.141 | 625.56  | -0.07  | 625.829 | -0.121 | 624.583 | -0.007 | 14.453  |       | 99.708  | -0.292 | 100.012 | 0.012 |
| 0.9          | 623.785 | -2.375 | 626.162 | -0.148 | 625.56  | -0.07  | 625.829 | -0.121 | 624.583 | -0.007 | 14.453  |       | 99.708  | -0.292 | 100.012 | 0.012 |
| 0.9166       | 623.754 | -2.408 | 626.162 | -0.148 | 625.553 | -0.077 | 625.829 | -0.121 | 624.59  | 0      | 14.453  |       | 99.702  | -0.298 | 100.012 | 0.012 |
| 0.9333       | 623.748 | -2.412 | 626.162 | -0.148 | 625.56  | -0.07  | 625.829 | -0.121 | 624.583 | -0.007 | 14.453  |       | 99.702  | -0.298 | 100.012 | 0.012 |
| 0.95         | 623.722 | -2.438 | 626.156 | -0.154 | 625.553 | -0.077 | 625.823 | -0.127 | 624.59  | 0      | 14.454  |       | 99.696  | -0.304 | 100.012 | 0.012 |
| 0.9666       | 623.722 | -2.438 | 626.156 | -0.154 | 625.553 | -0.077 | 625.829 | -0.121 | 624.59  | 0      | 14.453  |       | 99.696  | -0.304 | 100.019 | 0.019 |
| 0.9833       | 623.716 | -2.444 | 626.15  | -0.16  | 625.553 | -0.077 | 625.823 | -0.127 | 624.583 | -0.007 | 14.453  |       | 99.69   | -0.31  | 100.019 | 0.019 |
| 1            | 623.741 | -2.419 | 626.15  | -0.16  | 625.553 | -0.077 | 625.823 | -0.127 | 624.59  | 0      | 14.453  |       | 99.683  | -0.317 | 100.019 | 0.019 |
| 1.2          | 623.598 | -2.564 | 626.111 | -0.199 | 625.541 | -0.089 | 625.81  | -0.14  | 624.59  | 0      | 14.453  |       | 99.645  | -0.355 | 100.025 | 0.025 |
| 1.4          | 623.514 | -2.648 | 626.105 | -0.205 | 625.534 | -0.096 | 625.797 | -0.153 | 624.59  | 0      | 14.453  |       | 99.62   | -0.38  | 100.031 | 0.031 |
| 1.6          | 623.419 | -2.741 | 626.034 | -0.276 | 625.522 | -0.108 | 625.785 | -0.165 | 624.59  | 0      | 14.453  |       | 99.595  | -0.405 | 100.044 | 0.044 |
| 1.8          | 623.363 | -2.797 | 626.009 | -0.301 | 625.515 | -0.115 | 625.772 | -0.178 | 624.59  | 0      | 14.453  |       | 99.569  | -0.431 | 100.057 | 0.057 |
| 2            | 623.331 | -2.829 | 625.983 | -0.327 | 625.509 | -0.121 | 625.759 | -0.191 | 624.59  | 0      | 14.454  |       | 99.557  | -0.443 | 100.057 | 0.057 |
| 2.2          | 623.268 | -2.892 | 625.951 | -0.359 | 625.498 | -0.134 | 625.747 | -0.203 | 624.59  | 0      | 14.453  |       | 99.538  | -0.462 | 100.057 | 0.057 |
| 2.4          | 623.28  | -2.88  | 625.932 | -0.378 | 625.49  | -0.14  | 625.74  | -0.21  | 624.59  | 0      | 14.454  |       | 99.506  | -0.494 | 100.057 | 0.057 |
| 2.6          | 623.198 | -2.962 | 625.906 | -0.404 | 625.477 | -0.153 | 625.728 | -0.222 | 624.59  | 0      | 14.453  |       | 99.493  | -0.507 | 100.057 | 0.057 |
| 2.8          | 623.186 | -2.974 | 625.887 | -0.423 | 625.471 | -0.159 | 625.721 | -0.229 | 624.59  | 0      | 14.453  |       | 99.474  | -0.526 | 100.057 | 0.057 |
| 3            | 623.11  | -3.05  | 625.874 | -0.436 | 625.465 | -0.165 | 625.715 | -0.235 | 624.59  | 0      | 14.453  |       | 99.462  | -0.538 | 100.063 | 0.063 |
| 3.2          | 623.142 | -3.018 | 625.855 | -0.455 | 625.465 | -0.165 | 625.702 | -0.248 | 624.59  | 0      | 14.453  |       | 99.462  | -0.538 | 100.076 | 0.076 |

| Elapsed Time | INPUT 1 | INPUT 2 | INPUT 3 | INPUT 4 | INPUT 5 | INPUT 6 | INPUT 7 | INPUT 8 |
|--------------|---------|---------|---------|---------|---------|---------|---------|---------|
|              | RW-2    | MW-3    | 14S     | 14I     | DC-P3   | ATM     | MW-2R   | MW-6R   |
| 3.4          | 623.085 | -3.075  | 625.836 | -0.474  | 625.452 | -0.178  | 625.696 | -0.254  |
| 3.6          | 623.104 | -3.056  | 625.817 | -0.493  | 625.446 | -0.184  | 625.669 | -0.26   |
| 3.8          | 623.041 | -3.119  | 625.798 | -0.512  | 625.439 | -0.191  | 625.677 | -0.273  |
| 4            | 623.041 | -3.119  | 625.785 | -0.525  | 625.433 | -0.197  | 625.671 | -0.279  |
| 4.2          | 623.015 | -3.145  | 625.772 | -0.538  | 625.433 | -0.197  | 625.664 | -0.286  |
| 4.4          | 623.009 | -3.151  | 625.759 | -0.551  | 625.42  | -0.21   | 625.658 | -0.292  |
| 4.6          | 622.952 | -3.208  | 625.74  | -0.57   | 625.42  | -0.21   | 625.652 | -0.298  |
| 4.8          | 622.996 | -3.164  | 625.734 | -0.576  | 625.414 | -0.218  | 625.645 | -0.305  |
| 5            | 622.927 | -3.233  | 625.721 | -0.589  | 625.408 | -0.222  | 625.639 | -0.311  |
| 5.2          | 622.952 | -3.208  | 625.702 | -0.608  | 625.389 | -0.241  | 625.626 | -0.324  |
| 5.4          | 622.921 | -3.239  | 625.689 | -0.621  | 625.382 | -0.248  | 625.62  | -0.33   |
| 5.6          | 622.889 | -3.271  | 625.682 | -0.628  | 625.382 | -0.248  | 625.614 | -0.336  |
| 5.8          | 622.914 | -3.246  | 625.663 | -0.647  | 625.376 | -0.254  | 625.607 | -0.343  |
| 6            | 622.908 | -3.252  | 625.657 | -0.653  | 625.369 | -0.261  | 625.601 | -0.349  |
| 6.2          | 622.877 | -3.283  | 625.644 | -0.666  | 625.369 | -0.261  | 625.601 | -0.349  |
| 6.4          | 622.883 | -3.277  | 625.636 | -0.672  | 625.363 | -0.267  | 625.595 | -0.355  |
| 6.6          | 622.87  | -3.29   | 625.631 | -0.679  | 625.369 | -0.261  | 625.595 | -0.355  |
| 6.8          | 622.877 | -3.283  | 625.625 | -0.685  | 625.363 | -0.267  | 625.585 | -0.355  |
| 7            | 622.828 | -3.334  | 625.612 | -0.698  | 625.35  | -0.28   | 625.588 | -0.362  |
| 7.2          | 622.87  | -3.29   | 625.606 | -0.704  | 625.35  | -0.28   | 625.582 | -0.368  |
| 7.4          | 622.832 | -3.328  | 625.599 | -0.711  | 625.344 | -0.286  | 625.582 | -0.368  |
| 7.6          | 622.832 | -3.328  | 625.593 | -0.717  | 625.344 | -0.286  | 625.576 | -0.374  |
| 7.8          | 622.832 | -3.328  | 625.58  | -0.73   | 625.338 | -0.292  | 625.569 | -0.381  |
| 8            | 622.851 | -3.309  | 625.574 | -0.736  | 625.338 | -0.292  | 625.563 | -0.387  |
| 8.2          | 622.813 | -3.347  | 625.567 | -0.743  | 625.331 | -0.299  | 625.563 | -0.387  |
| 8.4          | 622.845 | -3.315  | 625.561 | -0.749  | 625.331 | -0.299  | 625.563 | -0.387  |
| 8.6          | 622.832 | -3.328  | 625.554 | -0.756  | 625.325 | -0.305  | 625.557 | -0.393  |
| 8.8          | 622.813 | -3.347  | 625.548 | -0.762  | 625.325 | -0.305  | 625.557 | -0.393  |
| 9            | 622.832 | -3.328  | 625.542 | -0.768  | 625.319 | -0.311  | 625.55  | -0.4    |
| 9.2          | 622.788 | -3.372  | 625.535 | -0.775  | 625.319 | -0.311  | 625.544 | -0.406  |
| 9.4          | 622.832 | -3.328  | 625.529 | -0.781  | 625.319 | -0.311  | 625.544 | -0.406  |
| 9.6          | 622.82  | -3.34   | 625.535 | -0.775  | 625.312 | -0.318  | 625.538 | -0.412  |
| 9.8          | 622.801 | -3.359  | 625.529 | -0.781  | 625.312 | -0.318  | 625.538 | -0.412  |
| 10           | 622.813 | -3.347  | 625.523 | -0.787  | 625.312 | -0.318  | 625.538 | -0.412  |
| 12           | 622.87  | -3.29   | 625.478 | -0.832  | 625.293 | -0.337  | 625.519 | -0.431  |
| 14           | 622.826 | -3.334  | 625.452 | -0.858  | 625.281 | -0.349  | 625.5   | -0.45   |
| 16           | 622.813 | -3.347  | 625.433 | -0.877  | 625.268 | -0.362  | 625.481 | -0.469  |
| 18           | 622.813 | -3.347  | 625.439 | -0.871  | 625.262 | -0.368  | 625.468 | -0.482  |
| 20           | 622.807 | -3.353  | 625.414 | -0.896  | 625.249 | -0.381  | 625.455 | -0.495  |
| 22           | 622.813 | -3.347  | 625.395 | -0.915  | 625.236 | -0.394  | 625.449 | -0.501  |
| 24           | 622.763 | -3.397  | 625.407 | -0.903  | 625.23  | -0.4    | 625.436 | -0.514  |
| 26           | 622.832 | -3.328  | 625.401 | -0.909  | 625.224 | -0.406  | 625.43  | -0.52   |
| 28           | 622.75  | -3.41   | 625.388 | -0.922  | 625.224 | -0.406  | 625.417 | -0.533  |
| 30           | 622.795 | -3.365  | 625.382 | -0.928  | 625.217 | -0.413  | 625.404 | -0.546  |
| 32           | 622.795 | -3.365  | 625.386 | -0.922  | 625.224 | -0.406  | 625.417 | -0.533  |
| 34           | 622.769 | -3.391  | 625.375 | -0.935  | 625.198 | -0.432  | 625.404 | -0.546  |

| Elapsed Time | INPUT 1 | INPUT 2 | INPUT 3 | INPUT 4 | INPUT 5 | INPUT 6 | INPUT 7 | INPUT 8 |
|--------------|---------|---------|---------|---------|---------|---------|---------|---------|
|              | RW-2    | MW-3    | 14S     | 14I     | DC-P3   | ATM     | MW-2R   | MW-6R   |
| 36           | 622.75  | -3.41   | 625.363 | -0.947  | 625.205 | -0.425  | 625.411 | -0.539  |
| 38           | 622.763 | -3.397  | 625.363 | -0.947  | 625.192 | -0.438  | 625.398 | -0.552  |
| 40           | 622.795 | -3.385  | 625.35  | -0.96   | 625.192 | -0.438  | 625.392 | -0.558  |
| 42           | 622.738 | -3.422  | 625.343 | -0.967  | 625.192 | -0.438  | 625.385 | -0.565  |
| 44           | 622.744 | -3.416  | 625.35  | -0.96   | 625.198 | -0.432  | 625.392 | -0.558  |
| 46           | 622.731 | -3.429  | 625.35  | -0.96   | 625.186 | -0.444  | 625.385 | -0.565  |
| 48           | 622.757 | -3.403  | 625.35  | -0.96   | 625.186 | -0.444  | 625.373 | -0.577  |
| 50           | 622.725 | -3.435  | 625.343 | -0.967  | 625.179 | -0.451  | 625.373 | -0.577  |
| 52           | 622.795 | -3.385  | 625.331 | -0.979  | 625.179 | -0.451  | 625.373 | -0.577  |
| 54           | 622.75  | -3.41   | 625.331 | -0.979  | 625.192 | -0.438  | 625.385 | -0.565  |
| 56           | 622.719 | -3.441  | 625.318 | -0.992  | 625.167 | -0.463  | 625.366 | -0.584  |
| 58           | 622.763 | -3.397  | 625.318 | -0.992  | 625.173 | -0.457  | 625.366 | -0.584  |
| 60           | 622.738 | -3.422  | 625.311 | -0.999  | 625.167 | -0.463  | 625.366 | -0.584  |
| 62           | 622.731 | -3.429  | 625.305 | -1.005  | 625.167 | -0.463  | 625.366 | -0.584  |
| 64           | 622.75  | -3.41   | 625.299 | -1.011  | 625.167 | -0.463  | 625.36  | -0.59   |
| 66           | 622.763 | -3.397  | 625.299 | -1.011  | 625.167 | -0.463  | 625.36  | -0.59   |
| 68           | 622.757 | -3.403  | 625.292 | -1.018  | 625.167 | -0.463  | 625.36  | -0.59   |
| 70           | 622.738 | -3.422  | 625.292 | -1.018  | 625.16  | -0.47   | 625.354 | -0.598  |
| 72           | 622.75  | -3.41   | 625.286 | -1.024  | 625.16  | -0.47   | 625.354 | -0.598  |
| 74           | 622.731 | -3.429  | 625.279 | -1.031  | 625.16  | -0.47   | 625.354 | -0.598  |
| 76           | 622.738 | -3.422  | 625.279 | -1.031  | 625.16  | -0.47   | 625.354 | -0.598  |
| 78           | 622.757 | -3.403  | 625.279 | -1.031  | 625.173 | -0.457  | 625.366 | -0.584  |
| 80           | 622.712 | -3.448  | 625.267 | -1.043  | 625.148 | -0.482  | 625.347 | -0.603  |
| 82           | 622.75  | -3.41   | 625.267 | -1.043  | 625.154 | -0.476  | 625.347 | -0.603  |
| 84           | 622.725 | -3.435  | 625.267 | -1.043  | 625.154 | -0.476  | 625.347 | -0.603  |
| 86           | 622.738 | -3.422  | 625.254 | -1.056  | 625.154 | -0.476  | 625.347 | -0.603  |
| 88           | 622.731 | -3.429  | 625.254 | -1.056  | 625.148 | -0.482  | 625.347 | -0.603  |
| 90           | 622.744 | -3.416  | 625.254 | -1.056  | 625.154 | -0.476  | 625.347 | -0.603  |
| 92           | 622.744 | -3.416  | 625.247 | -1.063  | 625.148 | -0.482  | 625.341 | -0.609  |
| 94           | 622.731 | -3.429  | 625.254 | -1.056  | 625.167 | -0.463  | 625.347 | -0.603  |
| 96           | 622.738 | -3.422  | 625.241 | -1.069  | 625.141 | -0.489  | 625.341 | -0.609  |
| 98           | 622.757 | -3.403  | 625.241 | -1.069  | 625.148 | -0.482  | 625.341 | -0.609  |
| 100          | 622.757 | -3.403  | 625.241 | -1.069  | 625.141 | -0.489  | 625.341 | -0.609  |
| 120          | 622.744 | -3.416  | 625.215 | -1.095  | 625.135 | -0.495  | 625.328 | -0.622  |
| 140          | 622.75  | -3.41   | 625.198 | -1.114  | 625.129 | -0.501  | 625.328 | -0.622  |
| 160          | 622.719 | -3.441  | 625.171 | -1.139  | 625.122 | -0.508  | 625.309 | -0.641  |
| 180          | 622.725 | -3.435  | 625.158 | -1.152  | 625.109 | -0.521  | 625.309 | -0.641  |
| 200          | 622.712 | -3.448  | 625.145 | -1.165  | 625.103 | -0.527  | 625.297 | -0.653  |
| 220          | 622.731 | -3.429  | 625.132 | -1.178  | 625.103 | -0.527  | 625.297 | -0.653  |
| 240          | 622.744 | -3.416  | 625.126 | -1.184  | 625.097 | -0.533  | 625.29  | -0.66   |
| 260          | 622.757 | -3.403  | 625.126 | -1.184  | 625.097 | -0.533  | 625.29  | -0.66   |
| 280          | 622.738 | -3.422  | 625.107 | -1.203  | 625.084 | -0.546  | 625.284 | -0.666  |
| 300          | 622.7   | -3.46   | 625.1   | -1.21   | 625.084 | -0.546  | 625.278 | -0.672  |
| 320          | 622.712 | -3.448  | 625.107 | -1.203  | 625.078 | -0.552  | 625.265 | -0.685  |
| 340          | 622.725 | -3.435  | 625.087 | -1.223  | 625.071 | -0.559  | 625.265 | -0.685  |
| 360          | 622.731 | -3.429  | 625.081 | -1.229  | 625.071 | -0.559  | 625.259 | -0.691  |

| Date     | Time     | Elapsed T | Feet H2O |         | Delta H | Celsius |
|----------|----------|-----------|----------|---------|---------|---------|
| 07/16/96 | 13:14:00 | 0         | 10.027   | 626.633 | -0.164  | 12.56   |
| 07/16/96 | 13:15:00 | 1         | 10.029   | 626.631 | -0.166  | 12.56   |
| 07/16/96 | 13:16:00 | 2         | 10.032   | 626.628 | -0.169  | 12.56   |
| 07/16/96 | 13:17:00 | 3         | 10.036   | 626.624 | -0.173  | 12.56   |
| 07/16/96 | 13:18:00 | 4         | 10.036   | 626.624 | -0.173  | 12.56   |
| 07/16/96 | 13:19:00 | 5         | 10.036   | 626.624 | -0.173  | 12.56   |
| 07/16/96 | 13:20:00 | 6         | 10.036   | 626.624 | -0.173  | 12.56   |
| 07/16/96 | 13:21:00 | 7         | 10.039   | 626.621 | -0.176  | 12.56   |
| 07/16/96 | 13:22:00 | 8         | 10.041   | 626.619 | -0.178  | 12.56   |
| 07/16/96 | 13:23:00 | 9         | 10.043   | 626.617 | -0.18   | 12.56   |
| 07/16/96 | 13:24:00 | 10        | 10.043   | 626.617 | -0.18   | 12.56   |
| 07/16/96 | 13:25:00 | 11        | 10.045   | 626.615 | -0.182  | 12.55   |
| 07/16/96 | 13:26:00 | 12        | 10.048   | 626.612 | -0.185  | 12.56   |
| 07/16/96 | 13:27:00 | 13        | 10.048   | 626.612 | -0.185  | 12.55   |
| 07/16/96 | 13:28:00 | 14        | 10.048   | 626.612 | -0.185  | 12.55   |
| 07/16/96 | 13:29:00 | 15        | 10.05    | 626.61  | -0.187  | 12.55   |
| 07/16/96 | 13:30:00 | 16        | 10.052   | 626.608 | -0.189  | 12.55   |
| 07/16/96 | 13:31:00 | 17        | 10.052   | 626.608 | -0.189  | 12.55   |
| 07/16/96 | 13:32:00 | 18        | 10.055   | 626.605 | -0.192  | 12.55   |
| 07/16/96 | 13:33:00 | 19        | 10.055   | 626.605 | -0.192  | 12.55   |
| 07/16/96 | 13:34:00 | 20        | 10.057   | 626.603 | -0.194  | 12.55   |
| 07/16/96 | 13:35:00 | 21        | 10.057   | 626.603 | -0.194  | 12.55   |
| 07/16/96 | 13:36:00 | 22        | 10.059   | 626.601 | -0.196  | 12.55   |
| 07/16/96 | 13:37:00 | 23        | 10.059   | 626.601 | -0.196  | 12.55   |
| 07/16/96 | 13:38:00 | 24        | 10.062   | 626.598 | -0.199  | 12.55   |
| 07/16/96 | 13:39:00 | 25        | 10.062   | 626.598 | -0.199  | 12.55   |
| 07/16/96 | 13:40:00 | 26        | 10.064   | 626.596 | -0.201  | 12.55   |
| 07/16/96 | 13:41:00 | 27        | 10.064   | 626.596 | -0.201  | 12.55   |
| 07/16/96 | 13:42:00 | 28        | 10.064   | 626.596 | -0.201  | 12.56   |
| 07/16/96 | 13:43:00 | 29        | 10.069   | 626.591 | -0.206  | 12.55   |
| 07/16/96 | 13:44:00 | 30        | 10.066   | 626.594 | -0.203  | 12.55   |
| 07/16/96 | 13:45:00 | 31        | 10.069   | 626.591 | -0.206  | 12.55   |
| 07/16/96 | 13:46:00 | 32        | 10.073   | 626.587 | -0.21   | 12.56   |
| 07/16/96 | 13:47:00 | 33        | 10.073   | 626.587 | -0.21   | 12.55   |
| 07/16/96 | 13:48:00 | 34        | 10.073   | 626.587 | -0.21   | 12.55   |
| 07/16/96 | 13:49:00 | 35        | 10.075   | 626.585 | -0.212  | 12.56   |
| 07/16/96 | 13:50:00 | 36        | 10.078   | 626.582 | -0.215  | 12.55   |
| 07/16/96 | 13:51:00 | 37        | 10.075   | 626.585 | -0.212  | 12.55   |
| 07/16/96 | 13:52:00 | 38        | 10.075   | 626.585 | -0.212  | 12.55   |
| 07/16/96 | 13:53:00 | 39        | 10.075   | 626.585 | -0.212  | 12.55   |
| 07/16/96 | 13:54:00 | 40        | 10.078   | 626.582 | -0.215  | 12.56   |
| 07/16/96 | 13:55:00 | 41        | 10.078   | 626.582 | -0.215  | 12.55   |
| 07/16/96 | 13:56:00 | 42        | 10.078   | 626.582 | -0.215  | 12.55   |
| 07/16/96 | 13:57:00 | 43        | 10.08    | 626.58  | -0.217  | 12.55   |
| 07/16/96 | 13:58:00 | 44        | 10.082   | 626.578 | -0.219  | 12.55   |
| 07/16/96 | 13:59:00 | 45        | 10.082   | 626.578 | -0.219  | 12.55   |
| 07/16/96 | 14:00:00 | 46        | 10.082   | 626.578 | -0.219  | 12.55   |
| 07/16/96 | 14:01:00 | 47        | 10.082   | 626.578 | -0.219  | 12.55   |
| 07/16/96 | 14:02:00 | 48        | 10.082   | 626.578 | -0.219  | 12.55   |
| 07/16/96 | 14:03:00 | 49        | 10.082   | 626.578 | -0.219  | 12.55   |

| Date     | Time     | Elapsed T | Feet H2O |         | Delta H | Celsius |
|----------|----------|-----------|----------|---------|---------|---------|
| 07/16/96 | 14:04:00 | 50        | 10.085   | 626.575 | -0.222  | 12.55   |
| 07/16/96 | 14:05:00 | 51        | 10.085   | 626.575 | -0.222  | 12.55   |
| 07/16/96 | 14:06:00 | 52        | 10.085   | 626.575 | -0.222  | 12.55   |
| 07/16/96 | 14:07:00 | 53        | 10.085   | 626.575 | -0.222  | 12.55   |
| 07/16/96 | 14:08:00 | 54        | 10.087   | 626.573 | -0.224  | 12.55   |
| 07/16/96 | 14:09:00 | 55        | 10.087   | 626.573 | -0.224  | 12.55   |
| 07/16/96 | 14:10:00 | 56        | 10.089   | 626.571 | -0.226  | 12.55   |
| 07/16/96 | 14:11:00 | 57        | 10.092   | 626.568 | -0.229  | 12.55   |
| 07/16/96 | 14:12:00 | 58        | 10.092   | 626.568 | -0.229  | 12.55   |
| 07/16/96 | 14:13:00 | 59        | 10.092   | 626.568 | -0.229  | 12.55   |
| 07/16/96 | 14:14:00 | 60        | 10.092   | 626.568 | -0.229  | 12.55   |
| 07/16/96 | 14:15:00 | 61        | 10.092   | 626.568 | -0.229  | 12.55   |
| 07/16/96 | 14:16:00 | 62        | 10.094   | 626.566 | -0.231  | 12.55   |
| 07/16/96 | 14:17:00 | 63        | 10.094   | 626.566 | -0.231  | 12.55   |
| 07/16/96 | 14:18:00 | 64        | 10.094   | 626.566 | -0.231  | 12.55   |
| 07/16/96 | 14:19:00 | 65        | 10.094   | 626.566 | -0.231  | 12.55   |
| 07/16/96 | 14:20:00 | 66        | 10.096   | 626.564 | -0.233  | 12.55   |
| 07/16/96 | 14:21:00 | 67        | 10.096   | 626.564 | -0.233  | 12.55   |
| 07/16/96 | 14:22:00 | 68        | 10.096   | 626.564 | -0.233  | 12.55   |
| 07/16/96 | 14:23:00 | 69        | 10.096   | 626.564 | -0.233  | 12.55   |
| 07/16/96 | 14:24:00 | 70        | 10.098   | 626.562 | -0.235  | 12.55   |
| 07/16/96 | 14:25:00 | 71        | 10.098   | 626.562 | -0.235  | 12.55   |
| 07/16/96 | 14:26:00 | 72        | 10.098   | 626.562 | -0.235  | 12.55   |
| 07/16/96 | 14:27:00 | 73        | 10.098   | 626.562 | -0.235  | 12.55   |
| 07/16/96 | 14:28:00 | 74        | 10.101   | 626.559 | -0.238  | 12.55   |
| 07/16/96 | 14:29:00 | 75        | 10.098   | 626.562 | -0.235  | 12.55   |
| 07/16/96 | 14:30:00 | 76        | 10.103   | 626.557 | -0.24   | 12.55   |
| 07/16/96 | 14:31:00 | 77        | 10.103   | 626.557 | -0.24   | 12.55   |
| 07/16/96 | 14:32:00 | 78        | 10.101   | 626.559 | -0.238  | 12.55   |
| 07/16/96 | 14:33:00 | 79        | 10.103   | 626.557 | -0.24   | 12.55   |
| 07/16/96 | 14:34:00 | 80        | 10.103   | 626.557 | -0.24   | 12.55   |
| 07/16/96 | 14:35:00 | 81        | 10.105   | 626.555 | -0.242  | 12.55   |
| 07/16/96 | 14:36:00 | 82        | 10.103   | 626.557 | -0.24   | 12.55   |
| 07/16/96 | 14:37:00 | 83        | 10.105   | 626.555 | -0.242  | 12.55   |
| 07/16/96 | 14:38:00 | 84        | 10.103   | 626.557 | -0.24   | 12.55   |
| 07/16/96 | 14:39:00 | 85        | 10.105   | 626.555 | -0.242  | 12.55   |
| 07/16/96 | 14:40:00 | 86        | 10.105   | 626.555 | -0.242  | 12.55   |
| 07/16/96 | 14:41:00 | 87        | 10.108   | 626.552 | -0.245  | 12.55   |
| 07/16/96 | 14:42:00 | 88        | 10.108   | 626.552 | -0.245  | 12.55   |
| 07/16/96 | 14:43:00 | 89        | 10.105   | 626.555 | -0.242  | 12.55   |
| 07/16/96 | 14:44:00 | 90        | 10.105   | 626.555 | -0.242  | 12.55   |
| 07/16/96 | 14:45:00 | 91        | 10.108   | 626.552 | -0.245  | 12.55   |
| 07/16/96 | 14:46:00 | 92        | 10.108   | 626.552 | -0.245  | 12.55   |
| 07/16/96 | 14:47:00 | 93        | 10.11    | 626.55  | -0.247  | 12.55   |
| 07/16/96 | 14:48:00 | 94        | 10.108   | 626.552 | -0.245  | 12.55   |
| 07/16/96 | 14:49:00 | 95        | 10.11    | 626.55  | -0.247  | 12.55   |
| 07/16/96 | 14:50:00 | 96        | 10.11    | 626.55  | -0.247  | 12.55   |
| 07/16/96 | 14:51:00 | 97        | 10.11    | 626.55  | -0.247  | 12.55   |
| 07/16/96 | 14:52:00 | 98        | 10.112   | 626.548 | -0.249  | 12.55   |
| 07/16/96 | 14:53:00 | 99        | 10.112   | 626.548 | -0.249  | 12.55   |

| Date     | Time     | Elapsed T | Feet H2O |         | Delta H | Celsius |
|----------|----------|-----------|----------|---------|---------|---------|
| 07/16/96 | 14:54:00 | 100       | 10.11    | 626.55  | -0.247  | 12.55   |
| 07/16/96 | 14:55:00 | 101       | 10.112   | 626.548 | -0.249  | 12.55   |
| 07/16/96 | 14:56:00 | 102       | 10.115   | 626.545 | -0.252  | 12.55   |
| 07/16/96 | 14:57:00 | 103       | 10.115   | 626.545 | -0.252  | 12.55   |
| 07/16/96 | 14:58:00 | 104       | 10.112   | 626.548 | -0.249  | 12.55   |
| 07/16/96 | 14:59:00 | 105       | 10.112   | 626.548 | -0.249  | 12.55   |
| 07/16/96 | 15:00:00 | 106       | 10.115   | 626.545 | -0.252  | 12.55   |
| 07/16/96 | 15:01:00 | 107       | 10.115   | 626.545 | -0.252  | 12.55   |
| 07/16/96 | 15:02:00 | 108       | 10.115   | 626.545 | -0.252  | 12.55   |
| 07/16/96 | 15:03:00 | 109       | 10.112   | 626.548 | -0.249  | 12.55   |
| 07/16/96 | 15:04:00 | 110       | 10.115   | 626.545 | -0.252  | 12.55   |
| 07/16/96 | 15:05:00 | 111       | 10.115   | 626.545 | -0.252  | 12.55   |
| 07/16/96 | 15:06:00 | 112       | 10.117   | 626.543 | -0.254  | 12.55   |
| 07/16/96 | 15:07:00 | 113       | 10.115   | 626.545 | -0.252  | 12.55   |
| 07/16/96 | 15:08:00 | 114       | 10.119   | 626.541 | -0.256  | 12.55   |
| 07/16/96 | 15:09:00 | 115       | 10.119   | 626.541 | -0.256  | 12.55   |
| 07/16/96 | 15:10:00 | 116       | 10.119   | 626.541 | -0.256  | 12.55   |
| 07/16/96 | 15:11:00 | 117       | 10.119   | 626.541 | -0.256  | 12.55   |
| 07/16/96 | 15:12:00 | 118       | 10.119   | 626.541 | -0.256  | 12.55   |
| 07/16/96 | 15:13:00 | 119       | 10.119   | 626.541 | -0.256  | 12.55   |
| 07/16/96 | 15:14:00 | 120       | 10.122   | 626.538 | -0.259  | 12.55   |
| 07/16/96 | 15:15:00 | 121       | 10.122   | 626.538 | -0.259  | 12.55   |
| 07/16/96 | 15:16:00 | 122       | 10.122   | 626.538 | -0.259  | 12.55   |
| 07/16/96 | 15:17:00 | 123       | 10.122   | 626.538 | -0.259  | 12.55   |
| 07/16/96 | 15:18:00 | 124       | 10.122   | 626.538 | -0.259  | 12.55   |
| 07/16/96 | 15:19:00 | 125       | 10.122   | 626.538 | -0.259  | 12.55   |
| 07/16/96 | 15:20:00 | 126       | 10.124   | 626.536 | -0.261  | 12.55   |
| 07/16/96 | 15:21:00 | 127       | 10.122   | 626.538 | -0.259  | 12.56   |
| 07/16/96 | 15:22:00 | 128       | 10.124   | 626.536 | -0.261  | 12.56   |
| 07/16/96 | 15:23:00 | 129       | 10.124   | 626.536 | -0.261  | 12.55   |
| 07/16/96 | 15:24:00 | 130       | 10.126   | 626.534 | -0.263  | 12.55   |
| 07/16/96 | 15:25:00 | 131       | 10.126   | 626.534 | -0.263  | 12.55   |
| 07/16/96 | 15:26:00 | 132       | 10.126   | 626.534 | -0.263  | 12.55   |
| 07/16/96 | 15:27:00 | 133       | 10.128   | 626.532 | -0.265  | 12.55   |
| 07/16/96 | 15:28:00 | 134       | 10.126   | 626.534 | -0.263  | 12.55   |
| 07/16/96 | 15:29:00 | 135       | 10.128   | 626.532 | -0.265  | 12.55   |
| 07/16/96 | 15:30:00 | 136       | 10.128   | 626.532 | -0.265  | 12.55   |
| 07/16/96 | 15:31:00 | 137       | 10.128   | 626.532 | -0.265  | 12.55   |
| 07/16/96 | 15:32:00 | 138       | 10.128   | 626.532 | -0.265  | 12.55   |
| 07/16/96 | 15:33:00 | 139       | 10.128   | 626.532 | -0.265  | 12.55   |
| 07/16/96 | 15:34:00 | 140       | 10.128   | 626.532 | -0.265  | 12.55   |
| 07/16/96 | 15:35:00 | 141       | 10.128   | 626.532 | -0.265  | 12.55   |
| 07/16/96 | 15:36:00 | 142       | 10.128   | 626.532 | -0.265  | 12.55   |
| 07/16/96 | 15:37:00 | 143       | 10.128   | 626.532 | -0.265  | 12.55   |
| 07/16/96 | 15:38:00 | 144       | 10.131   | 626.529 | -0.268  | 12.55   |
| 07/16/96 | 15:39:00 | 145       | 10.131   | 626.529 | -0.268  | 12.55   |
| 07/16/96 | 15:40:00 | 146       | 10.128   | 626.532 | -0.265  | 12.55   |
| 07/16/96 | 15:41:00 | 147       | 10.131   | 626.529 | -0.268  | 12.55   |
| 07/16/96 | 15:42:00 | 148       | 10.133   | 626.527 | -0.27   | 12.55   |
| 07/16/96 | 15:43:00 | 149       | 10.133   | 626.527 | -0.27   | 12.55   |

| Date     | Time     | Elapsed T | Feet H2O |         | Delta H | Celsius |
|----------|----------|-----------|----------|---------|---------|---------|
| 07/16/96 | 15:44:00 | 150       | 10.133   | 626.527 | -0.27   | 12.55   |
| 07/16/96 | 15:45:00 | 151       | 10.133   | 626.527 | -0.27   | 12.55   |
| 07/16/96 | 15:46:00 | 152       | 10.133   | 626.527 | -0.27   | 12.55   |
| 07/16/96 | 15:47:00 | 153       | 10.133   | 626.527 | -0.27   | 12.55   |
| 07/16/96 | 15:48:00 | 154       | 10.133   | 626.527 | -0.27   | 12.55   |
| 07/16/96 | 15:49:00 | 155       | 10.135   | 626.525 | -0.272  | 12.55   |
| 07/16/96 | 15:50:00 | 156       | 10.135   | 626.525 | -0.272  | 12.55   |
| 07/16/96 | 15:51:00 | 157       | 10.138   | 626.522 | -0.275  | 12.55   |
| 07/16/96 | 15:52:00 | 158       | 10.138   | 626.522 | -0.275  | 12.55   |
| 07/16/96 | 15:53:00 | 159       | 10.138   | 626.522 | -0.275  | 12.55   |
| 07/16/96 | 15:54:00 | 160       | 10.138   | 626.522 | -0.275  | 12.55   |
| 07/16/96 | 15:55:00 | 161       | 10.138   | 626.522 | -0.275  | 12.55   |
| 07/16/96 | 15:56:00 | 162       | 10.138   | 626.522 | -0.275  | 12.55   |
| 07/16/96 | 15:57:00 | 163       | 10.138   | 626.522 | -0.275  | 12.55   |
| 07/16/96 | 15:58:00 | 164       | 10.138   | 626.522 | -0.275  | 12.55   |
| 07/16/96 | 15:59:00 | 165       | 10.138   | 626.522 | -0.275  | 12.55   |
| 07/16/96 | 16:00:00 | 166       | 10.138   | 626.522 | -0.275  | 12.55   |
| 07/16/96 | 16:01:00 | 167       | 10.138   | 626.522 | -0.275  | 12.55   |
| 07/16/96 | 16:02:00 | 168       | 10.138   | 626.522 | -0.275  | 12.55   |
| 07/16/96 | 16:03:00 | 169       | 10.14    | 626.52  | -0.277  | 12.55   |
| 07/16/96 | 16:04:00 | 170       | 10.14    | 626.52  | -0.277  | 12.55   |
| 07/16/96 | 16:05:00 | 171       | 10.14    | 626.52  | -0.277  | 12.55   |
| 07/16/96 | 16:06:00 | 172       | 10.14    | 626.52  | -0.277  | 12.55   |
| 07/16/96 | 16:07:00 | 173       | 10.14    | 626.52  | -0.277  | 12.55   |
| 07/16/96 | 16:08:00 | 174       | 10.14    | 626.52  | -0.277  | 12.55   |
| 07/16/96 | 16:09:00 | 175       | 10.14    | 626.52  | -0.277  | 12.55   |
| 07/16/96 | 16:10:00 | 176       | 10.14    | 626.52  | -0.277  | 12.55   |
| 07/16/96 | 16:11:00 | 177       | 10.142   | 626.518 | -0.279  | 12.55   |
| 07/16/96 | 16:12:00 | 178       | 10.142   | 626.518 | -0.279  | 12.55   |
| 07/16/96 | 16:13:00 | 179       | 10.142   | 626.518 | -0.279  | 12.55   |
| 07/16/96 | 16:14:00 | 180       | 10.142   | 626.518 | -0.279  | 12.55   |
| 07/16/96 | 16:15:00 | 181       | 10.142   | 626.518 | -0.279  | 12.55   |
| 07/16/96 | 16:16:00 | 182       | 10.145   | 626.515 | -0.282  | 12.55   |
| 07/16/96 | 16:17:00 | 183       | 10.145   | 626.515 | -0.282  | 12.55   |
| 07/16/96 | 16:18:00 | 184       | 10.142   | 626.518 | -0.279  | 12.55   |
| 07/16/96 | 16:19:00 | 185       | 10.142   | 626.518 | -0.279  | 12.56   |
| 07/16/96 | 16:20:00 | 186       | 10.145   | 626.515 | -0.282  | 12.55   |
| 07/16/96 | 16:21:00 | 187       | 10.145   | 626.515 | -0.282  | 12.56   |
| 07/16/96 | 16:22:00 | 188       | 10.145   | 626.515 | -0.282  | 12.55   |
| 07/16/96 | 16:23:00 | 189       | 10.147   | 626.513 | -0.284  | 12.55   |
| 07/16/96 | 16:24:00 | 190       | 10.145   | 626.515 | -0.282  | 12.55   |
| 07/16/96 | 16:25:00 | 191       | 10.145   | 626.515 | -0.282  | 12.55   |
| 07/16/96 | 16:26:00 | 192       | 10.147   | 626.513 | -0.284  | 12.55   |
| 07/16/96 | 16:27:00 | 193       | 10.147   | 626.513 | -0.284  | 12.55   |
| 07/16/96 | 16:28:00 | 194       | 10.147   | 626.513 | -0.284  | 12.55   |
| 07/16/96 | 16:29:00 | 195       | 10.147   | 626.513 | -0.284  | 12.55   |
| 07/16/96 | 16:30:00 | 196       | 10.147   | 626.513 | -0.284  | 12.56   |
| 07/16/96 | 16:31:00 | 197       | 10.147   | 626.513 | -0.284  | 12.55   |
| 07/16/96 | 16:32:00 | 198       | 10.149   | 626.511 | -0.286  | 12.55   |
| 07/16/96 | 16:33:00 | 199       | 10.149   | 626.511 | -0.286  | 12.55   |

| Date     | Time     | Elapsed T | Feet H2O |         | Delta H | Celsius |
|----------|----------|-----------|----------|---------|---------|---------|
| 07/16/96 | 16:34:00 | 200       | 10.149   | 626.511 | -0.286  | 12.55   |
| 07/16/96 | 16:35:00 | 201       | 10.149   | 626.511 | -0.286  | 12.55   |
| 07/16/96 | 16:36:00 | 202       | 10.149   | 626.511 | -0.286  | 12.55   |
| 07/16/96 | 16:37:00 | 203       | 10.149   | 626.511 | -0.286  | 12.56   |
| 07/16/96 | 16:38:00 | 204       | 10.152   | 626.508 | -0.289  | 12.56   |
| 07/16/96 | 16:39:00 | 205       | 10.149   | 626.511 | -0.286  | 12.55   |
| 07/16/96 | 16:40:00 | 206       | 10.152   | 626.508 | -0.289  | 12.55   |
| 07/16/96 | 16:41:00 | 207       | 10.152   | 626.508 | -0.289  | 12.55   |
| 07/16/96 | 16:42:00 | 208       | 10.149   | 626.511 | -0.286  | 12.55   |
| 07/16/96 | 16:43:00 | 209       | 10.152   | 626.508 | -0.289  | 12.55   |
| 07/16/96 | 16:44:00 | 210       | 10.152   | 626.508 | -0.289  | 12.55   |
| 07/16/96 | 16:45:00 | 211       | 10.152   | 626.508 | -0.289  | 12.55   |
| 07/16/96 | 16:46:00 | 212       | 10.152   | 626.508 | -0.289  | 12.55   |
| 07/16/96 | 16:47:00 | 213       | 10.152   | 626.508 | -0.289  | 12.56   |
| 07/16/96 | 16:48:00 | 214       | 10.152   | 626.508 | -0.289  | 12.55   |
| 07/16/96 | 16:49:00 | 215       | 10.154   | 626.506 | -0.291  | 12.56   |
| 07/16/96 | 16:50:00 | 216       | 10.152   | 626.508 | -0.289  | 12.55   |
| 07/16/96 | 16:51:00 | 217       | 10.154   | 626.506 | -0.291  | 12.56   |
| 07/16/96 | 16:52:00 | 218       | 10.156   | 626.504 | -0.293  | 12.55   |
| 07/16/96 | 16:53:00 | 219       | 10.156   | 626.504 | -0.293  | 12.55   |
| 07/16/96 | 16:54:00 | 220       | 10.154   | 626.506 | -0.291  | 12.55   |
| 07/16/96 | 16:55:00 | 221       | 10.154   | 626.506 | -0.291  | 12.55   |
| 07/16/96 | 16:56:00 | 222       | 10.156   | 626.504 | -0.293  | 12.55   |
| 07/16/96 | 16:57:00 | 223       | 10.154   | 626.506 | -0.291  | 12.55   |
| 07/16/96 | 16:58:00 | 224       | 10.156   | 626.504 | -0.293  | 12.56   |
| 07/16/96 | 16:59:00 | 225       | 10.154   | 626.506 | -0.291  | 12.55   |
| 07/16/96 | 17:00:00 | 226       | 10.156   | 626.504 | -0.293  | 12.56   |
| 07/16/96 | 17:01:00 | 227       | 10.156   | 626.504 | -0.293  | 12.56   |
| 07/16/96 | 17:02:00 | 228       | 10.156   | 626.504 | -0.293  | 12.56   |
| 07/16/96 | 17:03:00 | 229       | 10.158   | 626.502 | -0.295  | 12.55   |
| 07/16/96 | 17:04:00 | 230       | 10.158   | 626.502 | -0.295  | 12.55   |
| 07/16/96 | 17:05:00 | 231       | 10.158   | 626.502 | -0.295  | 12.56   |
| 07/16/96 | 17:06:00 | 232       | 10.158   | 626.502 | -0.295  | 12.56   |
| 07/16/96 | 17:07:00 | 233       | 10.158   | 626.502 | -0.295  | 12.56   |
| 07/16/96 | 17:08:00 | 234       | 10.158   | 626.502 | -0.295  | 12.55   |
| 07/16/96 | 17:09:00 | 235       | 10.158   | 626.502 | -0.295  | 12.55   |
| 07/16/96 | 17:10:00 | 236       | 10.158   | 626.502 | -0.295  | 12.56   |
| 07/16/96 | 17:11:00 | 237       | 10.158   | 626.502 | -0.295  | 12.56   |
| 07/16/96 | 17:12:00 | 238       | 10.158   | 626.502 | -0.295  | 12.56   |
| 07/16/96 | 17:13:00 | 239       | 10.158   | 626.502 | -0.295  | 12.55   |
| 07/16/96 | 17:14:00 | 240       | 10.158   | 626.502 | -0.295  | 12.56   |
| 07/16/96 | 17:15:00 | 241       | 10.158   | 626.502 | -0.295  | 12.56   |
| 07/16/96 | 17:16:00 | 242       | 10.158   | 626.502 | -0.295  | 12.56   |
| 07/16/96 | 17:17:00 | 243       | 10.158   | 626.502 | -0.295  | 12.55   |
| 07/16/96 | 17:18:00 | 244       | 10.161   | 626.499 | -0.298  | 12.56   |
| 07/16/96 | 17:19:00 | 245       | 10.161   | 626.499 | -0.298  | 12.56   |
| 07/16/96 | 17:20:00 | 246       | 10.161   | 626.499 | -0.298  | 12.56   |
| 07/16/96 | 17:21:00 | 247       | 10.161   | 626.499 | -0.298  | 12.55   |
| 07/16/96 | 17:22:00 | 248       | 10.163   | 626.497 | -0.3    | 12.56   |
| 07/16/96 | 17:23:00 | 249       | 10.163   | 626.497 | -0.3    | 12.56   |

| Date     | Time     | Elapsed T | Feet H2O |         | Delta H | Celsius |
|----------|----------|-----------|----------|---------|---------|---------|
| 07/16/96 | 17:24:00 | 250       | 10.161   | 626.499 | -0.298  | 12.55   |
| 07/16/96 | 17:25:00 | 251       | 10.163   | 626.497 | -0.3    | 12.56   |
| 07/16/96 | 17:26:00 | 252       | 10.165   | 626.495 | -0.302  | 12.56   |
| 07/16/96 | 17:27:00 | 253       | 10.165   | 626.495 | -0.302  | 12.56   |
| 07/16/96 | 17:28:00 | 254       | 10.165   | 626.495 | -0.302  | 12.55   |
| 07/16/96 | 17:29:00 | 255       | 10.165   | 626.495 | -0.302  | 12.56   |
| 07/16/96 | 17:30:00 | 256       | 10.165   | 626.495 | -0.302  | 12.55   |
| 07/16/96 | 17:31:00 | 257       | 10.165   | 626.495 | -0.302  | 12.55   |
| 07/16/96 | 17:32:00 | 258       | 10.165   | 626.495 | -0.302  | 12.56   |
| 07/16/96 | 17:33:00 | 259       | 10.168   | 626.492 | -0.305  | 12.56   |
| 07/16/96 | 17:34:00 | 260       | 10.168   | 626.492 | -0.305  | 12.56   |
| 07/16/96 | 17:35:00 | 261       | 10.165   | 626.495 | -0.302  | 12.55   |
| 07/16/96 | 17:36:00 | 262       | 10.168   | 626.492 | -0.305  | 12.56   |
| 07/16/96 | 17:37:00 | 263       | 10.168   | 626.492 | -0.305  | 12.56   |
| 07/16/96 | 17:38:00 | 264       | 10.168   | 626.492 | -0.305  | 12.56   |
| 07/16/96 | 17:39:00 | 265       | 10.168   | 626.492 | -0.305  | 12.56   |
| 07/16/96 | 17:40:00 | 266       | 10.168   | 626.492 | -0.305  | 12.56   |
| 07/16/96 | 17:41:00 | 267       | 10.168   | 626.492 | -0.305  | 12.56   |
| 07/16/96 | 17:42:00 | 268       | 10.168   | 626.492 | -0.305  | 12.56   |
| 07/16/96 | 17:43:00 | 269       | 10.168   | 626.492 | -0.305  | 12.56   |
| 07/16/96 | 17:44:00 | 270       | 10.168   | 626.492 | -0.305  | 12.56   |
| 07/16/96 | 17:45:00 | 271       | 10.168   | 626.492 | -0.305  | 12.56   |
| 07/16/96 | 17:46:00 | 272       | 10.17    | 626.49  | -0.307  | 12.55   |
| 07/16/96 | 17:47:00 | 273       | 10.168   | 626.492 | -0.305  | 12.56   |
| 07/16/96 | 17:48:00 | 274       | 10.168   | 626.492 | -0.305  | 12.56   |
| 07/16/96 | 17:49:00 | 275       | 10.168   | 626.492 | -0.305  | 12.56   |
| 07/16/96 | 17:50:00 | 276       | 10.168   | 626.492 | -0.305  | 12.56   |
| 07/16/96 | 17:51:00 | 277       | 10.17    | 626.49  | -0.307  | 12.56   |
| 07/16/96 | 17:52:00 | 278       | 10.17    | 626.49  | -0.307  | 12.56   |
| 07/16/96 | 17:53:00 | 279       | 10.17    | 626.49  | -0.307  | 12.56   |
| 07/16/96 | 17:54:00 | 280       | 10.172   | 626.488 | -0.309  | 12.56   |
| 07/16/96 | 17:55:00 | 281       | 10.172   | 626.488 | -0.309  | 12.55   |
| 07/16/96 | 17:56:00 | 282       | 10.172   | 626.488 | -0.309  | 12.56   |
| 07/16/96 | 17:57:00 | 283       | 10.175   | 626.485 | -0.312  | 12.56   |
| 07/16/96 | 17:58:00 | 284       | 10.175   | 626.485 | -0.312  | 12.56   |
| 07/16/96 | 17:59:00 | 285       | 10.175   | 626.485 | -0.312  | 12.56   |
| 07/16/96 | 18:00:00 | 286       | 10.175   | 626.485 | -0.312  | 12.56   |
| 07/16/96 | 18:01:00 | 287       | 10.175   | 626.485 | -0.312  | 12.56   |
| 07/16/96 | 18:02:00 | 288       | 10.177   | 626.483 | -0.314  | 12.56   |
| 07/16/96 | 18:03:00 | 289       | 10.177   | 626.483 | -0.314  | 12.56   |
| 07/16/96 | 18:04:00 | 290       | 10.179   | 626.481 | -0.316  | 12.56   |
| 07/16/96 | 18:05:00 | 291       | 10.179   | 626.481 | -0.316  | 12.56   |
| 07/16/96 | 18:06:00 | 292       | 10.179   | 626.481 | -0.316  | 12.56   |
| 07/16/96 | 18:07:00 | 293       | 10.179   | 626.481 | -0.316  | 12.56   |
| 07/16/96 | 18:08:00 | 294       | 10.179   | 626.481 | -0.316  | 12.56   |
| 07/16/96 | 18:09:00 | 295       | 10.179   | 626.481 | -0.316  | 12.55   |
| 07/16/96 | 18:10:00 | 296       | 10.179   | 626.481 | -0.316  | 12.56   |
| 07/16/96 | 18:11:00 | 297       | 10.179   | 626.481 | -0.316  | 12.56   |
| 07/16/96 | 18:12:00 | 298       | 10.179   | 626.481 | -0.316  | 12.56   |
| 07/16/96 | 18:13:00 | 299       | 10.179   | 626.481 | -0.316  | 12.56   |

| Date     | Time     | Elapsed T | Feet H2O |         | Delta H | Celsius |
|----------|----------|-----------|----------|---------|---------|---------|
| 07/16/96 | 18:14:00 | 300       | 10.179   | 626.481 | -0.316  | 12.56   |
| 07/16/96 | 18:15:00 | 301       | 10.182   | 626.478 | -0.319  | 12.56   |
| 07/16/96 | 18:16:00 | 302       | 10.182   | 626.478 | -0.319  | 12.56   |
| 07/16/96 | 18:17:00 | 303       | 10.182   | 626.478 | -0.319  | 12.56   |
| 07/16/96 | 18:18:00 | 304       | 10.182   | 626.478 | -0.319  | 12.56   |
| 07/16/96 | 18:19:00 | 305       | 10.184   | 626.476 | -0.321  | 12.56   |
| 07/16/96 | 18:20:00 | 306       | 10.184   | 626.476 | -0.321  | 12.56   |
| 07/16/96 | 18:21:00 | 307       | 10.184   | 626.476 | -0.321  | 12.56   |
| 07/16/96 | 18:22:00 | 308       | 10.182   | 626.478 | -0.319  | 12.56   |
| 07/16/96 | 18:23:00 | 309       | 10.182   | 626.478 | -0.319  | 12.56   |
| 07/16/96 | 18:24:00 | 310       | 10.182   | 626.478 | -0.319  | 12.56   |
| 07/16/96 | 18:25:00 | 311       | 10.182   | 626.478 | -0.319  | 12.56   |
| 07/16/96 | 18:26:00 | 312       | 10.184   | 626.476 | -0.321  | 12.56   |
| 07/16/96 | 18:27:00 | 313       | 10.182   | 626.478 | -0.319  | 12.56   |
| 07/16/96 | 18:28:00 | 314       | 10.184   | 626.476 | -0.321  | 12.57   |
| 07/16/96 | 18:29:00 | 315       | 10.184   | 626.476 | -0.321  | 12.56   |
| 07/16/96 | 18:30:00 | 316       | 10.182   | 626.478 | -0.319  | 12.56   |
| 07/16/96 | 18:31:00 | 317       | 10.184   | 626.476 | -0.321  | 12.56   |
| 07/16/96 | 18:32:00 | 318       | 10.182   | 626.478 | -0.319  | 12.56   |
| 07/16/96 | 18:33:00 | 319       | 10.184   | 626.476 | -0.321  | 12.56   |
| 07/16/96 | 18:34:00 | 320       | 10.184   | 626.476 | -0.321  | 12.56   |
| 07/16/96 | 18:35:00 | 321       | 10.184   | 626.476 | -0.321  | 12.56   |
| 07/16/96 | 18:36:00 | 322       | 10.184   | 626.476 | -0.321  | 12.56   |
| 07/16/96 | 18:37:00 | 323       | 10.182   | 626.478 | -0.319  | 12.56   |
| 07/16/96 | 18:38:00 | 324       | 10.184   | 626.476 | -0.321  | 12.56   |
| 07/16/96 | 18:39:00 | 325       | 10.184   | 626.476 | -0.321  | 12.56   |
| 07/16/96 | 18:40:00 | 326       | 10.184   | 626.476 | -0.321  | 12.56   |
| 07/16/96 | 18:41:00 | 327       | 10.184   | 626.476 | -0.321  | 12.56   |
| 07/16/96 | 18:42:00 | 328       | 10.184   | 626.476 | -0.321  | 12.56   |
| 07/16/96 | 18:43:00 | 329       | 10.184   | 626.476 | -0.321  | 12.57   |
| 07/16/96 | 18:44:00 | 330       | 10.184   | 626.476 | -0.321  | 12.56   |
| 07/16/96 | 18:45:00 | 331       | 10.186   | 626.474 | -0.323  | 12.56   |
| 07/16/96 | 18:46:00 | 332       | 10.186   | 626.474 | -0.323  | 12.56   |
| 07/16/96 | 18:47:00 | 333       | 10.186   | 626.474 | -0.323  | 12.56   |
| 07/16/96 | 18:48:00 | 334       | 10.188   | 626.472 | -0.325  | 12.56   |
| 07/16/96 | 18:49:00 | 335       | 10.188   | 626.472 | -0.325  | 12.56   |
| 07/16/96 | 18:50:00 | 336       | 10.188   | 626.472 | -0.325  | 12.56   |
| 07/16/96 | 18:51:00 | 337       | 10.191   | 626.469 | -0.328  | 12.56   |
| 07/16/96 | 18:52:00 | 338       | 10.188   | 626.472 | -0.325  | 12.56   |
| 07/16/96 | 18:53:00 | 339       | 10.184   | 626.476 | -0.321  | 12.56   |
| 07/16/96 | 18:54:00 | 340       | 10.179   | 626.481 | -0.316  | 12.56   |
| 07/16/96 | 18:55:00 | 341       | 10.17    | 626.49  | -0.307  | 12.56   |
| 07/16/96 | 18:56:00 | 342       | 10.163   | 626.497 | -0.3    | 12.56   |
| 07/16/96 | 18:57:00 | 343       | 10.154   | 626.506 | -0.291  | 12.56   |
| 07/16/96 | 18:58:00 | 344       | 10.145   | 626.515 | -0.282  | 12.56   |
| 07/16/96 | 18:59:00 | 345       | 10.138   | 626.522 | -0.275  | 12.56   |
| 07/16/96 | 19:00:00 | 346       | 10.131   | 626.529 | -0.268  | 12.56   |
| 07/16/96 | 19:01:00 | 347       | 10.126   | 626.534 | -0.263  | 12.56   |
| 07/16/96 | 19:02:00 | 348       | 10.119   | 626.541 | -0.256  | 12.57   |
| 07/16/96 | 19:03:00 | 349       | 10.115   | 626.545 | -0.252  | 12.57   |

| Date     | Time     | Elapsed T | Feet H2O |         | Delta H | Celsius |
|----------|----------|-----------|----------|---------|---------|---------|
| 07/16/96 | 19:04:00 | 350       | 10.11    | 626.55  | -0.247  | 12.57   |
| 07/16/96 | 19:05:00 | 351       | 10.105   | 626.555 | -0.242  | 12.57   |
| 07/16/96 | 19:06:00 | 352       | 10.101   | 626.559 | -0.238  | 12.56   |
| 07/16/96 | 19:07:00 | 353       | 10.096   | 626.564 | -0.233  | 12.57   |
| 07/16/96 | 19:08:00 | 354       | 10.092   | 626.568 | -0.229  | 12.57   |
| 07/16/96 | 19:09:00 | 355       | 10.087   | 626.573 | -0.224  | 12.57   |
| 07/16/96 | 19:10:00 | 356       | 10.082   | 626.578 | -0.219  | 12.57   |
| 07/16/96 | 19:11:00 | 357       | 10.08    | 626.58  | -0.217  | 12.57   |
| 07/16/96 | 19:12:00 | 358       | 10.075   | 626.585 | -0.212  | 12.57   |
| 07/16/96 | 19:13:00 | 359       | 10.073   | 626.587 | -0.21   | 12.57   |
| 07/16/96 | 19:14:00 | 360       | 10.069   | 626.591 | -0.206  | 12.57   |
| 07/16/96 | 19:15:00 | 361       | 10.066   | 626.594 | -0.203  | 12.57   |
| 07/16/96 | 19:16:00 | 362       | 10.064   | 626.596 | -0.201  | 12.57   |
| 07/16/96 | 19:17:00 | 363       | 10.062   | 626.598 | -0.199  | 12.57   |
| 07/16/96 | 19:18:00 | 364       | 10.057   | 626.603 | -0.194  | 12.57   |
| 07/16/96 | 19:19:00 | 365       | 10.057   | 626.603 | -0.194  | 12.57   |
| 07/16/96 | 19:20:00 | 366       | 10.052   | 626.608 | -0.189  | 12.57   |
| 07/16/96 | 19:21:00 | 367       | 10.052   | 626.608 | -0.189  | 12.57   |
| 07/16/96 | 19:22:00 | 368       | 10.05    | 626.61  | -0.187  | 12.57   |
| 07/16/96 | 19:23:00 | 369       | 10.048   | 626.612 | -0.185  | 12.58   |
| 07/16/96 | 19:24:00 | 370       | 10.045   | 626.615 | -0.182  | 12.58   |
| 07/16/96 | 19:25:00 | 371       | 10.041   | 626.619 | -0.178  | 12.58   |
| 07/16/96 | 19:26:00 | 372       | 10.041   | 626.619 | -0.178  | 12.58   |
| 07/16/96 | 19:27:00 | 373       | 10.039   | 626.621 | -0.176  | 12.58   |
| 07/16/96 | 19:28:00 | 374       | 10.039   | 626.621 | -0.176  | 12.58   |
| 07/16/96 | 19:29:00 | 375       | 10.036   | 626.624 | -0.173  | 12.58   |
| 07/16/96 | 19:30:00 | 376       | 10.034   | 626.626 | -0.171  | 12.58   |
| 07/16/96 | 19:31:00 | 377       | 10.032   | 626.628 | -0.169  | 12.58   |
| 07/16/96 | 19:32:00 | 378       | 10.029   | 626.631 | -0.166  | 12.58   |
| 07/16/96 | 19:33:00 | 379       | 10.027   | 626.633 | -0.164  | 12.58   |
| 07/16/96 | 19:34:00 | 380       | 10.025   | 626.635 | -0.162  | 12.58   |
| 07/16/96 | 19:35:00 | 381       | 10.022   | 626.638 | -0.159  | 12.58   |
| 07/16/96 | 19:36:00 | 382       | 10.022   | 626.638 | -0.159  | 12.58   |
| 07/16/96 | 19:37:00 | 383       | 10.02    | 626.64  | -0.157  | 12.58   |
| 07/16/96 | 19:38:00 | 384       | 10.02    | 626.64  | -0.157  | 12.58   |
| 07/16/96 | 19:39:00 | 385       | 10.02    | 626.64  | -0.157  | 12.58   |
| 07/16/96 | 19:40:00 | 386       | 10.018   | 626.642 | -0.155  | 12.58   |
| 07/16/96 | 19:41:00 | 387       | 10.018   | 626.642 | -0.155  | 12.58   |
| 07/16/96 | 19:42:00 | 388       | 10.015   | 626.645 | -0.152  | 12.58   |
| 07/16/96 | 19:43:00 | 389       | 10.015   | 626.645 | -0.152  | 12.58   |
| 07/16/96 | 19:44:00 | 390       | 10.015   | 626.645 | -0.152  | 12.58   |
| 07/16/96 | 19:45:00 | 391       | 10.013   | 626.647 | -0.15   | 12.58   |
| 07/16/96 | 19:46:00 | 392       | 10.013   | 626.647 | -0.15   | 12.58   |
| 07/16/96 | 19:47:00 | 393       | 10.011   | 626.649 | -0.148  | 12.58   |
| 07/16/96 | 19:48:00 | 394       | 10.013   | 626.647 | -0.15   | 12.58   |
| 07/16/96 | 19:49:00 | 395       | 10.013   | 626.647 | -0.15   | 12.58   |
| 07/16/96 | 19:50:00 | 396       | 10.013   | 626.647 | -0.15   | 12.58   |
| 07/16/96 | 19:51:00 | 397       | 10.011   | 626.649 | -0.148  | 12.58   |
| 07/16/96 | 19:52:00 | 398       | 10.011   | 626.649 | -0.148  | 12.59   |
| 07/16/96 | 19:53:00 | 399       | 10.009   | 626.651 | -0.146  | 12.58   |

| Date     | Time     | Elapsed T | Feet H2O |         | Delta H | Celsius |
|----------|----------|-----------|----------|---------|---------|---------|
| 07/16/96 | 19:54:00 | 400       | 10.009   | 626.651 | -0.146  | 12.58   |
| 07/16/96 | 19:55:00 | 401       | 10.009   | 626.651 | -0.146  | 12.58   |
| 07/16/96 | 19:56:00 | 402       | 10.009   | 626.651 | -0.146  | 12.58   |
| 07/16/96 | 19:57:00 | 403       | 10.009   | 626.651 | -0.146  | 12.58   |
| 07/16/96 | 19:58:00 | 404       | 10.009   | 626.651 | -0.146  | 12.58   |
| 07/16/96 | 19:59:00 | 405       | 10.009   | 626.651 | -0.146  | 12.58   |
| 07/16/96 | 20:00:00 | 406       | 10.006   | 626.654 | -0.143  | 12.58   |
| 07/16/96 | 20:01:00 | 407       | 10.006   | 626.654 | -0.143  | 12.59   |
| 07/16/96 | 20:02:00 | 408       | 10.006   | 626.654 | -0.143  | 12.59   |
| 07/16/96 | 20:03:00 | 409       | 10.004   | 626.656 | -0.141  | 12.58   |
| 07/16/96 | 20:04:00 | 410       | 10.004   | 626.656 | -0.141  | 12.59   |
| 07/16/96 | 20:05:00 | 411       | 10.004   | 626.656 | -0.141  | 12.59   |
| 07/16/96 | 20:06:00 | 412       | 10.002   | 626.658 | -0.139  | 12.59   |
| 07/16/96 | 20:07:00 | 413       | 10.002   | 626.658 | -0.139  | 12.58   |
| 07/16/96 | 20:08:00 | 414       | 10.002   | 626.658 | -0.139  | 12.58   |
| 07/16/96 | 20:09:00 | 415       | 10.002   | 626.658 | -0.139  | 12.58   |
| 07/16/96 | 20:10:00 | 416       | 10.002   | 626.658 | -0.139  | 12.59   |
| 07/16/96 | 20:11:00 | 417       | 9.999    | 626.661 | -0.136  | 12.59   |
| 07/16/96 | 20:12:00 | 418       | 9.999    | 626.661 | -0.136  | 12.59   |
| 07/16/96 | 20:13:00 | 419       | 9.997    | 626.663 | -0.134  | 12.58   |
| 07/16/96 | 20:14:00 | 420       | 9.999    | 626.661 | -0.136  | 12.59   |
| 07/16/96 | 20:15:00 | 421       | 9.997    | 626.663 | -0.134  | 12.59   |
| 07/16/96 | 20:16:00 | 422       | 9.997    | 626.663 | -0.134  | 12.59   |
| 07/16/96 | 20:17:00 | 423       | 9.997    | 626.663 | -0.134  | 12.59   |
| 07/16/96 | 20:18:00 | 424       | 9.997    | 626.663 | -0.134  | 12.59   |
| 07/16/96 | 20:19:00 | 425       | 9.997    | 626.663 | -0.134  | 12.59   |
| 07/16/96 | 20:20:00 | 426       | 9.997    | 626.663 | -0.134  | 12.59   |
| 07/16/96 | 20:21:00 | 427       | 9.997    | 626.663 | -0.134  | 12.59   |
| 07/16/96 | 20:22:00 | 428       | 9.997    | 626.663 | -0.134  | 12.59   |
| 07/16/96 | 20:23:00 | 429       | 9.997    | 626.663 | -0.134  | 12.59   |
| 07/16/96 | 20:24:00 | 430       | 9.995    | 626.665 | -0.132  | 12.59   |
| 07/16/96 | 20:25:00 | 431       | 9.995    | 626.665 | -0.132  | 12.59   |
| 07/16/96 | 20:26:00 | 432       | 9.995    | 626.665 | -0.132  | 12.59   |
| 07/16/96 | 20:27:00 | 433       | 9.995    | 626.665 | -0.132  | 12.59   |
| 07/16/96 | 20:28:00 | 434       | 9.995    | 626.665 | -0.132  | 12.59   |
| 07/16/96 | 20:29:00 | 435       | 9.995    | 626.665 | -0.132  | 12.59   |
| 07/16/96 | 20:30:00 | 436       | 9.995    | 626.665 | -0.132  | 12.59   |
| 07/16/96 | 20:31:00 | 437       | 9.995    | 626.665 | -0.132  | 12.59   |
| 07/16/96 | 20:32:00 | 438       | 9.995    | 626.665 | -0.132  | 12.59   |
| 07/16/96 | 20:33:00 | 439       | 9.992    | 626.668 | -0.129  | 12.59   |
| 07/16/96 | 20:34:00 | 440       | 9.992    | 626.668 | -0.129  | 12.59   |
| 07/16/96 | 20:35:00 | 441       | 9.992    | 626.668 | -0.129  | 12.59   |
| 07/16/96 | 20:36:00 | 442       | 9.992    | 626.668 | -0.129  | 12.59   |
| 07/16/96 | 20:37:00 | 443       | 9.99     | 626.67  | -0.127  | 12.59   |
| 07/16/96 | 20:38:00 | 444       | 9.99     | 626.67  | -0.127  | 12.59   |
| 07/16/96 | 20:39:00 | 445       | 9.99     | 626.67  | -0.127  | 12.59   |
| 07/16/96 | 20:40:00 | 446       | 9.99     | 626.67  | -0.127  | 12.59   |
| 07/16/96 | 20:41:00 | 447       | 9.99     | 626.67  | -0.127  | 12.6    |
| 07/16/96 | 20:42:00 | 448       | 9.99     | 626.67  | -0.127  | 12.59   |
| 07/16/96 | 20:43:00 | 449       | 9.99     | 626.67  | -0.127  | 12.59   |

| Date     | Time     | Elapsed T | Feet H2O |         | Delta H | Celsius |
|----------|----------|-----------|----------|---------|---------|---------|
| 07/16/96 | 20:44:00 | 450       | 9.988    | 626.672 | -0.125  | 12.59   |
| 07/16/96 | 20:45:00 | 451       | 9.988    | 626.672 | -0.125  | 12.59   |
| 07/16/96 | 20:46:00 | 452       | 9.99     | 626.67  | -0.127  | 12.6    |
| 07/16/96 | 20:47:00 | 453       | 9.988    | 626.672 | -0.125  | 12.6    |
| 07/16/96 | 20:48:00 | 454       | 9.988    | 626.672 | -0.125  | 12.6    |
| 07/16/96 | 20:49:00 | 455       | 9.99     | 626.67  | -0.127  | 12.6    |
| 07/16/96 | 20:50:00 | 456       | 9.99     | 626.67  | -0.127  | 12.59   |
| 07/16/96 | 20:51:00 | 457       | 9.988    | 626.672 | -0.125  | 12.6    |
| 07/16/96 | 20:52:00 | 458       | 9.988    | 626.672 | -0.125  | 12.6    |
| 07/16/96 | 20:53:00 | 459       | 9.985    | 626.675 | -0.122  | 12.6    |
| 07/16/96 | 20:54:00 | 460       | 9.985    | 626.675 | -0.122  | 12.59   |
| 07/16/96 | 20:55:00 | 461       | 9.985    | 626.675 | -0.122  | 12.6    |
| 07/16/96 | 20:56:00 | 462       | 9.985    | 626.675 | -0.122  | 12.59   |
| 07/16/96 | 20:57:00 | 463       | 9.985    | 626.675 | -0.122  | 12.6    |
| 07/16/96 | 20:58:00 | 464       | 9.985    | 626.675 | -0.122  | 12.6    |
| 07/16/96 | 20:59:00 | 465       | 9.983    | 626.677 | -0.12   | 12.6    |
| 07/16/96 | 21:00:00 | 466       | 9.983    | 626.677 | -0.12   | 12.6    |
| 07/16/96 | 21:01:00 | 467       | 9.985    | 626.675 | -0.122  | 12.6    |
| 07/16/96 | 21:02:00 | 468       | 9.983    | 626.677 | -0.12   | 12.6    |
| 07/16/96 | 21:03:00 | 469       | 9.983    | 626.677 | -0.12   | 12.6    |
| 07/16/96 | 21:04:00 | 470       | 9.985    | 626.675 | -0.122  | 12.6    |
| 07/16/96 | 21:05:00 | 471       | 9.983    | 626.677 | -0.12   | 12.6    |
| 07/16/96 | 21:06:00 | 472       | 9.983    | 626.677 | -0.12   | 12.6    |
| 07/16/96 | 21:07:00 | 473       | 9.983    | 626.677 | -0.12   | 12.6    |
| 07/16/96 | 21:08:00 | 474       | 9.983    | 626.677 | -0.12   | 12.6    |
| 07/16/96 | 21:09:00 | 475       | 9.983    | 626.677 | -0.12   | 12.59   |
| 07/16/96 | 21:10:00 | 476       | 9.981    | 626.679 | -0.118  | 12.6    |
| 07/16/96 | 21:11:00 | 477       | 9.981    | 626.679 | -0.118  | 12.6    |
| 07/16/96 | 21:12:00 | 478       | 9.981    | 626.679 | -0.118  | 12.6    |
| 07/16/96 | 21:13:00 | 479       | 9.981    | 626.679 | -0.118  | 12.6    |
| 07/16/96 | 21:14:00 | 480       | 9.981    | 626.679 | -0.118  | 12.6    |
| 07/16/96 | 21:15:00 | 481       | 9.981    | 626.679 | -0.118  | 12.6    |
| 07/16/96 | 21:16:00 | 482       | 9.981    | 626.679 | -0.118  | 12.6    |
| 07/16/96 | 21:17:00 | 483       | 9.981    | 626.679 | -0.118  | 12.6    |
| 07/16/96 | 21:18:00 | 484       | 9.981    | 626.679 | -0.118  | 12.6    |
| 07/16/96 | 21:19:00 | 485       | 9.981    | 626.679 | -0.118  | 12.6    |
| 07/16/96 | 21:20:00 | 486       | 9.981    | 626.679 | -0.118  | 12.6    |
| 07/16/96 | 21:21:00 | 487       | 9.981    | 626.679 | -0.118  | 12.6    |
| 07/16/96 | 21:22:00 | 488       | 9.981    | 626.679 | -0.118  | 12.6    |
| 07/16/96 | 21:23:00 | 489       | 9.981    | 626.679 | -0.118  | 12.6    |
| 07/16/96 | 21:24:00 | 490       | 9.981    | 626.679 | -0.118  | 12.6    |
| 07/16/96 | 21:25:00 | 491       | 9.981    | 626.679 | -0.118  | 12.6    |
| 07/16/96 | 21:26:00 | 492       | 9.981    | 626.679 | -0.118  | 12.6    |
| 07/16/96 | 21:27:00 | 493       | 9.981    | 626.679 | -0.118  | 12.6    |
| 07/16/96 | 21:28:00 | 494       | 9.981    | 626.679 | -0.118  | 12.6    |
| 07/16/96 | 21:29:00 | 495       | 9.981    | 626.679 | -0.118  | 12.6    |
| 07/16/96 | 21:30:00 | 496       | 9.981    | 626.679 | -0.118  | 12.6    |
| 07/16/96 | 21:31:00 | 497       | 9.981    | 626.679 | -0.118  | 12.61   |
| 07/16/96 | 21:32:00 | 498       | 9.981    | 626.679 | -0.118  | 12.6    |
| 07/16/96 | 21:33:00 | 499       | 9.981    | 626.679 | -0.118  | 12.6    |

| Date     | Time     | Elapsed T | Feet H2O |         | Delta H | Celsius |
|----------|----------|-----------|----------|---------|---------|---------|
| 07/16/96 | 21:34:00 | 500       | 9.981    | 626.679 | -0.118  | 12.6    |
| 07/16/96 | 21:35:00 | 501       | 9.981    | 626.679 | -0.118  | 12.6    |
| 07/16/96 | 21:36:00 | 502       | 9.981    | 626.679 | -0.118  | 12.6    |
| 07/16/96 | 21:37:00 | 503       | 9.981    | 626.679 | -0.118  | 12.6    |
| 07/16/96 | 21:38:00 | 504       | 9.981    | 626.679 | -0.118  | 12.6    |
| 07/16/96 | 21:39:00 | 505       | 9.981    | 626.679 | -0.118  | 12.61   |
| 07/16/96 | 21:40:00 | 506       | 9.981    | 626.679 | -0.118  | 12.6    |
| 07/16/96 | 21:41:00 | 507       | 9.981    | 626.679 | -0.118  | 12.6    |
| 07/16/96 | 21:42:00 | 508       | 9.981    | 626.679 | -0.118  | 12.61   |
| 07/16/96 | 21:43:00 | 509       | 9.981    | 626.679 | -0.118  | 12.6    |
| 07/16/96 | 21:44:00 | 510       | 9.981    | 626.679 | -0.118  | 12.6    |
| 07/16/96 | 21:45:00 | 511       | 9.981    | 626.679 | -0.118  | 12.6    |
| 07/16/96 | 21:46:00 | 512       | 9.981    | 626.679 | -0.118  | 12.61   |
| 07/16/96 | 21:47:00 | 513       | 9.981    | 626.679 | -0.118  | 12.61   |
| 07/16/96 | 21:48:00 | 514       | 9.981    | 626.679 | -0.118  | 12.6    |
| 07/16/96 | 21:49:00 | 515       | 9.981    | 626.679 | -0.118  | 12.6    |
| 07/16/96 | 21:50:00 | 516       | 9.981    | 626.679 | -0.118  | 12.6    |
| 07/16/96 | 21:51:00 | 517       | 9.979    | 626.681 | -0.116  | 12.61   |
| 07/16/96 | 21:52:00 | 518       | 9.979    | 626.681 | -0.116  | 12.61   |
| 07/16/96 | 21:53:00 | 519       | 9.979    | 626.681 | -0.116  | 12.61   |
| 07/16/96 | 21:54:00 | 520       | 9.979    | 626.681 | -0.116  | 12.61   |
| 07/16/96 | 21:55:00 | 521       | 9.979    | 626.681 | -0.116  | 12.61   |
| 07/16/96 | 21:56:00 | 522       | 9.979    | 626.681 | -0.116  | 12.61   |
| 07/16/96 | 21:57:00 | 523       | 9.976    | 626.684 | -0.113  | 12.61   |
| 07/16/96 | 21:58:00 | 524       | 9.976    | 626.684 | -0.113  | 12.61   |
| 07/16/96 | 21:59:00 | 525       | 9.976    | 626.684 | -0.113  | 12.61   |
| 07/16/96 | 22:00:00 | 526       | 9.976    | 626.684 | -0.113  | 12.61   |
| 07/16/96 | 22:01:00 | 527       | 9.976    | 626.684 | -0.113  | 12.61   |
| 07/16/96 | 22:02:00 | 528       | 9.976    | 626.684 | -0.113  | 12.61   |
| 07/16/96 | 22:03:00 | 529       | 9.976    | 626.684 | -0.113  | 12.61   |
| 07/16/96 | 22:04:00 | 530       | 9.976    | 626.684 | -0.113  | 12.61   |
| 07/16/96 | 22:05:00 | 531       | 9.976    | 626.684 | -0.113  | 12.61   |
| 07/16/96 | 22:06:00 | 532       | 9.976    | 626.684 | -0.113  | 12.61   |
| 07/16/96 | 22:07:00 | 533       | 9.976    | 626.684 | -0.113  | 12.6    |
| 07/16/96 | 22:08:00 | 534       | 9.976    | 626.684 | -0.113  | 12.61   |
| 07/16/96 | 22:09:00 | 535       | 9.976    | 626.684 | -0.113  | 12.61   |
| 07/16/96 | 22:10:00 | 536       | 9.976    | 626.684 | -0.113  | 12.6    |
| 07/16/96 | 22:11:00 | 537       | 9.976    | 626.684 | -0.113  | 12.6    |
| 07/16/96 | 22:12:00 | 538       | 9.976    | 626.684 | -0.113  | 12.61   |
| 07/16/96 | 22:13:00 | 539       | 9.976    | 626.684 | -0.113  | 12.61   |
| 07/16/96 | 22:14:00 | 540       | 9.979    | 626.681 | -0.116  | 12.6    |
| 07/16/96 | 22:15:00 | 541       | 9.976    | 626.684 | -0.113  | 12.61   |
| 07/16/96 | 22:16:00 | 542       | 9.976    | 626.684 | -0.113  | 12.61   |
| 07/16/96 | 22:17:00 | 543       | 9.976    | 626.684 | -0.113  | 12.61   |
| 07/16/96 | 22:18:00 | 544       | 9.976    | 626.684 | -0.113  | 12.61   |
| 07/16/96 | 22:19:00 | 545       | 9.976    | 626.684 | -0.113  | 12.61   |
| 07/16/96 | 22:20:00 | 546       | 9.976    | 626.684 | -0.113  | 12.61   |
| 07/16/96 | 22:21:00 | 547       | 9.974    | 626.686 | -0.111  | 12.61   |
| 07/16/96 | 22:22:00 | 548       | 9.974    | 626.686 | -0.111  | 12.61   |
| 07/16/96 | 22:23:00 | 549       | 9.974    | 626.686 | -0.111  | 12.61   |

| Date     | Time     | Elapsed T | Feet H2O |         | Delta H | Celsius |
|----------|----------|-----------|----------|---------|---------|---------|
| 07/16/96 | 22:24:00 | 550       | 9.974    | 626.686 | -0.111  | 12.61   |
| 07/16/96 | 22:25:00 | 551       | 9.974    | 626.686 | -0.111  | 12.61   |
| 07/16/96 | 22:26:00 | 552       | 9.974    | 626.686 | -0.111  | 12.61   |
| 07/16/96 | 22:27:00 | 553       | 9.974    | 626.686 | -0.111  | 12.61   |
| 07/16/96 | 22:28:00 | 554       | 9.974    | 626.686 | -0.111  | 12.61   |
| 07/16/96 | 22:29:00 | 555       | 9.974    | 626.686 | -0.111  | 12.61   |
| 07/16/96 | 22:30:00 | 556       | 9.974    | 626.686 | -0.111  | 12.61   |
| 07/16/96 | 22:31:00 | 557       | 9.972    | 626.688 | -0.109  | 12.61   |
| 07/16/96 | 22:32:00 | 558       | 9.974    | 626.686 | -0.111  | 12.61   |
| 07/16/96 | 22:33:00 | 559       | 9.972    | 626.688 | -0.109  | 12.61   |
| 07/16/96 | 22:34:00 | 560       | 9.972    | 626.688 | -0.109  | 12.61   |
| 07/16/96 | 22:35:00 | 561       | 9.974    | 626.686 | -0.111  | 12.61   |
| 07/16/96 | 22:36:00 | 562       | 9.974    | 626.686 | -0.111  | 12.61   |
| 07/16/96 | 22:37:00 | 563       | 9.974    | 626.686 | -0.111  | 12.61   |
| 07/16/96 | 22:38:00 | 564       | 9.974    | 626.686 | -0.111  | 12.61   |
| 07/16/96 | 22:39:00 | 565       | 9.972    | 626.688 | -0.109  | 12.61   |
| 07/16/96 | 22:40:00 | 566       | 9.974    | 626.686 | -0.111  | 12.61   |
| 07/16/96 | 22:41:00 | 567       | 9.974    | 626.686 | -0.111  | 12.61   |
| 07/16/96 | 22:42:00 | 568       | 9.974    | 626.686 | -0.111  | 12.61   |
| 07/16/96 | 22:43:00 | 569       | 9.974    | 626.686 | -0.111  | 12.61   |
| 07/16/96 | 22:44:00 | 570       | 9.976    | 626.684 | -0.113  | 12.61   |
| 07/16/96 | 22:45:00 | 571       | 9.976    | 626.684 | -0.113  | 12.61   |
| 07/16/96 | 22:46:00 | 572       | 9.976    | 626.684 | -0.113  | 12.61   |
| 07/16/96 | 22:47:00 | 573       | 9.976    | 626.684 | -0.113  | 12.61   |
| 07/16/96 | 22:48:00 | 574       | 9.979    | 626.681 | -0.116  | 12.61   |
| 07/16/96 | 22:49:00 | 575       | 9.979    | 626.681 | -0.116  | 12.61   |
| 07/16/96 | 22:50:00 | 576       | 9.976    | 626.684 | -0.113  | 12.62   |
| 07/16/96 | 22:51:00 | 577       | 9.976    | 626.684 | -0.113  | 12.61   |
| 07/16/96 | 22:52:00 | 578       | 9.976    | 626.684 | -0.113  | 12.61   |
| 07/16/96 | 22:53:00 | 579       | 9.974    | 626.686 | -0.111  | 12.61   |
| 07/16/96 | 22:54:00 | 580       | 9.974    | 626.686 | -0.111  | 12.61   |
| 07/16/96 | 22:55:00 | 581       | 9.974    | 626.686 | -0.111  | 12.61   |
| 07/16/96 | 22:56:00 | 582       | 9.974    | 626.686 | -0.111  | 12.61   |
| 07/16/96 | 22:57:00 | 583       | 9.972    | 626.688 | -0.109  | 12.61   |
| 07/16/96 | 22:58:00 | 584       | 9.974    | 626.686 | -0.111  | 12.62   |
| 07/16/96 | 22:59:00 | 585       | 9.974    | 626.686 | -0.111  | 12.61   |
| 07/16/96 | 23:00:00 | 586       | 9.974    | 626.686 | -0.111  | 12.61   |
| 07/16/96 | 23:01:00 | 587       | 9.974    | 626.686 | -0.111  | 12.61   |
| 07/16/96 | 23:02:00 | 588       | 9.974    | 626.686 | -0.111  | 12.62   |
| 07/16/96 | 23:03:00 | 589       | 9.974    | 626.686 | -0.111  | 12.62   |
| 07/16/96 | 23:04:00 | 590       | 9.972    | 626.688 | -0.109  | 12.61   |
| 07/16/96 | 23:05:00 | 591       | 9.974    | 626.686 | -0.111  | 12.61   |
| 07/16/96 | 23:06:00 | 592       | 9.974    | 626.686 | -0.111  | 12.61   |
| 07/16/96 | 23:07:00 | 593       | 9.974    | 626.686 | -0.111  | 12.61   |
| 07/16/96 | 23:08:00 | 594       | 9.974    | 626.686 | -0.111  | 12.61   |
| 07/16/96 | 23:09:00 | 595       | 9.979    | 626.681 | -0.116  | 12.61   |
| 07/16/96 | 23:10:00 | 596       | 9.981    | 626.679 | -0.118  | 12.62   |
| 07/16/96 | 23:11:00 | 597       | 9.983    | 626.677 | -0.12   | 12.62   |
| 07/16/96 | 23:12:00 | 598       | 9.983    | 626.677 | -0.12   | 12.61   |
| 07/16/96 | 23:13:00 | 599       | 9.983    | 626.677 | -0.12   | 12.61   |

| Date     | Time     | Elapsed T | Feet H2O |         | Delta H | Celsius |
|----------|----------|-----------|----------|---------|---------|---------|
| 07/16/96 | 23:14:00 | 600       | 9.981    | 626.679 | -0.118  | 12.62   |
| 07/16/96 | 23:15:00 | 601       | 9.981    | 626.679 | -0.118  | 12.62   |
| 07/16/96 | 23:16:00 | 602       | 9.976    | 626.684 | -0.113  | 12.62   |
| 07/16/96 | 23:17:00 | 603       | 9.976    | 626.684 | -0.113  | 12.62   |
| 07/16/96 | 23:18:00 | 604       | 9.974    | 626.686 | -0.111  | 12.62   |
| 07/16/96 | 23:19:00 | 605       | 9.974    | 626.686 | -0.111  | 12.62   |
| 07/16/96 | 23:20:00 | 606       | 9.974    | 626.686 | -0.111  | 12.61   |
| 07/16/96 | 23:21:00 | 607       | 9.972    | 626.688 | -0.109  | 12.61   |
| 07/16/96 | 23:22:00 | 608       | 9.974    | 626.686 | -0.111  | 12.61   |
| 07/16/96 | 23:23:00 | 609       | 9.974    | 626.686 | -0.111  | 12.62   |
| 07/16/96 | 23:24:00 | 610       | 9.974    | 626.686 | -0.111  | 12.62   |
| 07/16/96 | 23:25:00 | 611       | 9.972    | 626.688 | -0.109  | 12.61   |
| 07/16/96 | 23:26:00 | 612       | 9.974    | 626.686 | -0.111  | 12.62   |
| 07/16/96 | 23:27:00 | 613       | 9.972    | 626.688 | -0.109  | 12.61   |
| 07/16/96 | 23:28:00 | 614       | 9.972    | 626.688 | -0.109  | 12.62   |
| 07/16/96 | 23:29:00 | 615       | 9.967    | 626.693 | -0.104  | 12.61   |
| 07/16/96 | 23:30:00 | 616       | 9.967    | 626.693 | -0.104  | 12.61   |
| 07/16/96 | 23:31:00 | 617       | 9.969    | 626.691 | -0.106  | 12.62   |
| 07/16/96 | 23:32:00 | 618       | 9.969    | 626.691 | -0.106  | 12.62   |
| 07/16/96 | 23:33:00 | 619       | 9.967    | 626.693 | -0.104  | 12.62   |
| 07/16/96 | 23:34:00 | 620       | 9.969    | 626.691 | -0.106  | 12.62   |
| 07/16/96 | 23:35:00 | 621       | 9.969    | 626.691 | -0.106  | 12.62   |
| 07/16/96 | 23:36:00 | 622       | 9.969    | 626.691 | -0.106  | 12.61   |
| 07/16/96 | 23:37:00 | 623       | 9.969    | 626.691 | -0.106  | 12.62   |
| 07/16/96 | 23:38:00 | 624       | 9.969    | 626.691 | -0.106  | 12.61   |
| 07/16/96 | 23:39:00 | 625       | 9.972    | 626.688 | -0.109  | 12.62   |
| 07/16/96 | 23:40:00 | 626       | 9.972    | 626.688 | -0.109  | 12.61   |
| 07/16/96 | 23:41:00 | 627       | 9.972    | 626.688 | -0.109  | 12.62   |
| 07/16/96 | 23:42:00 | 628       | 9.969    | 626.691 | -0.106  | 12.62   |
| 07/16/96 | 23:43:00 | 629       | 9.972    | 626.688 | -0.109  | 12.62   |
| 07/16/96 | 23:44:00 | 630       | 9.967    | 626.693 | -0.104  | 12.62   |
| 07/16/96 | 23:45:00 | 631       | 9.967    | 626.693 | -0.104  | 12.62   |
| 07/16/96 | 23:46:00 | 632       | 9.969    | 626.691 | -0.106  | 12.62   |
| 07/16/96 | 23:47:00 | 633       | 9.967    | 626.693 | -0.104  | 12.62   |
| 07/16/96 | 23:48:00 | 634       | 9.967    | 626.693 | -0.104  | 12.62   |
| 07/16/96 | 23:49:00 | 635       | 9.969    | 626.691 | -0.106  | 12.62   |
| 07/16/96 | 23:50:00 | 636       | 9.967    | 626.693 | -0.104  | 12.62   |
| 07/16/96 | 23:51:00 | 637       | 9.967    | 626.693 | -0.104  | 12.62   |
| 07/16/96 | 23:52:00 | 638       | 9.969    | 626.691 | -0.106  | 12.62   |
| 07/16/96 | 23:53:00 | 639       | 9.967    | 626.693 | -0.104  | 12.62   |
| 07/16/96 | 23:54:00 | 640       | 9.965    | 626.695 | -0.102  | 12.62   |
| 07/16/96 | 23:55:00 | 641       | 9.967    | 626.693 | -0.104  | 12.61   |
| 07/16/96 | 23:56:00 | 642       | 9.965    | 626.695 | -0.102  | 12.62   |
| 07/16/96 | 23:57:00 | 643       | 9.965    | 626.695 | -0.102  | 12.62   |
| 07/16/96 | 23:58:00 | 644       | 9.965    | 626.695 | -0.102  | 12.62   |
| 07/16/96 | 23:59:00 | 645       | 9.965    | 626.695 | -0.102  | 12.62   |
| 07/17/96 | 0:00:00  | 646       | 9.965    | 626.695 | -0.102  | 12.62   |
| 07/17/96 | 0:01:00  | 647       | 9.965    | 626.695 | -0.102  | 12.62   |
| 07/17/96 | 0:02:00  | 648       | 9.967    | 626.693 | -0.104  | 12.62   |
| 07/17/96 | 0:03:00  | 649       | 9.967    | 626.693 | -0.104  | 12.62   |

| Date     | Time    | Elapsed T | Feet H2O |         | Delta H | Celsius |
|----------|---------|-----------|----------|---------|---------|---------|
| 07/17/96 | 0:04:00 | 650       | 9.967    | 626.693 | -0.104  | 12.62   |
| 07/17/96 | 0:05:00 | 651       | 9.967    | 626.693 | -0.104  | 12.62   |
| 07/17/96 | 0:06:00 | 652       | 9.967    | 626.693 | -0.104  | 12.62   |
| 07/17/96 | 0:07:00 | 653       | 9.967    | 626.693 | -0.104  | 12.62   |
| 07/17/96 | 0:08:00 | 654       | 9.967    | 626.693 | -0.104  | 12.62   |
| 07/17/96 | 0:09:00 | 655       | 9.967    | 626.693 | -0.104  | 12.62   |
| 07/17/96 | 0:10:00 | 656       | 9.967    | 626.693 | -0.104  | 12.62   |
| 07/17/96 | 0:11:00 | 657       | 9.967    | 626.693 | -0.104  | 12.62   |
| 07/17/96 | 0:12:00 | 658       | 9.967    | 626.693 | -0.104  | 12.62   |
| 07/17/96 | 0:13:00 | 659       | 9.969    | 626.691 | -0.106  | 12.62   |
| 07/17/96 | 0:14:00 | 660       | 9.972    | 626.688 | -0.109  | 12.62   |
| 07/17/96 | 0:15:00 | 661       | 9.972    | 626.688 | -0.109  | 12.62   |
| 07/17/96 | 0:16:00 | 662       | 9.969    | 626.691 | -0.106  | 12.62   |
| 07/17/96 | 0:17:00 | 663       | 9.972    | 626.688 | -0.109  | 12.62   |
| 07/17/96 | 0:18:00 | 664       | 9.972    | 626.688 | -0.109  | 12.62   |
| 07/17/96 | 0:19:00 | 665       | 9.969    | 626.691 | -0.106  | 12.62   |
| 07/17/96 | 0:20:00 | 666       | 9.969    | 626.691 | -0.106  | 12.62   |
| 07/17/96 | 0:21:00 | 667       | 9.969    | 626.691 | -0.106  | 12.62   |
| 07/17/96 | 0:22:00 | 668       | 9.969    | 626.691 | -0.106  | 12.62   |
| 07/17/96 | 0:23:00 | 669       | 9.967    | 626.693 | -0.104  | 12.62   |
| 07/17/96 | 0:24:00 | 670       | 9.967    | 626.693 | -0.104  | 12.62   |
| 07/17/96 | 0:25:00 | 671       | 9.967    | 626.693 | -0.104  | 12.62   |
| 07/17/96 | 0:26:00 | 672       | 9.969    | 626.691 | -0.106  | 12.62   |
| 07/17/96 | 0:27:00 | 673       | 9.967    | 626.693 | -0.104  | 12.62   |
| 07/17/96 | 0:28:00 | 674       | 9.967    | 626.693 | -0.104  | 12.62   |
| 07/17/96 | 0:29:00 | 675       | 9.965    | 626.695 | -0.102  | 12.62   |
| 07/17/96 | 0:30:00 | 676       | 9.965    | 626.695 | -0.102  | 12.62   |
| 07/17/96 | 0:31:00 | 677       | 9.965    | 626.695 | -0.102  | 12.62   |
| 07/17/96 | 0:32:00 | 678       | 9.965    | 626.695 | -0.102  | 12.62   |
| 07/17/96 | 0:33:00 | 679       | 9.965    | 626.695 | -0.102  | 12.62   |
| 07/17/96 | 0:34:00 | 680       | 9.965    | 626.695 | -0.102  | 12.62   |
| 07/17/96 | 0:35:00 | 681       | 9.965    | 626.695 | -0.102  | 12.62   |
| 07/17/96 | 0:36:00 | 682       | 9.965    | 626.695 | -0.102  | 12.62   |
| 07/17/96 | 0:37:00 | 683       | 9.965    | 626.695 | -0.102  | 12.62   |
| 07/17/96 | 0:38:00 | 684       | 9.965    | 626.695 | -0.102  | 12.62   |
| 07/17/96 | 0:39:00 | 685       | 9.965    | 626.695 | -0.102  | 12.62   |
| 07/17/96 | 0:40:00 | 686       | 9.965    | 626.695 | -0.102  | 12.62   |
| 07/17/96 | 0:41:00 | 687       | 9.965    | 626.695 | -0.102  | 12.62   |
| 07/17/96 | 0:42:00 | 688       | 9.962    | 626.698 | -0.099  | 12.62   |
| 07/17/96 | 0:43:00 | 689       | 9.962    | 626.698 | -0.099  | 12.62   |
| 07/17/96 | 0:44:00 | 690       | 9.962    | 626.698 | -0.099  | 12.62   |
| 07/17/96 | 0:45:00 | 691       | 9.965    | 626.695 | -0.102  | 12.62   |
| 07/17/96 | 0:46:00 | 692       | 9.965    | 626.695 | -0.102  | 12.62   |
| 07/17/96 | 0:47:00 | 693       | 9.965    | 626.695 | -0.102  | 12.62   |
| 07/17/96 | 0:48:00 | 694       | 9.965    | 626.695 | -0.102  | 12.62   |
| 07/17/96 | 0:49:00 | 695       | 9.965    | 626.695 | -0.102  | 12.62   |
| 07/17/96 | 0:50:00 | 696       | 9.967    | 626.693 | -0.104  | 12.62   |
| 07/17/96 | 0:51:00 | 697       | 9.967    | 626.693 | -0.104  | 12.62   |
| 07/17/96 | 0:52:00 | 698       | 9.967    | 626.693 | -0.104  | 12.62   |
| 07/17/96 | 0:53:00 | 699       | 9.967    | 626.693 | -0.104  | 12.62   |

| Date     | Time    | Elapsed T | Feet H2O |         | Delta H | Celsius |
|----------|---------|-----------|----------|---------|---------|---------|
| 07/17/96 | 0:54:00 | 700       | 9.967    | 626.693 | -0.104  | 12.62   |
| 07/17/96 | 0:55:00 | 701       | 9.969    | 626.691 | -0.106  | 12.62   |
| 07/17/96 | 0:56:00 | 702       | 9.967    | 626.693 | -0.104  | 12.62   |
| 07/17/96 | 0:57:00 | 703       | 9.967    | 626.693 | -0.104  | 12.62   |
| 07/17/96 | 0:58:00 | 704       | 9.965    | 626.695 | -0.102  | 12.62   |
| 07/17/96 | 0:59:00 | 705       | 9.965    | 626.695 | -0.102  | 12.62   |
| 07/17/96 | 1:00:00 | 706       | 9.965    | 626.695 | -0.102  | 12.62   |
| 07/17/96 | 1:01:00 | 707       | 9.965    | 626.695 | -0.102  | 12.62   |
| 07/17/96 | 1:02:00 | 708       | 9.965    | 626.695 | -0.102  | 12.62   |
| 07/17/96 | 1:03:00 | 709       | 9.965    | 626.695 | -0.102  | 12.62   |
| 07/17/96 | 1:04:00 | 710       | 9.965    | 626.695 | -0.102  | 12.62   |
| 07/17/96 | 1:05:00 | 711       | 9.962    | 626.698 | -0.099  | 12.62   |
| 07/17/96 | 1:06:00 | 712       | 9.965    | 626.695 | -0.102  | 12.62   |
| 07/17/96 | 1:07:00 | 713       | 9.965    | 626.695 | -0.102  | 12.62   |
| 07/17/96 | 1:08:00 | 714       | 9.965    | 626.695 | -0.102  | 12.62   |
| 07/17/96 | 1:09:00 | 715       | 9.965    | 626.695 | -0.102  | 12.62   |
| 07/17/96 | 1:10:00 | 716       | 9.965    | 626.695 | -0.102  | 12.62   |
| 07/17/96 | 1:11:00 | 717       | 9.967    | 626.693 | -0.104  | 12.62   |
| 07/17/96 | 1:12:00 | 718       | 9.965    | 626.695 | -0.102  | 12.62   |
| 07/17/96 | 1:13:00 | 719       | 9.965    | 626.695 | -0.102  | 12.62   |
| 07/17/96 | 1:14:00 | 720       | 9.967    | 626.693 | -0.104  | 12.62   |
| 07/17/96 | 1:15:00 | 721       | 9.967    | 626.693 | -0.104  | 12.62   |
| 07/17/96 | 1:16:00 | 722       | 9.965    | 626.695 | -0.102  | 12.62   |
| 07/17/96 | 1:17:00 | 723       | 9.965    | 626.695 | -0.102  | 12.62   |
| 07/17/96 | 1:18:00 | 724       | 9.967    | 626.693 | -0.104  | 12.62   |
| 07/17/96 | 1:19:00 | 725       | 9.965    | 626.695 | -0.102  | 12.62   |
| 07/17/96 | 1:20:00 | 726       | 9.967    | 626.693 | -0.104  | 12.62   |
| 07/17/96 | 1:21:00 | 727       | 9.967    | 626.693 | -0.104  | 12.62   |
| 07/17/96 | 1:22:00 | 728       | 9.969    | 626.691 | -0.106  | 12.62   |
| 07/17/96 | 1:23:00 | 729       | 9.965    | 626.695 | -0.102  | 12.62   |
| 07/17/96 | 1:24:00 | 730       | 9.967    | 626.693 | -0.104  | 12.62   |
| 07/17/96 | 1:25:00 | 731       | 9.965    | 626.695 | -0.102  | 12.62   |
| 07/17/96 | 1:26:00 | 732       | 9.965    | 626.695 | -0.102  | 12.62   |
| 07/17/96 | 1:27:00 | 733       | 9.965    | 626.695 | -0.102  | 12.62   |
| 07/17/96 | 1:28:00 | 734       | 9.965    | 626.695 | -0.102  | 12.62   |
| 07/17/96 | 1:29:00 | 735       | 9.967    | 626.693 | -0.104  | 12.62   |
| 07/17/96 | 1:30:00 | 736       | 9.965    | 626.695 | -0.102  | 12.62   |
| 07/17/96 | 1:31:00 | 737       | 9.967    | 626.693 | -0.104  | 12.62   |
| 07/17/96 | 1:32:00 | 738       | 9.967    | 626.693 | -0.104  | 12.62   |
| 07/17/96 | 1:33:00 | 739       | 9.967    | 626.693 | -0.104  | 12.62   |
| 07/17/96 | 1:34:00 | 740       | 9.967    | 626.693 | -0.104  | 12.62   |
| 07/17/96 | 1:35:00 | 741       | 9.967    | 626.693 | -0.104  | 12.62   |
| 07/17/96 | 1:36:00 | 742       | 9.967    | 626.693 | -0.104  | 12.62   |
| 07/17/96 | 1:37:00 | 743       | 9.967    | 626.693 | -0.104  | 12.62   |
| 07/17/96 | 1:38:00 | 744       | 9.967    | 626.693 | -0.104  | 12.62   |
| 07/17/96 | 1:39:00 | 745       | 9.967    | 626.693 | -0.104  | 12.62   |
| 07/17/96 | 1:40:00 | 746       | 9.967    | 626.693 | -0.104  | 12.62   |
| 07/17/96 | 1:41:00 | 747       | 9.967    | 626.693 | -0.104  | 12.62   |
| 07/17/96 | 1:42:00 | 748       | 9.967    | 626.693 | -0.104  | 12.62   |
| 07/17/96 | 1:43:00 | 749       | 9.965    | 626.695 | -0.102  | 12.62   |

| Date     | Time    | Elapsed T | Feet H2O |         | Delta H | Celsius |
|----------|---------|-----------|----------|---------|---------|---------|
| 07/17/96 | 1:44:00 | 750       | 9.965    | 626.695 | -0.102  | 12.62   |
| 07/17/96 | 1:45:00 | 751       | 9.965    | 626.695 | -0.102  | 12.62   |
| 07/17/96 | 1:46:00 | 752       | 9.965    | 626.695 | -0.102  | 12.62   |
| 07/17/96 | 1:47:00 | 753       | 9.965    | 626.695 | -0.102  | 12.62   |
| 07/17/96 | 1:48:00 | 754       | 9.967    | 626.693 | -0.104  | 12.62   |
| 07/17/96 | 1:49:00 | 755       | 9.965    | 626.695 | -0.102  | 12.62   |
| 07/17/96 | 1:50:00 | 756       | 9.965    | 626.695 | -0.102  | 12.62   |
| 07/17/96 | 1:51:00 | 757       | 9.967    | 626.693 | -0.104  | 12.62   |
| 07/17/96 | 1:52:00 | 758       | 9.967    | 626.693 | -0.104  | 12.62   |
| 07/17/96 | 1:53:00 | 759       | 9.967    | 626.693 | -0.104  | 12.62   |
| 07/17/96 | 1:54:00 | 760       | 9.967    | 626.693 | -0.104  | 12.63   |
| 07/17/96 | 1:55:00 | 761       | 9.967    | 626.693 | -0.104  | 12.62   |
| 07/17/96 | 1:56:00 | 762       | 9.967    | 626.693 | -0.104  | 12.62   |
| 07/17/96 | 1:57:00 | 763       | 9.967    | 626.693 | -0.104  | 12.62   |
| 07/17/96 | 1:58:00 | 764       | 9.965    | 626.695 | -0.102  | 12.62   |
| 07/17/96 | 1:59:00 | 765       | 9.967    | 626.693 | -0.104  | 12.62   |
| 07/17/96 | 2:00:00 | 766       | 9.965    | 626.695 | -0.102  | 12.62   |
| 07/17/96 | 2:01:00 | 767       | 9.965    | 626.695 | -0.102  | 12.62   |
| 07/17/96 | 2:02:00 | 768       | 9.967    | 626.693 | -0.104  | 12.62   |
| 07/17/96 | 2:03:00 | 769       | 9.967    | 626.693 | -0.104  | 12.63   |
| 07/17/96 | 2:04:00 | 770       | 9.965    | 626.695 | -0.102  | 12.62   |
| 07/17/96 | 2:05:00 | 771       | 9.967    | 626.693 | -0.104  | 12.62   |
| 07/17/96 | 2:06:00 | 772       | 9.969    | 626.691 | -0.106  | 12.62   |
| 07/17/96 | 2:07:00 | 773       | 9.969    | 626.691 | -0.106  | 12.63   |
| 07/17/96 | 2:08:00 | 774       | 9.969    | 626.691 | -0.106  | 12.62   |
| 07/17/96 | 2:09:00 | 775       | 9.972    | 626.688 | -0.109  | 12.62   |
| 07/17/96 | 2:10:00 | 776       | 9.969    | 626.691 | -0.106  | 12.63   |
| 07/17/96 | 2:11:00 | 777       | 9.969    | 626.691 | -0.106  | 12.62   |
| 07/17/96 | 2:12:00 | 778       | 9.969    | 626.691 | -0.106  | 12.63   |
| 07/17/96 | 2:13:00 | 779       | 9.969    | 626.691 | -0.106  | 12.63   |
| 07/17/96 | 2:14:00 | 780       | 9.969    | 626.691 | -0.106  | 12.62   |
| 07/17/96 | 2:15:00 | 781       | 9.967    | 626.693 | -0.104  | 12.62   |
| 07/17/96 | 2:16:00 | 782       | 9.967    | 626.693 | -0.104  | 12.62   |
| 07/17/96 | 2:17:00 | 783       | 9.967    | 626.693 | -0.104  | 12.63   |
| 07/17/96 | 2:18:00 | 784       | 9.965    | 626.695 | -0.102  | 12.63   |
| 07/17/96 | 2:19:00 | 785       | 9.965    | 626.695 | -0.102  | 12.62   |
| 07/17/96 | 2:20:00 | 786       | 9.965    | 626.695 | -0.102  | 12.63   |
| 07/17/96 | 2:21:00 | 787       | 9.965    | 626.695 | -0.102  | 12.63   |
| 07/17/96 | 2:22:00 | 788       | 9.965    | 626.695 | -0.102  | 12.63   |
| 07/17/96 | 2:23:00 | 789       | 9.965    | 626.695 | -0.102  | 12.63   |
| 07/17/96 | 2:24:00 | 790       | 9.965    | 626.695 | -0.102  | 12.63   |
| 07/17/96 | 2:25:00 | 791       | 9.965    | 626.695 | -0.102  | 12.63   |
| 07/17/96 | 2:26:00 | 792       | 9.965    | 626.695 | -0.102  | 12.63   |
| 07/17/96 | 2:27:00 | 793       | 9.965    | 626.695 | -0.102  | 12.62   |
| 07/17/96 | 2:28:00 | 794       | 9.965    | 626.695 | -0.102  | 12.63   |
| 07/17/96 | 2:29:00 | 795       | 9.967    | 626.693 | -0.104  | 12.63   |
| 07/17/96 | 2:30:00 | 796       | 9.967    | 626.693 | -0.104  | 12.63   |
| 07/17/96 | 2:31:00 | 797       | 9.967    | 626.693 | -0.104  | 12.63   |
| 07/17/96 | 2:32:00 | 798       | 9.969    | 626.691 | -0.106  | 12.62   |
| 07/17/96 | 2:33:00 | 799       | 9.972    | 626.688 | -0.109  | 12.63   |

| Date     | Time    | Elapsed T | Feet H2O |         | Delta H | Celsius |
|----------|---------|-----------|----------|---------|---------|---------|
| 07/17/96 | 2:34:00 | 800       | 9.969    | 626.691 | -0.106  | 12.63   |
| 07/17/96 | 2:35:00 | 801       | 9.969    | 626.691 | -0.106  | 12.63   |
| 07/17/96 | 2:36:00 | 802       | 9.969    | 626.691 | -0.106  | 12.63   |
| 07/17/96 | 2:37:00 | 803       | 9.967    | 626.693 | -0.104  | 12.63   |
| 07/17/96 | 2:38:00 | 804       | 9.967    | 626.693 | -0.104  | 12.63   |
| 07/17/96 | 2:39:00 | 805       | 9.967    | 626.693 | -0.104  | 12.63   |
| 07/17/96 | 2:40:00 | 806       | 9.969    | 626.691 | -0.106  | 12.63   |
| 07/17/96 | 2:41:00 | 807       | 9.969    | 626.691 | -0.106  | 12.63   |
| 07/17/96 | 2:42:00 | 808       | 9.967    | 626.693 | -0.104  | 12.62   |
| 07/17/96 | 2:43:00 | 809       | 9.967    | 626.693 | -0.104  | 12.63   |
| 07/17/96 | 2:44:00 | 810       | 9.967    | 626.693 | -0.104  | 12.63   |
| 07/17/96 | 2:45:00 | 811       | 9.967    | 626.693 | -0.104  | 12.63   |
| 07/17/96 | 2:46:00 | 812       | 9.965    | 626.695 | -0.102  | 12.63   |
| 07/17/96 | 2:47:00 | 813       | 9.965    | 626.695 | -0.102  | 12.63   |
| 07/17/96 | 2:48:00 | 814       | 9.965    | 626.695 | -0.102  | 12.63   |
| 07/17/96 | 2:49:00 | 815       | 9.965    | 626.695 | -0.102  | 12.63   |
| 07/17/96 | 2:50:00 | 816       | 9.965    | 626.695 | -0.102  | 12.63   |
| 07/17/96 | 2:51:00 | 817       | 9.967    | 626.693 | -0.104  | 12.63   |
| 07/17/96 | 2:52:00 | 818       | 9.967    | 626.693 | -0.104  | 12.62   |
| 07/17/96 | 2:53:00 | 819       | 9.969    | 626.691 | -0.106  | 12.63   |
| 07/17/96 | 2:54:00 | 820       | 9.969    | 626.691 | -0.106  | 12.63   |
| 07/17/96 | 2:55:00 | 821       | 9.969    | 626.691 | -0.106  | 12.63   |
| 07/17/96 | 2:56:00 | 822       | 9.972    | 626.688 | -0.109  | 12.63   |
| 07/17/96 | 2:57:00 | 823       | 9.972    | 626.688 | -0.109  | 12.63   |
| 07/17/96 | 2:58:00 | 824       | 9.969    | 626.691 | -0.106  | 12.63   |
| 07/17/96 | 2:59:00 | 825       | 9.972    | 626.688 | -0.109  | 12.63   |
| 07/17/96 | 3:00:00 | 826       | 9.969    | 626.691 | -0.106  | 12.63   |
| 07/17/96 | 3:01:00 | 827       | 9.972    | 626.688 | -0.109  | 12.63   |
| 07/17/96 | 3:02:00 | 828       | 9.969    | 626.691 | -0.106  | 12.63   |
| 07/17/96 | 3:03:00 | 829       | 9.972    | 626.688 | -0.109  | 12.63   |
| 07/17/96 | 3:04:00 | 830       | 9.969    | 626.691 | -0.106  | 12.63   |
| 07/17/96 | 3:05:00 | 831       | 9.969    | 626.691 | -0.106  | 12.63   |
| 07/17/96 | 3:06:00 | 832       | 9.972    | 626.688 | -0.109  | 12.63   |
| 07/17/96 | 3:07:00 | 833       | 9.969    | 626.691 | -0.106  | 12.63   |
| 07/17/96 | 3:08:00 | 834       | 9.969    | 626.691 | -0.106  | 12.63   |
| 07/17/96 | 3:09:00 | 835       | 9.972    | 626.688 | -0.109  | 12.63   |
| 07/17/96 | 3:10:00 | 836       | 9.972    | 626.688 | -0.109  | 12.63   |
| 07/17/96 | 3:11:00 | 837       | 9.972    | 626.688 | -0.109  | 12.63   |
| 07/17/96 | 3:12:00 | 838       | 9.972    | 626.688 | -0.109  | 12.63   |
| 07/17/96 | 3:13:00 | 839       | 9.972    | 626.688 | -0.109  | 12.63   |
| 07/17/96 | 3:14:00 | 840       | 9.972    | 626.688 | -0.109  | 12.63   |
| 07/17/96 | 3:15:00 | 841       | 9.972    | 626.688 | -0.109  | 12.63   |
| 07/17/96 | 3:16:00 | 842       | 9.972    | 626.688 | -0.109  | 12.63   |
| 07/17/96 | 3:17:00 | 843       | 9.969    | 626.691 | -0.106  | 12.63   |
| 07/17/96 | 3:18:00 | 844       | 9.969    | 626.691 | -0.106  | 12.63   |
| 07/17/96 | 3:19:00 | 845       | 9.969    | 626.691 | -0.106  | 12.63   |
| 07/17/96 | 3:20:00 | 846       | 9.972    | 626.688 | -0.109  | 12.63   |
| 07/17/96 | 3:21:00 | 847       | 9.972    | 626.688 | -0.109  | 12.63   |
| 07/17/96 | 3:22:00 | 848       | 9.972    | 626.688 | -0.109  | 12.63   |
| 07/17/96 | 3:23:00 | 849       | 9.972    | 626.688 | -0.109  | 12.63   |

| Date     | Time    | Elapsed T | Feet H2O |         | Delta H | Celsius |
|----------|---------|-----------|----------|---------|---------|---------|
| 07/17/96 | 3:24:00 | 850       | 9.972    | 626.688 | -0.109  | 12.63   |
| 07/17/96 | 3:25:00 | 851       | 9.972    | 626.688 | -0.109  | 12.63   |
| 07/17/96 | 3:26:00 | 852       | 9.972    | 626.688 | -0.109  | 12.63   |
| 07/17/96 | 3:27:00 | 853       | 9.974    | 626.686 | -0.111  | 12.63   |
| 07/17/96 | 3:28:00 | 854       | 9.974    | 626.686 | -0.111  | 12.63   |
| 07/17/96 | 3:29:00 | 855       | 9.972    | 626.688 | -0.109  | 12.63   |
| 07/17/96 | 3:30:00 | 856       | 9.974    | 626.686 | -0.111  | 12.63   |
| 07/17/96 | 3:31:00 | 857       | 9.974    | 626.686 | -0.111  | 12.63   |
| 07/17/96 | 3:32:00 | 858       | 9.974    | 626.686 | -0.111  | 12.63   |
| 07/17/96 | 3:33:00 | 859       | 9.974    | 626.686 | -0.111  | 12.63   |
| 07/17/96 | 3:34:00 | 860       | 9.974    | 626.686 | -0.111  | 12.63   |
| 07/17/96 | 3:35:00 | 861       | 9.974    | 626.686 | -0.111  | 12.63   |
| 07/17/96 | 3:36:00 | 862       | 9.974    | 626.686 | -0.111  | 12.63   |
| 07/17/96 | 3:37:00 | 863       | 9.974    | 626.686 | -0.111  | 12.63   |
| 07/17/96 | 3:38:00 | 864       | 9.974    | 626.686 | -0.111  | 12.63   |
| 07/17/96 | 3:39:00 | 865       | 9.974    | 626.686 | -0.111  | 12.63   |
| 07/17/96 | 3:40:00 | 866       | 9.974    | 626.686 | -0.111  | 12.63   |
| 07/17/96 | 3:41:00 | 867       | 9.974    | 626.686 | -0.111  | 12.63   |
| 07/17/96 | 3:42:00 | 868       | 9.974    | 626.686 | -0.111  | 12.63   |
| 07/17/96 | 3:43:00 | 869       | 9.974    | 626.686 | -0.111  | 12.63   |
| 07/17/96 | 3:44:00 | 870       | 9.974    | 626.686 | -0.111  | 12.63   |
| 07/17/96 | 3:45:00 | 871       | 9.972    | 626.688 | -0.109  | 12.63   |
| 07/17/96 | 3:46:00 | 872       | 9.972    | 626.688 | -0.109  | 12.63   |
| 07/17/96 | 3:47:00 | 873       | 9.974    | 626.686 | -0.111  | 12.63   |
| 07/17/96 | 3:48:00 | 874       | 9.979    | 626.681 | -0.118  | 12.63   |
| 07/17/96 | 3:49:00 | 875       | 9.979    | 626.681 | -0.118  | 12.63   |
| 07/17/96 | 3:50:00 | 876       | 9.979    | 626.681 | -0.118  | 12.63   |
| 07/17/96 | 3:51:00 | 877       | 9.981    | 626.679 | -0.118  | 12.63   |
| 07/17/96 | 3:52:00 | 878       | 9.979    | 626.681 | -0.118  | 12.63   |
| 07/17/96 | 3:53:00 | 879       | 9.974    | 626.686 | -0.111  | 12.63   |
| 07/17/96 | 3:54:00 | 880       | 9.974    | 626.686 | -0.111  | 12.63   |
| 07/17/96 | 3:55:00 | 881       | 9.974    | 626.686 | -0.111  | 12.63   |
| 07/17/96 | 3:56:00 | 882       | 9.974    | 626.686 | -0.111  | 12.63   |
| 07/17/96 | 3:57:00 | 883       | 9.974    | 626.686 | -0.111  | 12.63   |
| 07/17/96 | 3:58:00 | 884       | 9.974    | 626.686 | -0.111  | 12.63   |
| 07/17/96 | 3:59:00 | 885       | 9.974    | 626.686 | -0.111  | 12.63   |
| 07/17/96 | 4:00:00 | 886       | 9.974    | 626.686 | -0.111  | 12.63   |
| 07/17/96 | 4:01:00 | 887       | 9.974    | 626.686 | -0.111  | 12.63   |
| 07/17/96 | 4:02:00 | 888       | 9.974    | 626.686 | -0.111  | 12.63   |
| 07/17/96 | 4:03:00 | 889       | 9.974    | 626.686 | -0.111  | 12.63   |
| 07/17/96 | 4:04:00 | 890       | 9.972    | 626.688 | -0.109  | 12.63   |
| 07/17/96 | 4:05:00 | 891       | 9.972    | 626.688 | -0.109  | 12.63   |
| 07/17/96 | 4:06:00 | 892       | 9.974    | 626.686 | -0.111  | 12.63   |
| 07/17/96 | 4:07:00 | 893       | 9.972    | 626.688 | -0.109  | 12.63   |
| 07/17/96 | 4:08:00 | 894       | 9.972    | 626.688 | -0.109  | 12.63   |
| 07/17/96 | 4:09:00 | 895       | 9.972    | 626.688 | -0.109  | 12.63   |
| 07/17/96 | 4:10:00 | 896       | 9.969    | 626.691 | -0.106  | 12.63   |
| 07/17/96 | 4:11:00 | 897       | 9.969    | 626.691 | -0.106  | 12.63   |
| 07/17/96 | 4:12:00 | 898       | 9.967    | 626.693 | -0.104  | 12.63   |
| 07/17/96 | 4:13:00 | 899       | 9.969    | 626.691 | -0.106  | 12.63   |

| Date     | Time    | Elapsed T | Feet H2O |         | Delta H | Celsius |
|----------|---------|-----------|----------|---------|---------|---------|
| 07/17/96 | 4:14:00 | 900       | 9.969    | 626.691 | -0.106  | 12.63   |
| 07/17/96 | 4:15:00 | 901       | 9.967    | 626.693 | -0.104  | 12.63   |
| 07/17/96 | 4:16:00 | 902       | 9.969    | 626.691 | -0.106  | 12.63   |
| 07/17/96 | 4:17:00 | 903       | 9.967    | 626.693 | -0.104  | 12.63   |
| 07/17/96 | 4:18:00 | 904       | 9.967    | 626.693 | -0.104  | 12.63   |
| 07/17/96 | 4:19:00 | 905       | 9.965    | 626.695 | -0.102  | 12.63   |
| 07/17/96 | 4:20:00 | 906       | 9.965    | 626.695 | -0.102  | 12.63   |
| 07/17/96 | 4:21:00 | 907       | 9.965    | 626.695 | -0.102  | 12.63   |
| 07/17/96 | 4:22:00 | 908       | 9.965    | 626.695 | -0.102  | 12.64   |
| 07/17/96 | 4:23:00 | 909       | 9.965    | 626.695 | -0.102  | 12.63   |
| 07/17/96 | 4:24:00 | 910       | 9.965    | 626.695 | -0.102  | 12.63   |
| 07/17/96 | 4:25:00 | 911       | 9.967    | 626.693 | -0.104  | 12.63   |
| 07/17/96 | 4:26:00 | 912       | 9.969    | 626.691 | -0.106  | 12.63   |
| 07/17/96 | 4:27:00 | 913       | 9.969    | 626.691 | -0.106  | 12.63   |
| 07/17/96 | 4:28:00 | 914       | 9.967    | 626.693 | -0.104  | 12.63   |
| 07/17/96 | 4:29:00 | 915       | 9.967    | 626.693 | -0.104  | 12.63   |
| 07/17/96 | 4:30:00 | 916       | 9.965    | 626.695 | -0.102  | 12.63   |
| 07/17/96 | 4:31:00 | 917       | 9.967    | 626.693 | -0.104  | 12.63   |
| 07/17/96 | 4:32:00 | 918       | 9.967    | 626.693 | -0.104  | 12.63   |
| 07/17/96 | 4:33:00 | 919       | 9.967    | 626.693 | -0.104  | 12.63   |
| 07/17/96 | 4:34:00 | 920       | 9.967    | 626.693 | -0.104  | 12.63   |
| 07/17/96 | 4:35:00 | 921       | 9.967    | 626.693 | -0.104  | 12.63   |
| 07/17/96 | 4:36:00 | 922       | 9.967    | 626.693 | -0.104  | 12.63   |
| 07/17/96 | 4:37:00 | 923       | 9.967    | 626.693 | -0.104  | 12.63   |
| 07/17/96 | 4:38:00 | 924       | 9.967    | 626.693 | -0.104  | 12.63   |
| 07/17/96 | 4:39:00 | 925       | 9.972    | 626.688 | -0.109  | 12.63   |
| 07/17/96 | 4:40:00 | 926       | 9.972    | 626.688 | -0.109  | 12.63   |
| 07/17/96 | 4:41:00 | 927       | 9.972    | 626.688 | -0.109  | 12.63   |
| 07/17/96 | 4:42:00 | 928       | 9.972    | 626.688 | -0.109  | 12.63   |
| 07/17/96 | 4:43:00 | 929       | 9.972    | 626.688 | -0.109  | 12.63   |
| 07/17/96 | 4:44:00 | 930       | 9.969    | 626.691 | -0.106  | 12.63   |
| 07/17/96 | 4:45:00 | 931       | 9.974    | 626.686 | -0.111  | 12.63   |
| 07/17/96 | 4:46:00 | 932       | 9.972    | 626.688 | -0.109  | 12.63   |
| 07/17/96 | 4:47:00 | 933       | 9.972    | 626.688 | -0.109  | 12.63   |
| 07/17/96 | 4:48:00 | 934       | 9.969    | 626.691 | -0.106  | 12.63   |
| 07/17/96 | 4:49:00 | 935       | 9.972    | 626.688 | -0.109  | 12.63   |
| 07/17/96 | 4:50:00 | 936       | 9.972    | 626.688 | -0.109  | 12.63   |
| 07/17/96 | 4:51:00 | 937       | 9.974    | 626.686 | -0.111  | 12.63   |
| 07/17/96 | 4:52:00 | 938       | 9.974    | 626.686 | -0.111  | 12.63   |
| 07/17/96 | 4:53:00 | 939       | 9.974    | 626.686 | -0.111  | 12.63   |
| 07/17/96 | 4:54:00 | 940       | 9.974    | 626.686 | -0.111  | 12.63   |
| 07/17/96 | 4:55:00 | 941       | 9.974    | 626.686 | -0.111  | 12.63   |
| 07/17/96 | 4:56:00 | 942       | 9.974    | 626.686 | -0.111  | 12.64   |
| 07/17/96 | 4:57:00 | 943       | 9.976    | 626.684 | -0.113  | 12.63   |
| 07/17/96 | 4:58:00 | 944       | 9.979    | 626.681 | -0.116  | 12.63   |
| 07/17/96 | 4:59:00 | 945       | 9.979    | 626.681 | -0.116  | 12.63   |
| 07/17/96 | 5:00:00 | 946       | 9.979    | 626.681 | -0.116  | 12.64   |
| 07/17/96 | 5:01:00 | 947       | 9.976    | 626.684 | -0.113  | 12.63   |
| 07/17/96 | 5:02:00 | 948       | 9.976    | 626.684 | -0.113  | 12.63   |
| 07/17/96 | 5:03:00 | 949       | 9.974    | 626.686 | -0.111  | 12.64   |

| Date     | Time    | Elapsed T | Feet H2O |         | Delta H | Celsius |
|----------|---------|-----------|----------|---------|---------|---------|
| 07/17/96 | 5:04:00 | 950       | 9.976    | 626.684 | -0.113  | 12.63   |
| 07/17/96 | 5:05:00 | 951       | 9.974    | 626.686 | -0.111  | 12.63   |
| 07/17/96 | 5:06:00 | 952       | 9.974    | 626.686 | -0.111  | 12.64   |
| 07/17/96 | 5:07:00 | 953       | 9.974    | 626.686 | -0.111  | 12.63   |
| 07/17/96 | 5:08:00 | 954       | 9.976    | 626.684 | -0.113  | 12.63   |
| 07/17/96 | 5:09:00 | 955       | 9.979    | 626.681 | -0.116  | 12.64   |
| 07/17/96 | 5:10:00 | 956       | 9.979    | 626.681 | -0.116  | 12.63   |
| 07/17/96 | 5:11:00 | 957       | 9.979    | 626.681 | -0.116  | 12.63   |
| 07/17/96 | 5:12:00 | 958       | 9.979    | 626.681 | -0.116  | 12.63   |
| 07/17/96 | 5:13:00 | 959       | 9.981    | 626.679 | -0.118  | 12.64   |
| 07/17/96 | 5:14:00 | 960       | 9.981    | 626.679 | -0.118  | 12.63   |
| 07/17/96 | 5:15:00 | 961       | 9.981    | 626.679 | -0.118  | 12.64   |
| 07/17/96 | 5:16:00 | 962       | 9.979    | 626.681 | -0.116  | 12.64   |
| 07/17/96 | 5:17:00 | 963       | 9.979    | 626.681 | -0.116  | 12.63   |
| 07/17/96 | 5:18:00 | 964       | 9.981    | 626.679 | -0.118  | 12.63   |
| 07/17/96 | 5:19:00 | 965       | 9.981    | 626.679 | -0.118  | 12.63   |
| 07/17/96 | 5:20:00 | 966       | 9.979    | 626.681 | -0.116  | 12.64   |
| 07/17/96 | 5:21:00 | 967       | 9.976    | 626.684 | -0.113  | 12.64   |
| 07/17/96 | 5:22:00 | 968       | 9.976    | 626.684 | -0.113  | 12.64   |
| 07/17/96 | 5:23:00 | 969       | 9.976    | 626.684 | -0.113  | 12.64   |
| 07/17/96 | 5:24:00 | 970       | 9.976    | 626.684 | -0.113  | 12.64   |
| 07/17/96 | 5:25:00 | 971       | 9.976    | 626.684 | -0.113  | 12.63   |
| 07/17/96 | 5:26:00 | 972       | 9.979    | 626.681 | -0.116  | 12.63   |
| 07/17/96 | 5:27:00 | 973       | 9.981    | 626.679 | -0.118  | 12.64   |
| 07/17/96 | 5:28:00 | 974       | 9.981    | 626.679 | -0.118  | 12.64   |
| 07/17/96 | 5:29:00 | 975       | 9.981    | 626.679 | -0.118  | 12.64   |
| 07/17/96 | 5:30:00 | 976       | 9.981    | 626.679 | -0.118  | 12.64   |
| 07/17/96 | 5:31:00 | 977       | 9.981    | 626.679 | -0.118  | 12.64   |
| 07/17/96 | 5:32:00 | 978       | 9.981    | 626.679 | -0.118  | 12.64   |
| 07/17/96 | 5:33:00 | 979       | 9.981    | 626.679 | -0.118  | 12.64   |
| 07/17/96 | 5:34:00 | 980       | 9.983    | 626.677 | -0.12   | 12.64   |
| 07/17/96 | 5:35:00 | 981       | 9.981    | 626.679 | -0.118  | 12.63   |
| 07/17/96 | 5:36:00 | 982       | 9.981    | 626.679 | -0.118  | 12.63   |
| 07/17/96 | 5:37:00 | 983       | 9.983    | 626.677 | -0.12   | 12.64   |
| 07/17/96 | 5:38:00 | 984       | 9.983    | 626.677 | -0.12   | 12.64   |
| 07/17/96 | 5:39:00 | 985       | 9.981    | 626.679 | -0.118  | 12.64   |
| 07/17/96 | 5:40:00 | 986       | 9.983    | 626.677 | -0.12   | 12.64   |
| 07/17/96 | 5:41:00 | 987       | 9.983    | 626.677 | -0.12   | 12.64   |
| 07/17/96 | 5:42:00 | 988       | 9.983    | 626.677 | -0.12   | 12.64   |
| 07/17/96 | 5:43:00 | 989       | 9.983    | 626.677 | -0.12   | 12.64   |
| 07/17/96 | 5:44:00 | 990       | 9.983    | 626.677 | -0.12   | 12.64   |
| 07/17/96 | 5:45:00 | 991       | 9.983    | 626.677 | -0.12   | 12.64   |
| 07/17/96 | 5:46:00 | 992       | 9.985    | 626.675 | -0.122  | 12.64   |
| 07/17/96 | 5:47:00 | 993       | 9.985    | 626.675 | -0.122  | 12.64   |
| 07/17/96 | 5:48:00 | 994       | 9.985    | 626.675 | -0.122  | 12.64   |
| 07/17/96 | 5:49:00 | 995       | 9.988    | 626.672 | -0.125  | 12.63   |
| 07/17/96 | 5:50:00 | 996       | 9.985    | 626.675 | -0.122  | 12.64   |
| 07/17/96 | 5:51:00 | 997       | 9.983    | 626.677 | -0.12   | 12.64   |
| 07/17/96 | 5:52:00 | 998       | 9.983    | 626.677 | -0.12   | 12.64   |
| 07/17/96 | 5:53:00 | 999       | 9.983    | 626.677 | -0.12   | 12.64   |

| Date     | Time    | Elapsed T | Feet H2O |         | Delta H | Celsius |
|----------|---------|-----------|----------|---------|---------|---------|
| 07/17/96 | 5:54:00 | 1000      | 9.981    | 626.679 | -0.118  | 12.64   |
| 07/17/96 | 5:55:00 | 1001      | 9.981    | 626.679 | -0.118  | 12.64   |
| 07/17/96 | 5:56:00 | 1002      | 9.981    | 626.679 | -0.118  | 12.64   |
| 07/17/96 | 5:57:00 | 1003      | 9.981    | 626.679 | -0.118  | 12.64   |
| 07/17/96 | 5:58:00 | 1004      | 9.983    | 626.677 | -0.12   | 12.64   |
| 07/17/96 | 5:59:00 | 1005      | 9.983    | 626.677 | -0.12   | 12.64   |
| 07/17/96 | 6:00:00 | 1006      | 9.983    | 626.677 | -0.12   | 12.64   |
| 07/17/96 | 6:01:00 | 1007      | 9.983    | 626.677 | -0.12   | 12.64   |
| 07/17/96 | 6:02:00 | 1008      | 9.983    | 626.677 | -0.12   | 12.63   |
| 07/17/96 | 6:03:00 | 1009      | 9.983    | 626.677 | -0.12   | 12.64   |
| 07/17/96 | 6:04:00 | 1010      | 9.983    | 626.677 | -0.12   | 12.64   |
| 07/17/96 | 6:05:00 | 1011      | 9.983    | 626.677 | -0.12   | 12.64   |
| 07/17/96 | 6:06:00 | 1012      | 9.983    | 626.677 | -0.12   | 12.64   |
| 07/17/96 | 6:07:00 | 1013      | 9.983    | 626.677 | -0.12   | 12.64   |
| 07/17/96 | 6:08:00 | 1014      | 9.983    | 626.677 | -0.12   | 12.64   |
| 07/17/96 | 6:09:00 | 1015      | 9.981    | 626.679 | -0.118  | 12.64   |
| 07/17/96 | 6:10:00 | 1016      | 9.981    | 626.679 | -0.118  | 12.64   |
| 07/17/96 | 6:11:00 | 1017      | 9.981    | 626.679 | -0.118  | 12.64   |
| 07/17/96 | 6:12:00 | 1018      | 9.981    | 626.679 | -0.118  | 12.64   |
| 07/17/96 | 6:13:00 | 1019      | 9.981    | 626.679 | -0.118  | 12.64   |
| 07/17/96 | 6:14:00 | 1020      | 9.983    | 626.677 | -0.12   | 12.64   |
| 07/17/96 | 6:15:00 | 1021      | 9.981    | 626.679 | -0.118  | 12.64   |
| 07/17/96 | 6:16:00 | 1022      | 9.983    | 626.677 | -0.12   | 12.64   |
| 07/17/96 | 6:17:00 | 1023      | 9.983    | 626.677 | -0.12   | 12.64   |
| 07/17/96 | 6:18:00 | 1024      | 9.983    | 626.677 | -0.12   | 12.64   |
| 07/17/96 | 6:19:00 | 1025      | 9.981    | 626.679 | -0.118  | 12.64   |
| 07/17/96 | 6:20:00 | 1026      | 9.983    | 626.677 | -0.12   | 12.64   |
| 07/17/96 | 6:21:00 | 1027      | 9.983    | 626.677 | -0.12   | 12.64   |
| 07/17/96 | 6:22:00 | 1028      | 9.983    | 626.677 | -0.12   | 12.64   |
| 07/17/96 | 6:23:00 | 1029      | 9.983    | 626.677 | -0.12   | 12.64   |
| 07/17/96 | 6:24:00 | 1030      | 9.981    | 626.679 | -0.118  | 12.64   |
| 07/17/96 | 6:25:00 | 1031      | 9.983    | 626.677 | -0.12   | 12.64   |
| 07/17/96 | 6:26:00 | 1032      | 9.981    | 626.679 | -0.118  | 12.64   |
| 07/17/96 | 6:27:00 | 1033      | 9.981    | 626.679 | -0.118  | 12.64   |
| 07/17/96 | 6:28:00 | 1034      | 9.983    | 626.677 | -0.12   | 12.64   |
| 07/17/96 | 6:29:00 | 1035      | 9.981    | 626.679 | -0.118  | 12.64   |
| 07/17/96 | 6:30:00 | 1036      | 9.981    | 626.679 | -0.118  | 12.64   |
| 07/17/96 | 6:31:00 | 1037      | 9.981    | 626.679 | -0.118  | 12.64   |
| 07/17/96 | 6:32:00 | 1038      | 9.981    | 626.679 | -0.118  | 12.64   |
| 07/17/96 | 6:33:00 | 1039      | 9.983    | 626.677 | -0.12   | 12.64   |
| 07/17/96 | 6:34:00 | 1040      | 9.983    | 626.677 | -0.12   | 12.64   |
| 07/17/96 | 6:35:00 | 1041      | 9.983    | 626.677 | -0.12   | 12.64   |
| 07/17/96 | 6:36:00 | 1042      | 9.983    | 626.677 | -0.12   | 12.64   |
| 07/17/96 | 6:37:00 | 1043      | 9.983    | 626.677 | -0.12   | 12.64   |
| 07/17/96 | 6:38:00 | 1044      | 9.983    | 626.677 | -0.12   | 12.64   |
| 07/17/96 | 6:39:00 | 1045      | 9.983    | 626.677 | -0.12   | 12.64   |
| 07/17/96 | 6:40:00 | 1046      | 9.983    | 626.677 | -0.12   | 12.64   |
| 07/17/96 | 6:41:00 | 1047      | 9.983    | 626.677 | -0.12   | 12.64   |
| 07/17/96 | 6:42:00 | 1048      | 9.983    | 626.677 | -0.12   | 12.64   |
| 07/17/96 | 6:43:00 | 1049      | 9.985    | 626.675 | -0.122  | 12.64   |

| Date     | Time    | Elapsed T | Feet H2O |         | Delta H | Celsius |
|----------|---------|-----------|----------|---------|---------|---------|
| 07/17/96 | 6:44:00 | 1050      | 9.985    | 626.675 | -0.122  | 12.64   |
| 07/17/96 | 6:45:00 | 1051      | 9.983    | 626.677 | -0.12   | 12.64   |
| 07/17/96 | 6:46:00 | 1052      | 9.983    | 626.677 | -0.12   | 12.64   |
| 07/17/96 | 6:47:00 | 1053      | 9.983    | 626.677 | -0.12   | 12.64   |
| 07/17/96 | 6:48:00 | 1054      | 9.983    | 626.677 | -0.12   | 12.64   |
| 07/17/96 | 6:49:00 | 1055      | 9.983    | 626.677 | -0.12   | 12.64   |
| 07/17/96 | 6:50:00 | 1056      | 9.983    | 626.677 | -0.12   | 12.64   |
| 07/17/96 | 6:51:00 | 1057      | 9.983    | 626.677 | -0.12   | 12.64   |
| 07/17/96 | 6:52:00 | 1058      | 9.981    | 626.679 | -0.118  | 12.64   |
| 07/17/96 | 6:53:00 | 1059      | 9.983    | 626.677 | -0.12   | 12.64   |
| 07/17/96 | 6:54:00 | 1060      | 9.981    | 626.679 | -0.118  | 12.64   |
| 07/17/96 | 6:55:00 | 1061      | 9.983    | 626.677 | -0.12   | 12.64   |
| 07/17/96 | 6:56:00 | 1062      | 9.983    | 626.677 | -0.12   | 12.64   |
| 07/17/96 | 6:57:00 | 1063      | 9.983    | 626.677 | -0.12   | 12.64   |
| 07/17/96 | 6:58:00 | 1064      | 9.983    | 626.677 | -0.12   | 12.64   |
| 07/17/96 | 6:59:00 | 1065      | 9.981    | 626.679 | -0.118  | 12.64   |
| 07/17/96 | 7:00:00 | 1066      | 9.981    | 626.679 | -0.118  | 12.64   |
| 07/17/96 | 7:01:00 | 1067      | 9.981    | 626.679 | -0.118  | 12.64   |
| 07/17/96 | 7:02:00 | 1068      | 9.981    | 626.679 | -0.118  | 12.64   |
| 07/17/96 | 7:03:00 | 1069      | 9.981    | 626.679 | -0.118  | 12.64   |
| 07/17/96 | 7:04:00 | 1070      | 9.981    | 626.679 | -0.118  | 12.64   |
| 07/17/96 | 7:05:00 | 1071      | 9.979    | 626.681 | -0.116  | 12.64   |
| 07/17/96 | 7:06:00 | 1072      | 9.979    | 626.681 | -0.116  | 12.64   |
| 07/17/96 | 7:07:00 | 1073      | 9.976    | 626.684 | -0.113  | 12.64   |
| 07/17/96 | 7:08:00 | 1074      | 9.976    | 626.684 | -0.113  | 12.64   |
| 07/17/96 | 7:09:00 | 1075      | 9.976    | 626.684 | -0.113  | 12.64   |
| 07/17/96 | 7:10:00 | 1076      | 9.976    | 626.684 | -0.113  | 12.64   |
| 07/17/96 | 7:11:00 | 1077      | 9.974    | 626.686 | -0.111  | 12.64   |
| 07/17/96 | 7:12:00 | 1078      | 9.974    | 626.686 | -0.111  | 12.64   |
| 07/17/96 | 7:13:00 | 1079      | 9.974    | 626.686 | -0.111  | 12.64   |
| 07/17/96 | 7:14:00 | 1080      | 9.976    | 626.684 | -0.113  | 12.64   |
| 07/17/96 | 7:15:00 | 1081      | 9.976    | 626.684 | -0.113  | 12.64   |
| 07/17/96 | 7:16:00 | 1082      | 9.979    | 626.681 | -0.116  | 12.64   |
| 07/17/96 | 7:17:00 | 1083      | 9.979    | 626.681 | -0.116  | 12.64   |
| 07/17/96 | 7:18:00 | 1084      | 9.981    | 626.679 | -0.118  | 12.64   |
| 07/17/96 | 7:19:00 | 1085      | 9.981    | 626.679 | -0.118  | 12.64   |
| 07/17/96 | 7:20:00 | 1086      | 9.981    | 626.679 | -0.118  | 12.64   |
| 07/17/96 | 7:21:00 | 1087      | 9.981    | 626.679 | -0.118  | 12.64   |
| 07/17/96 | 7:22:00 | 1088      | 9.983    | 626.677 | -0.12   | 12.64   |
| 07/17/96 | 7:23:00 | 1089      | 9.983    | 626.677 | -0.12   | 12.64   |
| 07/17/96 | 7:24:00 | 1090      | 9.983    | 626.677 | -0.12   | 12.64   |
| 07/17/96 | 7:25:00 | 1091      | 9.985    | 626.675 | -0.122  | 12.65   |
| 07/17/96 | 7:26:00 | 1092      | 9.981    | 626.679 | -0.118  | 12.64   |
| 07/17/96 | 7:27:00 | 1093      | 9.985    | 626.675 | -0.122  | 12.65   |
| 07/17/96 | 7:28:00 | 1094      | 9.981    | 626.679 | -0.118  | 12.64   |
| 07/17/96 | 7:29:00 | 1095      | 9.985    | 626.675 | -0.122  | 12.65   |
| 07/17/96 | 7:30:00 | 1096      | 9.983    | 626.677 | -0.12   | 12.64   |
| 07/17/96 | 7:31:00 | 1097      | 9.983    | 626.677 | -0.12   | 12.64   |
| 07/17/96 | 7:32:00 | 1098      | 9.983    | 626.677 | -0.12   | 12.64   |
| 07/17/96 | 7:33:00 | 1099      | 9.988    | 626.672 | -0.125  | 12.65   |

| Date     | Time    | Elapsed T | Feet H <sub>2</sub> O |         | Delta H | Celsius |
|----------|---------|-----------|-----------------------|---------|---------|---------|
| 07/17/96 | 7:34:00 | 1100      | 9.983                 | 626.677 | -0.12   | 12.64   |
| 07/17/96 | 7:35:00 | 1101      | 9.985                 | 626.675 | -0.122  | 12.65   |
| 07/17/96 | 7:36:00 | 1102      | 9.983                 | 626.677 | -0.12   | 12.64   |
| 07/17/96 | 7:37:00 | 1103      | 9.983                 | 626.677 | -0.12   | 12.65   |
| 07/17/96 | 7:38:00 | 1104      | 9.983                 | 626.677 | -0.12   | 12.65   |
| 07/17/96 | 7:39:00 | 1105      | 9.981                 | 626.679 | -0.118  | 12.64   |
| 07/17/96 | 7:40:00 | 1106      | 9.981                 | 626.679 | -0.118  | 12.64   |
| 07/17/96 | 7:41:00 | 1107      | 9.985                 | 626.675 | -0.122  | 12.65   |
| 07/17/96 | 7:42:00 | 1108      | 9.981                 | 626.679 | -0.118  | 12.64   |
| 07/17/96 | 7:43:00 | 1109      | 9.981                 | 626.679 | -0.118  | 12.64   |
| 07/17/96 | 7:44:00 | 1110      | 9.981                 | 626.679 | -0.118  | 12.64   |
| 07/17/96 | 7:45:00 | 1111      | 9.983                 | 626.677 | -0.12   | 12.65   |
| 07/17/96 | 7:46:00 | 1112      | 9.983                 | 626.677 | -0.12   | 12.64   |
| 07/17/96 | 7:47:00 | 1113      | 9.985                 | 626.675 | -0.122  | 12.65   |
| 07/17/96 | 7:48:00 | 1114      | 9.983                 | 626.677 | -0.12   | 12.64   |
| 07/17/96 | 7:49:00 | 1115      | 9.983                 | 626.677 | -0.12   | 12.64   |
| 07/17/96 | 7:50:00 | 1116      | 9.985                 | 626.675 | -0.122  | 12.65   |
| 07/17/96 | 7:51:00 | 1117      | 9.985                 | 626.675 | -0.122  | 12.65   |
| 07/17/96 | 7:52:00 | 1118      | 9.985                 | 626.675 | -0.122  | 12.65   |
| 07/17/96 | 7:53:00 | 1119      | 9.983                 | 626.677 | -0.12   | 12.64   |
| 07/17/96 | 7:54:00 | 1120      | 9.985                 | 626.675 | -0.122  | 12.65   |
| 07/17/96 | 7:55:00 | 1121      | 9.985                 | 626.675 | -0.122  | 12.65   |
| 07/17/96 | 7:56:00 | 1122      | 9.988                 | 626.672 | -0.125  | 12.65   |
| 07/17/96 | 7:57:00 | 1123      | 9.988                 | 626.672 | -0.125  | 12.65   |
| 07/17/96 | 7:58:00 | 1124      | 9.988                 | 626.672 | -0.125  | 12.65   |
| 07/17/96 | 7:59:00 | 1125      | 9.988                 | 626.672 | -0.125  | 12.64   |
| 07/17/96 | 8:00:00 | 1126      | 9.988                 | 626.672 | -0.125  | 12.65   |
| 07/17/96 | 8:01:00 | 1127      | 9.988                 | 626.672 | -0.125  | 12.65   |
| 07/17/96 | 8:02:00 | 1128      | 9.988                 | 626.672 | -0.125  | 12.65   |
| 07/17/96 | 8:03:00 | 1129      | 9.99                  | 626.67  | -0.127  | 12.65   |
| 07/17/96 | 8:04:00 | 1130      | 9.99                  | 626.67  | -0.127  | 12.65   |
| 07/17/96 | 8:05:00 | 1131      | 9.988                 | 626.672 | -0.125  | 12.65   |
| 07/17/96 | 8:06:00 | 1132      | 9.99                  | 626.67  | -0.127  | 12.65   |
| 07/17/96 | 8:07:00 | 1133      | 9.988                 | 626.672 | -0.125  | 12.65   |
| 07/17/96 | 8:08:00 | 1134      | 9.988                 | 626.672 | -0.125  | 12.65   |
| 07/17/96 | 8:09:00 | 1135      | 9.988                 | 626.672 | -0.125  | 12.65   |
| 07/17/96 | 8:10:00 | 1136      | 9.988                 | 626.672 | -0.125  | 12.65   |
| 07/17/96 | 8:11:00 | 1137      | 9.988                 | 626.672 | -0.125  | 12.65   |
| 07/17/96 | 8:12:00 | 1138      | 9.988                 | 626.672 | -0.125  | 12.65   |
| 07/17/96 | 8:13:00 | 1139      | 9.985                 | 626.675 | -0.122  | 12.64   |
| 07/17/96 | 8:14:00 | 1140      | 9.99                  | 626.67  | -0.127  | 12.65   |

| Date     | Time     | ET (min) |    | Feet H2O | Feet H2O | Celsius |
|----------|----------|----------|----|----------|----------|---------|
| 07/16/96 | 13:14:00 | 74       | 0  | 627.234  | -0.096   | 15.47   |
| 07/16/96 | 13:15:00 | 75       | 1  | 627.234  | -0.096   | 15.47   |
| 07/16/96 | 13:16:00 | 76       | 2  | 627.234  | -0.096   | 15.47   |
| 07/16/96 | 13:17:00 | 77       | 3  | 627.234  | -0.096   | 15.47   |
| 07/16/96 | 13:18:00 | 78       | 4  | 627.229  | -0.101   | 15.47   |
| 07/16/96 | 13:19:00 | 79       | 5  | 627.229  | -0.101   | 15.47   |
| 07/16/96 | 13:20:00 | 80       | 6  | 627.229  | -0.101   | 15.48   |
| 07/16/96 | 13:21:00 | 81       | 7  | 627.229  | -0.101   | 15.48   |
| 07/16/96 | 13:22:00 | 82       | 8  | 627.229  | -0.101   | 15.47   |
| 07/16/96 | 13:23:00 | 83       | 9  | 627.224  | -0.106   | 15.48   |
| 07/16/96 | 13:24:00 | 84       | 10 | 627.224  | -0.106   | 15.48   |
| 07/16/96 | 13:25:00 | 85       | 11 | 627.224  | -0.106   | 15.48   |
| 07/16/96 | 13:26:00 | 86       | 12 | 627.224  | -0.106   | 15.48   |
| 07/16/96 | 13:27:00 | 87       | 13 | 627.224  | -0.106   | 15.48   |
| 07/16/96 | 13:28:00 | 88       | 14 | 627.222  | -0.108   | 15.48   |
| 07/16/96 | 13:29:00 | 89       | 15 | 627.222  | -0.108   | 15.48   |
| 07/16/96 | 13:30:00 | 90       | 16 | 627.222  | -0.108   | 15.48   |
| 07/16/96 | 13:31:00 | 91       | 17 | 627.222  | -0.108   | 15.48   |
| 07/16/96 | 13:32:00 | 92       | 18 | 627.217  | -0.113   | 15.48   |
| 07/16/96 | 13:33:00 | 93       | 19 | 627.217  | -0.113   | 15.48   |
| 07/16/96 | 13:34:00 | 94       | 20 | 627.217  | -0.113   | 15.48   |
| 07/16/96 | 13:35:00 | 95       | 21 | 627.217  | -0.113   | 15.48   |
| 07/16/96 | 13:36:00 | 96       | 22 | 627.217  | -0.113   | 15.48   |
| 07/16/96 | 13:37:00 | 97       | 23 | 627.213  | -0.117   | 15.48   |
| 07/16/96 | 13:38:00 | 98       | 24 | 627.213  | -0.117   | 15.48   |
| 07/16/96 | 13:39:00 | 99       | 25 | 627.208  | -0.122   | 15.48   |
| 07/16/96 | 13:40:00 | 100      | 26 | 627.208  | -0.122   | 15.48   |
| 07/16/96 | 13:41:00 | 101      | 27 | 627.208  | -0.122   | 15.48   |
| 07/16/96 | 13:42:00 | 102      | 28 | 627.208  | -0.122   | 15.48   |
| 07/16/96 | 13:43:00 | 103      | 29 | 627.208  | -0.122   | 15.48   |
| 07/16/96 | 13:44:00 | 104      | 30 | 627.208  | -0.122   | 15.48   |
| 07/16/96 | 13:45:00 | 105      | 31 | 627.208  | -0.122   | 15.48   |
| 07/16/96 | 13:46:00 | 106      | 32 | 627.204  | -0.126   | 15.48   |
| 07/16/96 | 13:47:00 | 107      | 33 | 627.199  | -0.131   | 15.49   |
| 07/16/96 | 13:48:00 | 108      | 34 | 627.199  | -0.131   | 15.48   |
| 07/16/96 | 13:49:00 | 109      | 35 | 627.199  | -0.131   | 15.49   |
| 07/16/96 | 13:50:00 | 110      | 36 | 627.194  | -0.136   | 15.48   |
| 07/16/96 | 13:51:00 | 111      | 37 | 627.199  | -0.131   | 15.48   |
| 07/16/96 | 13:52:00 | 112      | 38 | 627.199  | -0.131   | 15.49   |
| 07/16/96 | 13:53:00 | 113      | 39 | 627.194  | -0.136   | 15.49   |
| 07/16/96 | 13:54:00 | 114      | 40 | 627.194  | -0.136   | 15.48   |
| 07/16/96 | 13:55:00 | 115      | 41 | 627.194  | -0.136   | 15.48   |
| 07/16/96 | 13:56:00 | 116      | 42 | 627.194  | -0.136   | 15.49   |
| 07/16/96 | 13:57:00 | 117      | 43 | 627.194  | -0.136   | 15.49   |
| 07/16/96 | 13:58:00 | 118      | 44 | 627.19   | -0.14    | 15.49   |
| 07/16/96 | 13:59:00 | 119      | 45 | 627.19   | -0.14    | 15.48   |
| 07/16/96 | 14:00:00 | 120      | 46 | 627.19   | -0.14    | 15.49   |
| 07/16/96 | 14:01:00 | 121      | 47 | 627.19   | -0.14    | 15.49   |
| 07/16/96 | 14:02:00 | 122      | 48 | 627.19   | -0.14    | 15.49   |
| 07/16/96 | 14:03:00 | 123      | 49 | 627.19   | -0.14    | 15.49   |

| Date     | Time     | ET (min) |    | Feet H2O | Feet H2O | Celsius |
|----------|----------|----------|----|----------|----------|---------|
| 07/16/96 | 14:04:00 | 124      | 50 | 627.185  | -0.145   | 15.49   |
| 07/16/96 | 14:05:00 | 125      | 51 | 627.185  | -0.145   | 15.49   |
| 07/16/96 | 14:06:00 | 126      | 52 | 627.185  | -0.145   | 15.49   |
| 07/16/96 | 14:07:00 | 127      | 53 | 627.19   | -0.14    | 15.49   |
| 07/16/96 | 14:08:00 | 128      | 54 | 627.185  | -0.145   | 15.49   |
| 07/16/96 | 14:09:00 | 129      | 55 | 627.185  | -0.145   | 15.49   |
| 07/16/96 | 14:10:00 | 130      | 56 | 627.181  | -0.149   | 15.49   |
| 07/16/96 | 14:11:00 | 131      | 57 | 627.181  | -0.149   | 15.5    |
| 07/16/96 | 14:12:00 | 132      | 58 | 627.181  | -0.149   | 15.49   |
| 07/16/96 | 14:13:00 | 133      | 59 | 627.181  | -0.149   | 15.5    |
| 07/16/96 | 14:14:00 | 134      | 60 | 627.181  | -0.149   | 15.49   |
| 07/16/96 | 14:15:00 | 135      | 61 | 627.176  | -0.154   | 15.49   |
| 07/16/96 | 14:16:00 | 136      | 62 | 627.176  | -0.154   | 15.49   |
| 07/16/96 | 14:17:00 | 137      | 63 | 627.171  | -0.159   | 15.49   |
| 07/16/96 | 14:18:00 | 138      | 64 | 627.171  | -0.159   | 15.49   |
| 07/16/96 | 14:19:00 | 139      | 65 | 627.176  | -0.154   | 15.49   |
| 07/16/96 | 14:20:00 | 140      | 66 | 627.176  | -0.154   | 15.5    |
| 07/16/96 | 14:21:00 | 141      | 67 | 627.171  | -0.159   | 15.49   |
| 07/16/96 | 14:22:00 | 142      | 68 | 627.171  | -0.159   | 15.49   |
| 07/16/96 | 14:23:00 | 143      | 69 | 627.171  | -0.159   | 15.49   |
| 07/16/96 | 14:24:00 | 144      | 70 | 627.171  | -0.159   | 15.5    |
| 07/16/96 | 14:25:00 | 145      | 71 | 627.171  | -0.159   | 15.5    |
| 07/16/96 | 14:26:00 | 146      | 72 | 627.171  | -0.159   | 15.5    |
| 07/16/96 | 14:27:00 | 147      | 73 | 627.171  | -0.159   | 15.5    |
| 07/16/96 | 14:28:00 | 148      | 74 | 627.167  | -0.163   | 15.5    |
| 07/16/96 | 14:29:00 | 149      | 75 | 627.167  | -0.163   | 15.5    |
| 07/16/96 | 14:30:00 | 150      | 76 | 627.162  | -0.168   | 15.5    |
| 07/16/96 | 14:31:00 | 151      | 77 | 627.167  | -0.163   | 15.5    |
| 07/16/96 | 14:32:00 | 152      | 78 | 627.167  | -0.163   | 15.5    |
| 07/16/96 | 14:33:00 | 153      | 79 | 627.167  | -0.163   | 15.5    |
| 07/16/96 | 14:34:00 | 154      | 80 | 627.167  | -0.163   | 15.5    |
| 07/16/96 | 14:35:00 | 155      | 81 | 627.162  | -0.168   | 15.5    |
| 07/16/96 | 14:36:00 | 156      | 82 | 627.157  | -0.173   | 15.5    |
| 07/16/96 | 14:37:00 | 157      | 83 | 627.162  | -0.168   | 15.5    |
| 07/16/96 | 14:38:00 | 158      | 84 | 627.162  | -0.168   | 15.49   |
| 07/16/96 | 14:39:00 | 159      | 85 | 627.157  | -0.173   | 15.5    |
| 07/16/96 | 14:40:00 | 160      | 86 | 627.162  | -0.168   | 15.49   |
| 07/16/96 | 14:41:00 | 161      | 87 | 627.157  | -0.173   | 15.49   |
| 07/16/96 | 14:42:00 | 162      | 88 | 627.157  | -0.173   | 15.5    |
| 07/16/96 | 14:43:00 | 163      | 89 | 627.157  | -0.173   | 15.5    |
| 07/16/96 | 14:44:00 | 164      | 90 | 627.157  | -0.173   | 15.5    |
| 07/16/96 | 14:45:00 | 165      | 91 | 627.157  | -0.173   | 15.49   |
| 07/16/96 | 14:46:00 | 166      | 92 | 627.153  | -0.177   | 15.49   |
| 07/16/96 | 14:47:00 | 167      | 93 | 627.157  | -0.173   | 15.5    |
| 07/16/96 | 14:48:00 | 168      | 94 | 627.153  | -0.177   | 15.5    |
| 07/16/96 | 14:49:00 | 169      | 95 | 627.153  | -0.177   | 15.5    |
| 07/16/96 | 14:50:00 | 170      | 96 | 627.153  | -0.177   | 15.5    |
| 07/16/96 | 14:51:00 | 171      | 97 | 627.153  | -0.177   | 15.5    |
| 07/16/96 | 14:52:00 | 172      | 98 | 627.153  | -0.177   | 15.5    |
| 07/16/96 | 14:53:00 | 173      | 99 | 627.153  | -0.177   | 15.5    |

| Date     | Time     | ET (min) |     | Feet H2O | Feet H2O | Celsius |
|----------|----------|----------|-----|----------|----------|---------|
| 07/16/96 | 14:54:00 | 174      | 100 | 627.153  | -0.177   | 15.5    |
| 07/16/96 | 14:55:00 | 175      | 101 | 627.148  | -0.182   | 15.5    |
| 07/16/96 | 14:56:00 | 176      | 102 | 627.148  | -0.182   | 15.5    |
| 07/16/96 | 14:57:00 | 177      | 103 | 627.148  | -0.182   | 15.5    |
| 07/16/96 | 14:58:00 | 178      | 104 | 627.148  | -0.182   | 15.5    |
| 07/16/96 | 14:59:00 | 179      | 105 | 627.148  | -0.182   | 15.5    |
| 07/16/96 | 15:00:00 | 180      | 106 | 627.148  | -0.182   | 15.5    |
| 07/16/96 | 15:01:00 | 181      | 107 | 627.148  | -0.182   | 15.5    |
| 07/16/96 | 15:02:00 | 182      | 108 | 627.148  | -0.182   | 15.5    |
| 07/16/96 | 15:03:00 | 183      | 109 | 627.144  | -0.186   | 15.5    |
| 07/16/96 | 15:04:00 | 184      | 110 | 627.144  | -0.186   | 15.5    |
| 07/16/96 | 15:05:00 | 185      | 111 | 627.144  | -0.186   | 15.5    |
| 07/16/96 | 15:06:00 | 186      | 112 | 627.144  | -0.186   | 15.5    |
| 07/16/96 | 15:07:00 | 187      | 113 | 627.144  | -0.186   | 15.49   |
| 07/16/96 | 15:08:00 | 188      | 114 | 627.144  | -0.186   | 15.5    |
| 07/16/96 | 15:09:00 | 189      | 115 | 627.144  | -0.186   | 15.5    |
| 07/16/96 | 15:10:00 | 190      | 116 | 627.139  | -0.191   | 15.5    |
| 07/16/96 | 15:11:00 | 191      | 117 | 627.139  | -0.191   | 15.5    |
| 07/16/96 | 15:12:00 | 192      | 118 | 627.139  | -0.191   | 15.5    |
| 07/16/96 | 15:13:00 | 193      | 119 | 627.144  | -0.186   | 15.5    |
| 07/16/96 | 15:14:00 | 194      | 120 | 627.139  | -0.191   | 15.5    |
| 07/16/96 | 15:15:00 | 195      | 121 | 627.139  | -0.191   | 15.5    |
| 07/16/96 | 15:16:00 | 196      | 122 | 627.139  | -0.191   | 15.5    |
| 07/16/96 | 15:17:00 | 197      | 123 | 627.139  | -0.191   | 15.5    |
| 07/16/96 | 15:18:00 | 198      | 124 | 627.137  | -0.193   | 15.5    |
| 07/16/96 | 15:19:00 | 199      | 125 | 627.137  | -0.193   | 15.5    |
| 07/16/96 | 15:20:00 | 200      | 126 | 627.137  | -0.193   | 15.5    |
| 07/16/96 | 15:21:00 | 201      | 127 | 627.137  | -0.193   | 15.49   |
| 07/16/96 | 15:22:00 | 202      | 128 | 627.137  | -0.193   | 15.5    |
| 07/16/96 | 15:23:00 | 203      | 129 | 627.137  | -0.193   | 15.5    |
| 07/16/96 | 15:24:00 | 204      | 130 | 627.137  | -0.193   | 15.5    |
| 07/16/96 | 15:25:00 | 205      | 131 | 627.137  | -0.193   | 15.5    |
| 07/16/96 | 15:26:00 | 206      | 132 | 627.132  | -0.198   | 15.5    |
| 07/16/96 | 15:27:00 | 207      | 133 | 627.132  | -0.198   | 15.5    |
| 07/16/96 | 15:28:00 | 208      | 134 | 627.132  | -0.198   | 15.5    |
| 07/16/96 | 15:29:00 | 209      | 135 | 627.132  | -0.198   | 15.5    |
| 07/16/96 | 15:30:00 | 210      | 136 | 627.132  | -0.198   | 15.5    |
| 07/16/96 | 15:31:00 | 211      | 137 | 627.128  | -0.202   | 15.5    |
| 07/16/96 | 15:32:00 | 212      | 138 | 627.132  | -0.198   | 15.5    |
| 07/16/96 | 15:33:00 | 213      | 139 | 627.132  | -0.198   | 15.5    |
| 07/16/96 | 15:34:00 | 214      | 140 | 627.128  | -0.202   | 15.5    |
| 07/16/96 | 15:35:00 | 215      | 141 | 627.128  | -0.202   | 15.5    |
| 07/16/96 | 15:36:00 | 216      | 142 | 627.128  | -0.202   | 15.5    |
| 07/16/96 | 15:37:00 | 217      | 143 | 627.128  | -0.202   | 15.5    |
| 07/16/96 | 15:38:00 | 218      | 144 | 627.128  | -0.202   | 15.5    |
| 07/16/96 | 15:39:00 | 219      | 145 | 627.128  | -0.202   | 15.5    |
| 07/16/96 | 15:40:00 | 220      | 146 | 627.128  | -0.202   | 15.5    |
| 07/16/96 | 15:41:00 | 221      | 147 | 627.123  | -0.207   | 15.5    |
| 07/16/96 | 15:42:00 | 222      | 148 | 627.128  | -0.202   | 15.5    |
| 07/16/96 | 15:43:00 | 223      | 149 | 627.128  | -0.202   | 15.5    |

| Date     | Time     | ET (min) |     | Feet H2O | Feet H2O | Celsius |
|----------|----------|----------|-----|----------|----------|---------|
| 07/16/96 | 15:44:00 | 224      | 150 | 627.123  | -0.207   | 15.5    |
| 07/16/96 | 15:45:00 | 225      | 151 | 627.123  | -0.207   | 15.5    |
| 07/16/96 | 15:46:00 | 226      | 152 | 627.118  | -0.212   | 15.5    |
| 07/16/96 | 15:47:00 | 227      | 153 | 627.123  | -0.207   | 15.5    |
| 07/16/96 | 15:48:00 | 228      | 154 | 627.123  | -0.207   | 15.5    |
| 07/16/96 | 15:49:00 | 229      | 155 | 627.118  | -0.212   | 15.5    |
| 07/16/96 | 15:50:00 | 230      | 156 | 627.118  | -0.212   | 15.5    |
| 07/16/96 | 15:51:00 | 231      | 157 | 627.118  | -0.212   | 15.5    |
| 07/16/96 | 15:52:00 | 232      | 158 | 627.118  | -0.212   | 15.5    |
| 07/16/96 | 15:53:00 | 233      | 159 | 627.118  | -0.212   | 15.5    |
| 07/16/96 | 15:54:00 | 234      | 160 | 627.114  | -0.216   | 15.5    |
| 07/16/96 | 15:55:00 | 235      | 161 | 627.118  | -0.212   | 15.5    |
| 07/16/96 | 15:56:00 | 236      | 162 | 627.114  | -0.216   | 15.5    |
| 07/16/96 | 15:57:00 | 237      | 163 | 627.114  | -0.216   | 15.5    |
| 07/16/96 | 15:58:00 | 238      | 164 | 627.114  | -0.216   | 15.5    |
| 07/16/96 | 15:59:00 | 239      | 165 | 627.118  | -0.212   | 15.5    |
| 07/16/96 | 16:00:00 | 240      | 166 | 627.114  | -0.216   | 15.5    |
| 07/16/96 | 16:01:00 | 241      | 167 | 627.114  | -0.216   | 15.5    |
| 07/16/96 | 16:02:00 | 242      | 168 | 627.114  | -0.216   | 15.5    |
| 07/16/96 | 16:03:00 | 243      | 169 | 627.114  | -0.216   | 15.51   |
| 07/16/96 | 16:04:00 | 244      | 170 | 627.114  | -0.216   | 15.5    |
| 07/16/96 | 16:05:00 | 245      | 171 | 627.114  | -0.216   | 15.5    |
| 07/16/96 | 16:06:00 | 246      | 172 | 627.114  | -0.216   | 15.5    |
| 07/16/96 | 16:07:00 | 247      | 173 | 627.109  | -0.221   | 15.51   |
| 07/16/96 | 16:08:00 | 248      | 174 | 627.109  | -0.221   | 15.5    |
| 07/16/96 | 16:09:00 | 249      | 175 | 627.109  | -0.221   | 15.51   |
| 07/16/96 | 16:10:00 | 250      | 176 | 627.109  | -0.221   | 15.51   |
| 07/16/96 | 16:11:00 | 251      | 177 | 627.109  | -0.221   | 15.51   |
| 07/16/96 | 16:12:00 | 252      | 178 | 627.109  | -0.221   | 15.51   |
| 07/16/96 | 16:13:00 | 253      | 179 | 627.109  | -0.221   | 15.51   |
| 07/16/96 | 16:14:00 | 254      | 180 | 627.104  | -0.226   | 15.51   |
| 07/16/96 | 16:15:00 | 255      | 181 | 627.104  | -0.226   | 15.51   |
| 07/16/96 | 16:16:00 | 256      | 182 | 627.104  | -0.226   | 15.51   |
| 07/16/96 | 16:17:00 | 257      | 183 | 627.104  | -0.226   | 15.51   |
| 07/16/96 | 16:18:00 | 258      | 184 | 627.104  | -0.226   | 15.51   |
| 07/16/96 | 16:19:00 | 259      | 185 | 627.104  | -0.226   | 15.51   |
| 07/16/96 | 16:20:00 | 260      | 186 | 627.104  | -0.226   | 15.51   |
| 07/16/96 | 16:21:00 | 261      | 187 | 627.104  | -0.226   | 15.5    |
| 07/16/96 | 16:22:00 | 262      | 188 | 627.104  | -0.226   | 15.5    |
| 07/16/96 | 16:23:00 | 263      | 189 | 627.104  | -0.226   | 15.5    |
| 07/16/96 | 16:24:00 | 264      | 190 | 627.104  | -0.226   | 15.51   |
| 07/16/96 | 16:25:00 | 265      | 191 | 627.104  | -0.226   | 15.5    |
| 07/16/96 | 16:26:00 | 266      | 192 | 627.104  | -0.226   | 15.51   |
| 07/16/96 | 16:27:00 | 267      | 193 | 627.1    | -0.23    | 15.5    |
| 07/16/96 | 16:28:00 | 268      | 194 | 627.1    | -0.23    | 15.5    |
| 07/16/96 | 16:29:00 | 269      | 195 | 627.1    | -0.23    | 15.51   |
| 07/16/96 | 16:30:00 | 270      | 196 | 627.1    | -0.23    | 15.5    |
| 07/16/96 | 16:31:00 | 271      | 197 | 627.1    | -0.23    | 15.5    |
| 07/16/96 | 16:32:00 | 272      | 198 | 627.1    | -0.23    | 15.5    |
| 07/16/96 | 16:33:00 | 273      | 199 | 627.1    | -0.23    | 15.51   |

| Date     | Time     | ET (min) |     | Feet H2O | Feet H2O | Celsius |
|----------|----------|----------|-----|----------|----------|---------|
| 07/16/96 | 16:34:00 | 274      | 200 | 627.1    | -0.23    | 15.51   |
| 07/16/96 | 16:35:00 | 275      | 201 | 627.1    | -0.23    | 15.5    |
| 07/16/96 | 16:36:00 | 276      | 202 | 627.095  | -0.235   | 15.51   |
| 07/16/96 | 16:37:00 | 277      | 203 | 627.095  | -0.235   | 15.51   |
| 07/16/96 | 16:38:00 | 278      | 204 | 627.095  | -0.235   | 15.51   |
| 07/16/96 | 16:39:00 | 279      | 205 | 627.095  | -0.235   | 15.51   |
| 07/16/96 | 16:40:00 | 280      | 206 | 627.095  | -0.235   | 15.51   |
| 07/16/96 | 16:41:00 | 281      | 207 | 627.091  | -0.239   | 15.51   |
| 07/16/96 | 16:42:00 | 282      | 208 | 627.095  | -0.235   | 15.51   |
| 07/16/96 | 16:43:00 | 283      | 209 | 627.095  | -0.235   | 15.52   |
| 07/16/96 | 16:44:00 | 284      | 210 | 627.095  | -0.235   | 15.51   |
| 07/16/96 | 16:45:00 | 285      | 211 | 627.095  | -0.235   | 15.51   |
| 07/16/96 | 16:46:00 | 286      | 212 | 627.091  | -0.239   | 15.52   |
| 07/16/96 | 16:47:00 | 287      | 213 | 627.091  | -0.239   | 15.52   |
| 07/16/96 | 16:48:00 | 288      | 214 | 627.091  | -0.239   | 15.52   |
| 07/16/96 | 16:49:00 | 289      | 215 | 627.091  | -0.239   | 15.51   |
| 07/16/96 | 16:50:00 | 290      | 216 | 627.091  | -0.239   | 15.51   |
| 07/16/96 | 16:51:00 | 291      | 217 | 627.091  | -0.239   | 15.51   |
| 07/16/96 | 16:52:00 | 292      | 218 | 627.086  | -0.244   | 15.52   |
| 07/16/96 | 16:53:00 | 293      | 219 | 627.091  | -0.239   | 15.52   |
| 07/16/96 | 16:54:00 | 294      | 220 | 627.086  | -0.244   | 15.52   |
| 07/16/96 | 16:55:00 | 295      | 221 | 627.091  | -0.239   | 15.51   |
| 07/16/96 | 16:56:00 | 296      | 222 | 627.086  | -0.244   | 15.51   |
| 07/16/96 | 16:57:00 | 297      | 223 | 627.086  | -0.244   | 15.51   |
| 07/16/96 | 16:58:00 | 298      | 224 | 627.086  | -0.244   | 15.52   |
| 07/16/96 | 16:59:00 | 299      | 225 | 627.086  | -0.244   | 15.51   |
| 07/16/96 | 17:00:00 | 300      | 226 | 627.086  | -0.244   | 15.51   |
| 07/16/96 | 17:01:00 | 301      | 227 | 627.081  | -0.249   | 15.51   |
| 07/16/96 | 17:02:00 | 302      | 228 | 627.086  | -0.244   | 15.51   |
| 07/16/96 | 17:03:00 | 303      | 229 | 627.086  | -0.244   | 15.52   |
| 07/16/96 | 17:04:00 | 304      | 230 | 627.086  | -0.244   | 15.52   |
| 07/16/96 | 17:05:00 | 305      | 231 | 627.086  | -0.244   | 15.52   |
| 07/16/96 | 17:06:00 | 306      | 232 | 627.081  | -0.249   | 15.52   |
| 07/16/96 | 17:07:00 | 307      | 233 | 627.081  | -0.249   | 15.51   |
| 07/16/96 | 17:08:00 | 308      | 234 | 627.081  | -0.249   | 15.52   |
| 07/16/96 | 17:09:00 | 309      | 235 | 627.077  | -0.253   | 15.52   |
| 07/16/96 | 17:10:00 | 310      | 236 | 627.081  | -0.249   | 15.52   |
| 07/16/96 | 17:11:00 | 311      | 237 | 627.077  | -0.253   | 15.52   |
| 07/16/96 | 17:12:00 | 312      | 238 | 627.081  | -0.249   | 15.52   |
| 07/16/96 | 17:13:00 | 313      | 239 | 627.081  | -0.249   | 15.52   |
| 07/16/96 | 17:14:00 | 314      | 240 | 627.081  | -0.249   | 15.52   |
| 07/16/96 | 17:15:00 | 315      | 241 | 627.081  | -0.249   | 15.52   |
| 07/16/96 | 17:16:00 | 316      | 242 | 627.081  | -0.249   | 15.52   |
| 07/16/96 | 17:17:00 | 317      | 243 | 627.081  | -0.249   | 15.52   |
| 07/16/96 | 17:18:00 | 318      | 244 | 627.077  | -0.253   | 15.52   |
| 07/16/96 | 17:19:00 | 319      | 245 | 627.081  | -0.249   | 15.52   |
| 07/16/96 | 17:20:00 | 320      | 246 | 627.077  | -0.253   | 15.52   |
| 07/16/96 | 17:21:00 | 321      | 247 | 627.077  | -0.253   | 15.52   |
| 07/16/96 | 17:22:00 | 322      | 248 | 627.077  | -0.253   | 15.52   |
| 07/16/96 | 17:23:00 | 323      | 249 | 627.077  | -0.253   | 15.52   |

| Date     | Time     | ET (min) |     | Feet H2O | Feet H2O | Celsius |
|----------|----------|----------|-----|----------|----------|---------|
| 07/16/96 | 17:24:00 | 324      | 250 | 627.077  | -0.253   | 15.52   |
| 07/16/96 | 17:25:00 | 325      | 251 | 627.077  | -0.253   | 15.52   |
| 07/16/96 | 17:26:00 | 326      | 252 | 627.077  | -0.253   | 15.52   |
| 07/16/96 | 17:27:00 | 327      | 253 | 627.072  | -0.258   | 15.52   |
| 07/16/96 | 17:28:00 | 328      | 254 | 627.072  | -0.258   | 15.52   |
| 07/16/96 | 17:29:00 | 329      | 255 | 627.072  | -0.258   | 15.52   |
| 07/16/96 | 17:30:00 | 330      | 256 | 627.072  | -0.258   | 15.52   |
| 07/16/96 | 17:31:00 | 331      | 257 | 627.072  | -0.258   | 15.52   |
| 07/16/96 | 17:32:00 | 332      | 258 | 627.072  | -0.258   | 15.52   |
| 07/16/96 | 17:33:00 | 333      | 259 | 627.072  | -0.258   | 15.52   |
| 07/16/96 | 17:34:00 | 334      | 260 | 627.072  | -0.258   | 15.52   |
| 07/16/96 | 17:35:00 | 335      | 261 | 627.072  | -0.258   | 15.52   |
| 07/16/96 | 17:36:00 | 336      | 262 | 627.068  | -0.262   | 15.52   |
| 07/16/96 | 17:37:00 | 337      | 263 | 627.068  | -0.262   | 15.52   |
| 07/16/96 | 17:38:00 | 338      | 264 | 627.072  | -0.258   | 15.52   |
| 07/16/96 | 17:39:00 | 339      | 265 | 627.068  | -0.262   | 15.52   |
| 07/16/96 | 17:40:00 | 340      | 266 | 627.068  | -0.262   | 15.52   |
| 07/16/96 | 17:41:00 | 341      | 267 | 627.068  | -0.262   | 15.52   |
| 07/16/96 | 17:42:00 | 342      | 268 | 627.068  | -0.262   | 15.52   |
| 07/16/96 | 17:43:00 | 343      | 269 | 627.068  | -0.262   | 15.52   |
| 07/16/96 | 17:44:00 | 344      | 270 | 627.068  | -0.262   | 15.52   |
| 07/16/96 | 17:45:00 | 345      | 271 | 627.068  | -0.262   | 15.52   |
| 07/16/96 | 17:46:00 | 346      | 272 | 627.068  | -0.262   | 15.52   |
| 07/16/96 | 17:47:00 | 347      | 273 | 627.068  | -0.262   | 15.52   |
| 07/16/96 | 17:48:00 | 348      | 274 | 627.068  | -0.262   | 15.52   |
| 07/16/96 | 17:49:00 | 349      | 275 | 627.068  | -0.262   | 15.52   |
| 07/16/96 | 17:50:00 | 350      | 276 | 627.063  | -0.267   | 15.52   |
| 07/16/96 | 17:51:00 | 351      | 277 | 627.068  | -0.262   | 15.52   |
| 07/16/96 | 17:52:00 | 352      | 278 | 627.063  | -0.267   | 15.52   |
| 07/16/96 | 17:53:00 | 353      | 279 | 627.063  | -0.267   | 15.52   |
| 07/16/96 | 17:54:00 | 354      | 280 | 627.063  | -0.267   | 15.52   |
| 07/16/96 | 17:55:00 | 355      | 281 | 627.063  | -0.267   | 15.52   |
| 07/16/96 | 17:56:00 | 356      | 282 | 627.063  | -0.267   | 15.52   |
| 07/16/96 | 17:57:00 | 357      | 283 | 627.063  | -0.267   | 15.52   |
| 07/16/96 | 17:58:00 | 358      | 284 | 627.063  | -0.267   | 15.52   |
| 07/16/96 | 17:59:00 | 359      | 285 | 627.058  | -0.272   | 15.52   |
| 07/16/96 | 18:00:00 | 360      | 286 | 627.058  | -0.272   | 15.52   |
| 07/16/96 | 18:01:00 | 361      | 287 | 627.058  | -0.272   | 15.52   |
| 07/16/96 | 18:02:00 | 362      | 288 | 627.058  | -0.272   | 15.52   |
| 07/16/96 | 18:03:00 | 363      | 289 | 627.058  | -0.272   | 15.52   |
| 07/16/96 | 18:04:00 | 364      | 290 | 627.058  | -0.272   | 15.52   |
| 07/16/96 | 18:05:00 | 365      | 291 | 627.058  | -0.272   | 15.52   |
| 07/16/96 | 18:06:00 | 366      | 292 | 627.058  | -0.272   | 15.52   |
| 07/16/96 | 18:07:00 | 367      | 293 | 627.058  | -0.272   | 15.52   |
| 07/16/96 | 18:08:00 | 368      | 294 | 627.054  | -0.276   | 15.52   |
| 07/16/96 | 18:09:00 | 369      | 295 | 627.054  | -0.276   | 15.52   |
| 07/16/96 | 18:10:00 | 370      | 296 | 627.054  | -0.276   | 15.52   |
| 07/16/96 | 18:11:00 | 371      | 297 | 627.054  | -0.276   | 15.52   |
| 07/16/96 | 18:12:00 | 372      | 298 | 627.054  | -0.276   | 15.52   |
| 07/16/96 | 18:13:00 | 373      | 299 | 627.054  | -0.276   | 15.52   |

| Date     | Time     | ET (min) |     | Feet H2O | Feet H2O | Celsius |
|----------|----------|----------|-----|----------|----------|---------|
| 07/16/96 | 18:14:00 | 374      | 300 | 627.054  | -0.276   | 15.52   |
| 07/16/96 | 18:15:00 | 375      | 301 | 627.054  | -0.276   | 15.53   |
| 07/16/96 | 18:16:00 | 376      | 302 | 627.054  | -0.276   | 15.53   |
| 07/16/96 | 18:17:00 | 377      | 303 | 627.049  | -0.281   | 15.52   |
| 07/16/96 | 18:18:00 | 378      | 304 | 627.049  | -0.281   | 15.52   |
| 07/16/96 | 18:19:00 | 379      | 305 | 627.049  | -0.281   | 15.53   |
| 07/16/96 | 18:20:00 | 380      | 306 | 627.054  | -0.276   | 15.53   |
| 07/16/96 | 18:21:00 | 381      | 307 | 627.049  | -0.281   | 15.53   |
| 07/16/96 | 18:22:00 | 382      | 308 | 627.049  | -0.281   | 15.53   |
| 07/16/96 | 18:23:00 | 383      | 309 | 627.049  | -0.281   | 15.53   |
| 07/16/96 | 18:24:00 | 384      | 310 | 627.049  | -0.281   | 15.53   |
| 07/16/96 | 18:25:00 | 385      | 311 | 627.049  | -0.281   | 15.53   |
| 07/16/96 | 18:26:00 | 386      | 312 | 627.049  | -0.281   | 15.53   |
| 07/16/96 | 18:27:00 | 387      | 313 | 627.049  | -0.281   | 15.53   |
| 07/16/96 | 18:28:00 | 388      | 314 | 627.044  | -0.286   | 15.53   |
| 07/16/96 | 18:29:00 | 389      | 315 | 627.049  | -0.281   | 15.53   |
| 07/16/96 | 18:30:00 | 390      | 316 | 627.049  | -0.281   | 15.53   |
| 07/16/96 | 18:31:00 | 391      | 317 | 627.049  | -0.281   | 15.53   |
| 07/16/96 | 18:32:00 | 392      | 318 | 627.049  | -0.281   | 15.53   |
| 07/16/96 | 18:33:00 | 393      | 319 | 627.049  | -0.281   | 15.53   |
| 07/16/96 | 18:34:00 | 394      | 320 | 627.044  | -0.286   | 15.53   |
| 07/16/96 | 18:35:00 | 395      | 321 | 627.049  | -0.281   | 15.53   |
| 07/16/96 | 18:36:00 | 396      | 322 | 627.049  | -0.281   | 15.53   |
| 07/16/96 | 18:37:00 | 397      | 323 | 627.044  | -0.286   | 15.53   |
| 07/16/96 | 18:38:00 | 398      | 324 | 627.044  | -0.286   | 15.53   |
| 07/16/96 | 18:39:00 | 399      | 325 | 627.044  | -0.286   | 15.53   |
| 07/16/96 | 18:40:00 | 400      | 326 | 627.044  | -0.286   | 15.53   |
| 07/16/96 | 18:41:00 | 401      | 327 | 627.044  | -0.286   | 15.53   |
| 07/16/96 | 18:42:00 | 402      | 328 | 627.044  | -0.286   | 15.53   |
| 07/16/96 | 18:43:00 | 403      | 329 | 627.044  | -0.286   | 15.53   |
| 07/16/96 | 18:44:00 | 404      | 330 | 627.044  | -0.286   | 15.53   |
| 07/16/96 | 18:45:00 | 405      | 331 | 627.044  | -0.286   | 15.53   |
| 07/16/96 | 18:46:00 | 406      | 332 | 627.044  | -0.286   | 15.53   |
| 07/16/96 | 18:47:00 | 407      | 333 | 627.044  | -0.286   | 15.53   |
| 07/16/96 | 18:48:00 | 408      | 334 | 627.042  | -0.288   | 15.53   |
| 07/16/96 | 18:49:00 | 409      | 335 | 627.042  | -0.288   | 15.53   |
| 07/16/96 | 18:50:00 | 410      | 336 | 627.042  | -0.288   | 15.53   |
| 07/16/96 | 18:51:00 | 411      | 337 | 627.042  | -0.288   | 15.53   |

| Elapsed Time | INPUT 1 | INPUT 2 | INPUT 3 | INPUT 4 | INPUT 5 | INPUT 6 | INPUT 7 | INPUT 8 |
|--------------|---------|---------|---------|---------|---------|---------|---------|---------|
|              | RW-2    | MW-3    | 14S     | 14I     | DC-P3   | ATM     | MW-2R   | MW-6R   |
| 0            | 622.694 | -3.466  | 625.087 | -1.223  | 625.071 | -0.559  | 625.252 | -0.698  |
| 0.0083       | 622.731 | -3.429  | 625.087 | -1.223  | 625.078 | -0.552  | 625.252 | -0.698  |
| 0.0166       | 622.712 | -3.448  | 625.087 | -1.223  | 625.078 | -0.552  | 625.252 | -0.698  |
| 0.025        | 622.738 | -3.422  | 625.087 | -1.223  | 625.078 | -0.552  | 625.252 | -0.698  |
| 0.0333       | 622.738 | -3.422  | 625.087 | -1.223  | 625.078 | -0.552  | 625.252 | -0.698  |
| 0.0416       | 622.719 | -3.441  | 625.087 | -1.223  | 625.071 | -0.559  | 625.252 | -0.698  |
| 0.05         | 622.75  | -3.41   | 625.087 | -1.223  | 625.071 | -0.559  | 625.252 | -0.698  |
| 0.0583       | 623.381 | -2.779  | 625.087 | -1.223  | 625.078 | -0.552  | 625.252 | -0.698  |
| 0.0668       | 623.034 | -3.126  | 625.084 | -1.216  | 625.078 | -0.552  | 625.259 | -0.691  |
| 0.075        | 623.085 | -3.075  | 625.087 | -1.223  | 625.078 | -0.552  | 625.259 | -0.691  |
| 0.0833       | 623.11  | -3.05   | 625.087 | -1.223  | 625.071 | -0.559  | 625.252 | -0.698  |
| 0.0916       | 623.104 | -3.056  | 625.087 | -1.223  | 625.078 | -0.552  | 625.252 | -0.698  |
| 0.1          | 623.097 | -3.063  | 625.087 | -1.223  | 625.078 | -0.552  | 625.252 | -0.698  |
| 0.1083       | 623.079 | -3.081  | 625.087 | -1.223  | 625.071 | -0.559  | 625.252 | -0.698  |
| 0.1166       | 623.068 | -3.094  | 625.087 | -1.223  | 625.078 | -0.552  | 625.259 | -0.691  |
| 0.125        | 623.06  | -3.1    | 625.087 | -1.223  | 625.078 | -0.552  | 625.252 | -0.698  |
| 0.1333       | 623.072 | -3.088  | 625.087 | -1.223  | 625.078 | -0.552  | 625.259 | -0.691  |
| 0.1416       | 623.097 | -3.063  | 625.087 | -1.223  | 625.078 | -0.552  | 625.259 | -0.691  |
| 0.15         | 623.123 | -3.037  | 625.087 | -1.223  | 625.078 | -0.552  | 625.259 | -0.691  |
| 0.1583       | 623.148 | -3.012  | 625.094 | -1.216  | 625.078 | -0.552  | 625.259 | -0.691  |
| 0.1666       | 623.161 | -2.988  | 625.094 | -1.216  | 625.078 | -0.552  | 625.259 | -0.691  |
| 0.175        | 623.167 | -2.993  | 625.094 | -1.216  | 625.078 | -0.552  | 625.259 | -0.691  |
| 0.1833       | 623.161 | -2.999  | 625.094 | -1.216  | 625.084 | -0.546  | 625.259 | -0.691  |
| 0.1916       | 623.167 | -2.993  | 625.094 | -1.216  | 625.084 | -0.546  | 625.259 | -0.691  |
| 0.2          | 623.167 | -2.993  | 625.094 | -1.216  | 625.078 | -0.552  | 625.259 | -0.691  |
| 0.2083       | 623.173 | -2.987  | 625.094 | -1.216  | 625.078 | -0.552  | 625.259 | -0.691  |
| 0.2166       | 623.192 | -2.988  | 625.094 | -1.216  | 625.078 | -0.552  | 625.259 | -0.691  |
| 0.225        | 623.211 | -2.949  | 625.094 | -1.216  | 625.078 | -0.552  | 625.259 | -0.691  |
| 0.2333       | 623.23  | -2.93   | 625.094 | -1.216  | 625.078 | -0.552  | 625.259 | -0.691  |
| 0.2416       | 623.249 | -2.911  | 625.094 | -1.216  | 625.084 | -0.546  | 625.259 | -0.691  |
| 0.25         | 623.255 | -2.905  | 625.094 | -1.216  | 625.078 | -0.552  | 625.259 | -0.691  |
| 0.2583       | 623.255 | -2.905  | 625.094 | -1.216  | 625.078 | -0.552  | 625.259 | -0.691  |
| 0.2668       | 623.255 | -2.905  | 625.1   | -1.21   | 625.084 | -0.546  | 625.259 | -0.691  |
| 0.275        | 623.255 | -2.905  | 625.094 | -1.216  | 625.084 | -0.546  | 625.265 | -0.685  |
| 0.2833       | 623.262 | -2.888  | 625.094 | -1.216  | 625.078 | -0.552  | 625.265 | -0.685  |
| 0.2916       | 623.274 | -2.886  | 625.1   | -1.21   | 625.078 | -0.552  | 625.265 | -0.685  |
| 0.3          | 623.293 | -2.867  | 625.094 | -1.216  | 625.078 | -0.552  | 625.265 | -0.685  |
| 0.3083       | 623.306 | -2.854  | 625.1   | -1.21   | 625.084 | -0.546  | 625.265 | -0.685  |
| 0.3166       | 623.325 | -2.835  | 625.1   | -1.21   | 625.078 | -0.552  | 625.265 | -0.685  |
| 0.325        | 623.331 | -2.829  | 625.1   | -1.21   | 625.084 | -0.546  | 625.265 | -0.685  |
| 0.3333       | 623.337 | -2.823  | 625.1   | -1.21   | 625.084 | -0.546  | 625.265 | -0.685  |
| 0.35         | 623.337 | -2.823  | 625.1   | -1.21   | 625.084 | -0.546  | 625.265 | -0.685  |
| 0.3666       | 623.363 | -2.797  | 625.107 | -1.203  | 625.084 | -0.546  | 625.265 | -0.685  |
| 0.3833       | 623.388 | -2.772  | 625.1   | -1.21   | 625.084 | -0.546  | 625.271 | -0.679  |
| 0.4          | 623.413 | -2.747  | 625.107 | -1.203  | 625.084 | -0.546  | 625.265 | -0.685  |
| 0.4166       | 623.419 | -2.741  | 625.107 | -1.203  | 625.084 | -0.546  | 625.271 | -0.679  |

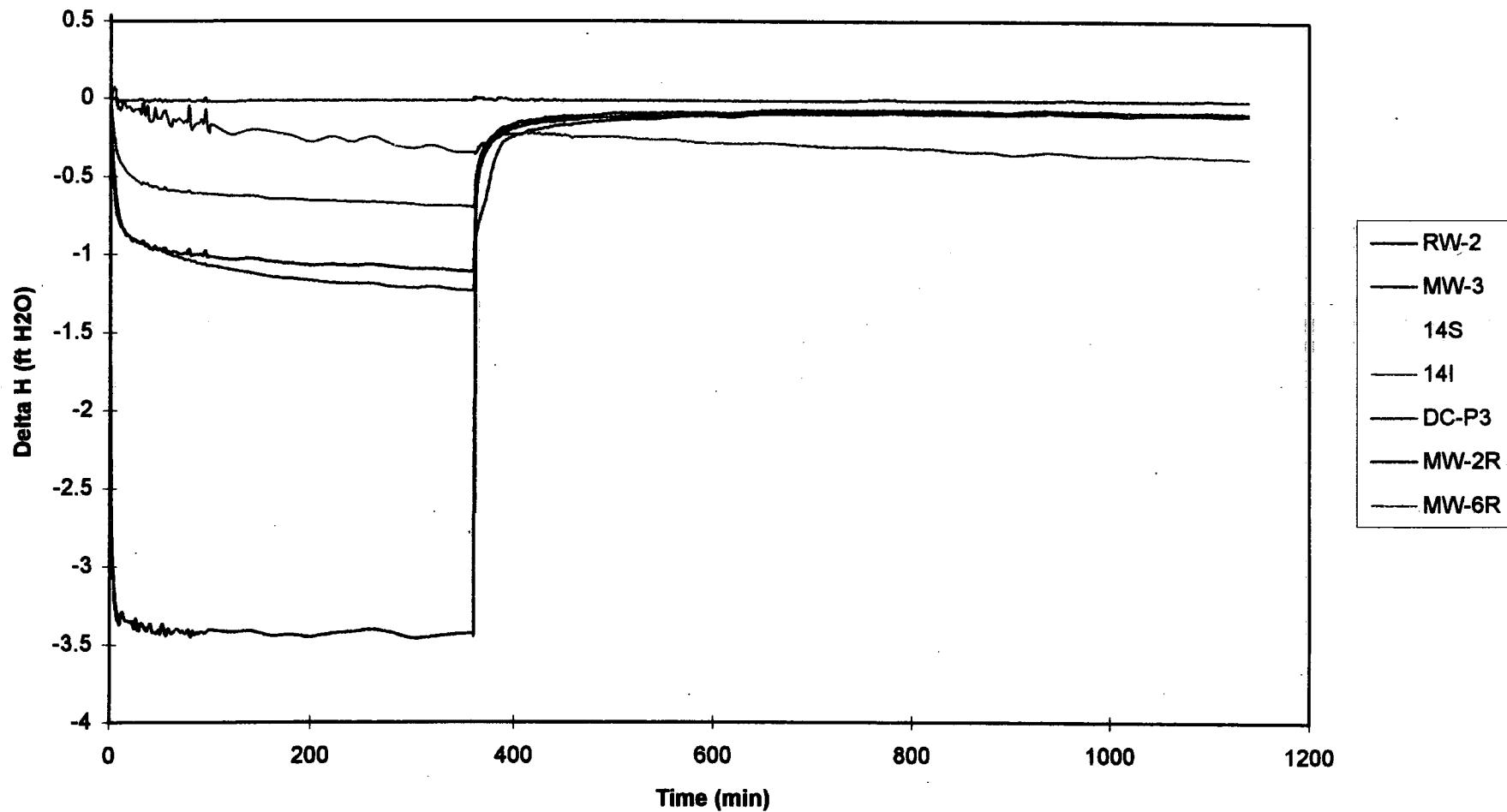
|        | RW-2    | MW-3   | 14S     | 14I    | DC-P3   | ATM    | MW-2R   | MW-6R  |
|--------|---------|--------|---------|--------|---------|--------|---------|--------|
| 0.4333 | 623.432 | -2.728 | 625.107 | -1.203 | 625.084 | -0.546 | 625.271 | -0.679 |
| 0.45   | 623.451 | -2.709 | 625.107 | -1.203 | 625.084 | -0.546 | 625.271 | -0.679 |
| 0.4666 | 623.476 | -2.684 | 625.113 | -1.197 | 625.084 | -0.546 | 625.271 | -0.679 |
| 0.4833 | 623.495 | -2.665 | 625.107 | -1.203 | 625.084 | -0.546 | 625.271 | -0.679 |
| 0.5    | 623.508 | -2.652 | 625.113 | -1.197 | 625.084 | -0.546 | 625.271 | -0.679 |
| 0.5166 | 623.52  | -2.64  | 625.113 | -1.197 | 625.084 | -0.546 | 625.271 | -0.679 |
| 0.5333 | 623.539 | -2.621 | 625.113 | -1.197 | 625.09  | -0.54  | 625.271 | -0.679 |
| 0.55   | 623.564 | -2.596 | 625.119 | -1.191 | 625.09  | -0.54  | 625.278 | -0.672 |
| 0.5666 | 623.577 | -2.583 | 625.119 | -1.191 | 625.09  | -0.54  | 625.278 | -0.672 |
| 0.5833 | 623.59  | -2.57  | 625.119 | -1.191 | 625.09  | -0.54  | 625.278 | -0.672 |
| 0.6    | 623.609 | -2.551 | 625.119 | -1.191 | 625.09  | -0.54  | 625.278 | -0.672 |
| 0.6166 | 623.628 | -2.532 | 625.119 | -1.191 | 625.09  | -0.54  | 625.278 | -0.672 |
| 0.6333 | 623.647 | -2.513 | 625.126 | -1.184 | 625.09  | -0.54  | 625.278 | -0.672 |
| 0.65   | 623.665 | -2.495 | 625.126 | -1.184 | 625.09  | -0.54  | 625.278 | -0.672 |
| 0.6666 | 623.678 | -2.482 | 625.132 | -1.178 | 625.097 | -0.533 | 625.278 | -0.672 |
| 0.6833 | 623.691 | -2.469 | 625.132 | -1.178 | 625.097 | -0.533 | 625.284 | -0.666 |
| 0.7    | 623.716 | -2.444 | 625.132 | -1.178 | 625.097 | -0.533 | 625.284 | -0.666 |
| 0.7166 | 623.729 | -2.431 | 625.132 | -1.178 | 625.097 | -0.533 | 625.284 | -0.666 |
| 0.7333 | 623.748 | -2.412 | 625.139 | -1.171 | 625.097 | -0.533 | 625.284 | -0.666 |
| 0.75   | 623.76  | -2.4   | 625.139 | -1.171 | 625.097 | -0.533 | 625.29  | -0.66  |
| 0.7666 | 623.779 | -2.381 | 625.139 | -1.171 | 625.103 | -0.527 | 625.29  | -0.66  |
| 0.7833 | 623.798 | -2.362 | 625.145 | -1.165 | 625.103 | -0.527 | 625.29  | -0.66  |
| 0.8    | 623.817 | -2.343 | 625.145 | -1.165 | 625.097 | -0.533 | 625.29  | -0.66  |
| 0.8166 | 623.83  | -2.33  | 625.145 | -1.165 | 625.103 | -0.527 | 625.29  | -0.66  |
| 0.8333 | 623.849 | -2.311 | 625.145 | -1.165 | 625.103 | -0.527 | 625.29  | -0.66  |
| 0.85   | 623.867 | -2.293 | 625.151 | -1.159 | 625.103 | -0.527 | 625.29  | -0.66  |
| 0.8666 | 623.886 | -2.274 | 625.151 | -1.159 | 625.103 | -0.527 | 625.297 | -0.653 |
| 0.8833 | 623.905 | -2.255 | 625.151 | -1.159 | 625.103 | -0.527 | 625.297 | -0.653 |
| 0.9    | 623.918 | -2.242 | 625.158 | -1.152 | 625.109 | -0.521 | 625.297 | -0.653 |
| 0.9166 | 623.937 | -2.223 | 625.158 | -1.152 | 625.103 | -0.527 | 625.297 | -0.653 |
| 0.9333 | 623.956 | -2.204 | 625.158 | -1.152 | 625.103 | -0.527 | 625.297 | -0.653 |
| 0.95   | 623.975 | -2.185 | 625.158 | -1.152 | 625.109 | -0.521 | 625.303 | -0.647 |
| 0.9666 | 624     | -2.16  | 625.164 | -1.146 | 625.109 | -0.521 | 625.303 | -0.647 |
| 0.9833 | 624.019 | -2.141 | 625.164 | -1.146 | 625.109 | -0.521 | 625.297 | -0.653 |
| 1      | 624.044 | -2.116 | 625.171 | -1.139 | 625.109 | -0.521 | 625.297 | -0.653 |
| 1.2    | 624.461 | -1.699 | 625.196 | -1.114 | 625.122 | -0.508 | 625.316 | -0.634 |
| 1.4    | 625.073 | -1.087 | 625.247 | -1.063 | 625.141 | -0.489 | 625.347 | -0.603 |
| 1.6    | 625.288 | -0.872 | 625.305 | -1.005 | 625.16  | -0.47  | 625.373 | -0.577 |
| 1.8    | 625.389 | -0.771 | 625.356 | -0.954 | 625.186 | -0.444 | 625.392 | -0.558 |
| 2      | 625.446 | -0.714 | 625.382 | -0.928 | 625.198 | -0.432 | 625.411 | -0.539 |
| 2.2    | 625.484 | -0.676 | 625.407 | -0.903 | 625.211 | -0.419 | 625.43  | -0.52  |
| 2.4    | 625.509 | -0.651 | 625.427 | -0.883 | 625.217 | -0.413 | 625.443 | -0.507 |
| 2.6    | 625.528 | -0.632 | 625.439 | -0.871 | 625.23  | -0.4   | 625.455 | -0.495 |
| 2.8    | 625.553 | -0.607 | 625.446 | -0.864 | 625.236 | -0.394 | 625.468 | -0.482 |
| 3      | 625.572 | -0.588 | 625.459 | -0.851 | 625.243 | -0.387 | 625.474 | -0.476 |
| 3.2    | 625.585 | -0.575 | 625.465 | -0.845 | 625.255 | -0.375 | 625.481 | -0.469 |
| 3.4    | 625.604 | -0.556 | 625.471 | -0.839 | 625.262 | -0.368 | 625.493 | -0.457 |

|     |         | RW-2   | MW-3    | 14S    | 14I     | DC-P3  |         | ATM    | MW-2R   | MW-6R  |
|-----|---------|--------|---------|--------|---------|--------|---------|--------|---------|--------|
| 3.6 | 625.616 | -0.544 | 625.478 | -0.832 | 625.268 | -0.362 | 625.5   | -0.45  | 624.583 | 0      |
| 3.8 | 625.623 | -0.537 | 625.478 | -0.832 | 625.274 | -0.356 | 625.506 | -0.444 | 624.583 | 0      |
| 4   | 625.635 | -0.525 | 625.484 | -0.826 | 625.281 | -0.349 | 625.512 | -0.438 | 624.583 | 0      |
| 4.2 | 625.648 | -0.512 | 625.491 | -0.819 | 625.281 | -0.349 | 625.525 | -0.425 | 624.583 | 0      |
| 4.4 | 625.654 | -0.506 | 625.497 | -0.813 | 625.287 | -0.343 | 625.525 | -0.425 | 624.583 | 0      |
| 4.6 | 625.667 | -0.493 | 625.503 | -0.807 | 625.293 | -0.337 | 625.531 | -0.419 | 624.583 | 0      |
| 4.8 | 625.673 | -0.487 | 625.51  | -0.8   | 625.3   | -0.33  | 625.544 | -0.406 | 624.583 | 0      |
| 5   | 625.68  | -0.48  | 625.516 | -0.794 | 625.306 | -0.324 | 625.544 | -0.406 | 624.583 | 0      |
| 5.2 | 625.692 | -0.488 | 625.523 | -0.787 | 625.312 | -0.318 | 625.55  | -0.4   | 624.583 | 0      |
| 5.4 | 625.698 | -0.482 | 625.523 | -0.787 | 625.312 | -0.318 | 625.557 | -0.393 | 624.583 | 0      |
| 5.6 | 625.698 | -0.482 | 625.529 | -0.781 | 625.312 | -0.318 | 625.563 | -0.387 | 624.583 | 0      |
| 5.8 | 625.705 | -0.455 | 625.529 | -0.781 | 625.319 | -0.311 | 625.563 | -0.387 | 624.583 | 0      |
| 6   | 625.711 | -0.449 | 625.535 | -0.775 | 625.325 | -0.305 | 625.569 | -0.381 | 624.583 | 0      |
| 6.2 | 625.717 | -0.443 | 625.542 | -0.768 | 625.325 | -0.305 | 625.569 | -0.381 | 624.583 | 0      |
| 6.4 | 625.724 | -0.436 | 625.542 | -0.768 | 625.325 | -0.305 | 625.576 | -0.374 | 624.583 | 0      |
| 6.6 | 625.73  | -0.43  | 625.554 | -0.756 | 625.338 | -0.292 | 625.582 | -0.368 | 624.583 | 0      |
| 6.8 | 625.736 | -0.424 | 625.554 | -0.756 | 625.338 | -0.292 | 625.588 | -0.362 | 624.583 | 0      |
| 7   | 625.743 | -0.417 | 625.561 | -0.749 | 625.338 | -0.292 | 625.588 | -0.362 | 624.583 | 0      |
| 7.2 | 625.743 | -0.417 | 625.561 | -0.749 | 625.338 | -0.292 | 625.588 | -0.362 | 624.583 | 0      |
| 7.4 | 625.749 | -0.411 | 625.567 | -0.743 | 625.344 | -0.286 | 625.595 | -0.355 | 624.583 | 0      |
| 7.6 | 625.749 | -0.411 | 625.574 | -0.736 | 625.344 | -0.286 | 625.601 | -0.349 | 624.583 | 0      |
| 7.8 | 625.755 | -0.405 | 625.574 | -0.736 | 625.35  | -0.28  | 625.601 | -0.349 | 624.583 | 0      |
| 8   | 625.762 | -0.398 | 625.58  | -0.73  | 625.35  | -0.28  | 625.607 | -0.343 | 624.583 | 0      |
| 8.2 | 625.768 | -0.392 | 625.586 | -0.724 | 625.357 | -0.273 | 625.607 | -0.343 | 624.583 | 0      |
| 8.4 | 625.768 | -0.392 | 625.593 | -0.717 | 625.357 | -0.273 | 625.614 | -0.336 | 624.583 | 0      |
| 8.6 | 625.774 | -0.386 | 625.593 | -0.717 | 625.363 | -0.267 | 625.614 | -0.336 | 624.583 | 0      |
| 8.8 | 625.781 | -0.379 | 625.599 | -0.711 | 625.363 | -0.267 | 625.62  | -0.33  | 624.583 | 0      |
| 9   | 625.781 | -0.379 | 625.606 | -0.704 | 625.363 | -0.267 | 625.62  | -0.33  | 624.583 | 0      |
| 9.2 | 625.787 | -0.373 | 625.612 | -0.698 | 625.369 | -0.261 | 625.626 | -0.324 | 624.583 | 0      |
| 9.4 | 625.787 | -0.373 | 625.612 | -0.698 | 625.369 | -0.261 | 625.626 | -0.324 | 624.583 | 0      |
| 9.6 | 625.793 | -0.367 | 625.618 | -0.692 | 625.369 | -0.261 | 625.633 | -0.317 | 624.577 | -0.006 |
| 9.8 | 625.8   | -0.36  | 625.618 | -0.692 | 625.369 | -0.261 | 625.639 | -0.311 | 624.577 | -0.006 |
| 10  | 625.8   | -0.36  | 625.625 | -0.685 | 625.369 | -0.261 | 625.639 | -0.311 | 624.577 | -0.006 |
| 12  | 625.825 | -0.335 | 625.67  | -0.64  | 625.389 | -0.241 | 625.664 | -0.286 | 624.577 | -0.006 |
| 14  | 625.844 | -0.316 | 625.727 | -0.583 | 625.401 | -0.229 | 625.677 | -0.273 | 624.577 | -0.006 |
| 16  | 625.863 | -0.297 | 625.804 | -0.506 | 625.414 | -0.216 | 625.702 | -0.248 | 624.577 | -0.006 |
| 18  | 625.882 | -0.278 | 625.849 | -0.461 | 625.427 | -0.203 | 625.709 | -0.241 | 624.577 | -0.006 |
| 20  | 625.894 | -0.266 | 625.906 | -0.404 | 625.433 | -0.197 | 625.715 | -0.235 | 624.571 | -0.012 |
| 22  | 625.907 | -0.253 | 625.938 | -0.372 | 625.439 | -0.191 | 625.728 | -0.222 | 624.571 | -0.012 |
| 24  | 625.92  | -0.24  | 625.964 | -0.346 | 625.458 | -0.172 | 625.734 | -0.216 | 624.583 | 0      |
| 26  | 625.932 | -0.228 | 626.002 | -0.308 | 625.465 | -0.165 | 625.74  | -0.21  | 624.583 | 0      |
| 28  | 625.938 | -0.222 | 626.022 | -0.288 | 625.465 | -0.165 | 625.747 | -0.203 | 624.583 | 0      |
| 30  | 625.945 | -0.215 | 626.041 | -0.269 | 625.471 | -0.159 | 625.753 | -0.197 | 624.583 | 0      |
| 32  | 625.945 | -0.215 | 626.047 | -0.263 | 625.477 | -0.153 | 625.759 | -0.191 | 624.583 | 0      |
| 34  | 625.957 | -0.203 | 626.054 | -0.256 | 625.477 | -0.153 | 625.766 | -0.184 | 624.577 | -0.006 |
| 36  | 625.964 | -0.196 | 626.06  | -0.25  | 625.484 | -0.146 | 625.778 | -0.172 | 624.577 | -0.006 |
| 38  | 625.97  | -0.19  | 626.066 | -0.244 | 625.484 | -0.146 | 625.778 | -0.172 | 624.571 | -0.012 |

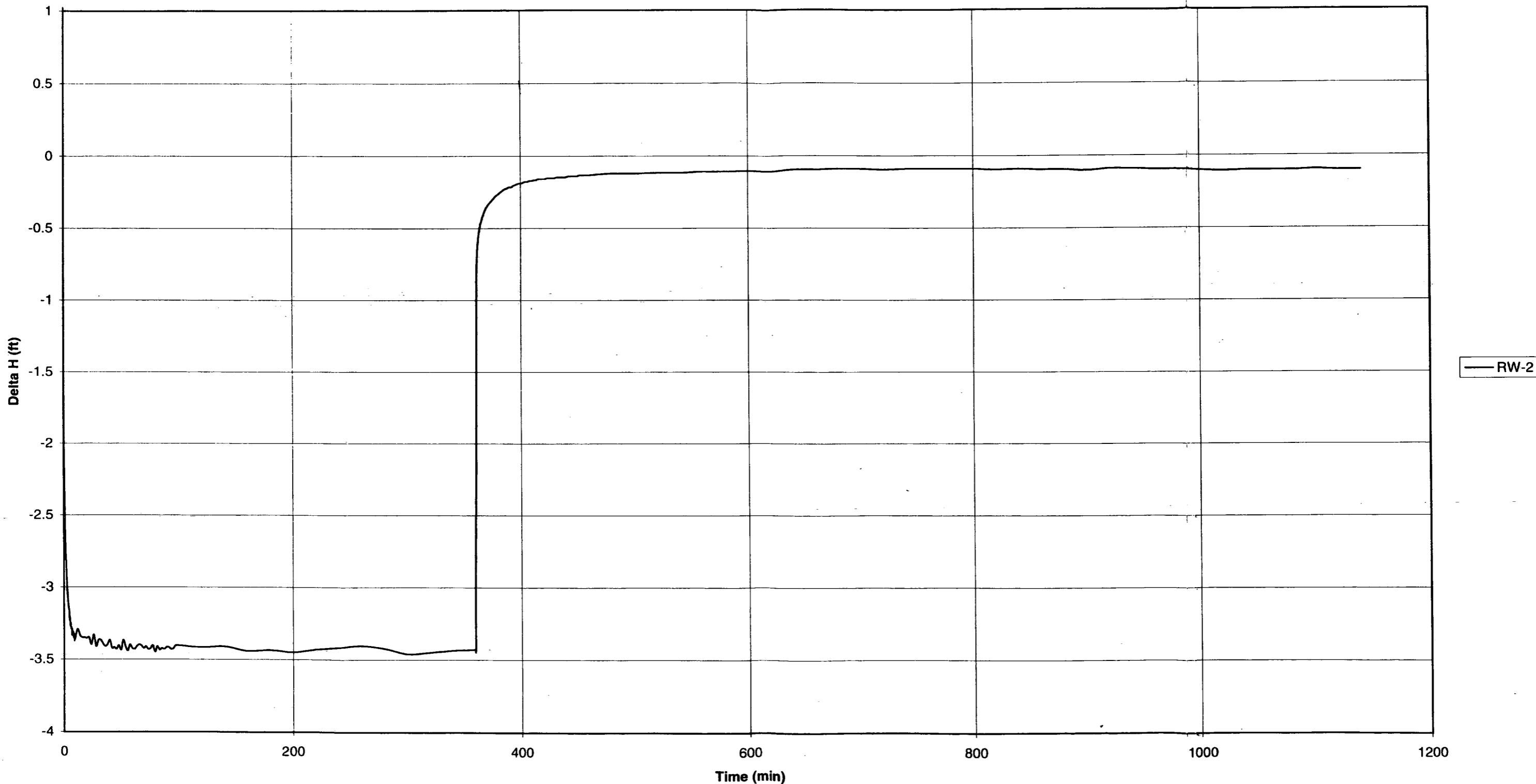
|     |         | RW-2   | MW-3    | 14S    |         | 14I    |         | DC-P3  |         | ATM    |        | MW-2R  |        | MW-6R  |        |        |
|-----|---------|--------|---------|--------|---------|--------|---------|--------|---------|--------|--------|--------|--------|--------|--------|--------|
| 40  | 625.97  | -0.19  | 626.066 | -0.244 | 625.49  | -0.14  | 625.785 | -0.165 | 624.571 | -0.012 | 14.435 | 0.003  | 99.835 | -0.165 | 99.777 | -0.223 |
| 42  | 625.976 | -0.184 | 626.079 | -0.231 | 625.49  | -0.14  | 625.785 | -0.165 | 624.577 | -0.006 | 14.432 | 0      | 99.841 | -0.159 | 99.777 | -0.223 |
| 44  | 625.983 | -0.177 | 626.086 | -0.224 | 625.496 | -0.134 | 625.797 | -0.153 | 624.571 | -0.012 | 14.431 | -0.001 | 99.848 | -0.152 | 99.777 | -0.223 |
| 46  | 625.983 | -0.177 | 626.079 | -0.231 | 625.496 | -0.134 | 625.797 | -0.153 | 624.577 | -0.006 | 14.431 | -0.001 | 99.848 | -0.152 | 99.777 | -0.223 |
| 48  | 625.989 | -0.171 | 626.086 | -0.224 | 625.496 | -0.134 | 625.797 | -0.153 | 624.571 | -0.012 | 14.431 | -0.001 | 99.854 | -0.146 | 99.777 | -0.223 |
| 50  | 625.989 | -0.171 | 626.092 | -0.218 | 625.503 | -0.127 | 625.797 | -0.153 | 624.571 | -0.012 | 14.432 | 0      | 99.854 | -0.146 | 99.784 | -0.216 |
| 52  | 625.995 | -0.165 | 626.098 | -0.212 | 625.509 | -0.121 | 625.804 | -0.146 | 624.571 | -0.012 | 14.433 | 0.001  | 99.854 | -0.146 | 99.784 | -0.216 |
| 54  | 625.995 | -0.165 | 626.105 | -0.205 | 625.509 | -0.121 | 625.804 | -0.146 | 624.571 | -0.012 | 14.432 | 0      | 99.86  | -0.14  | 99.777 | -0.223 |
| 56  | 626.002 | -0.158 | 626.105 | -0.205 | 625.509 | -0.121 | 625.804 | -0.146 | 624.577 | -0.006 | 14.433 | 0.001  | 99.86  | -0.14  | 99.784 | -0.216 |
| 58  | 626.002 | -0.158 | 626.111 | -0.198 | 625.509 | -0.121 | 625.804 | -0.146 | 624.577 | -0.006 | 14.435 | 0.003  | 99.86  | -0.14  | 99.784 | -0.216 |
| 60  | 626.002 | -0.158 | 626.111 | -0.198 | 625.509 | -0.121 | 625.81  | -0.14  | 624.571 | -0.012 | 14.434 | 0.002  | 99.86  | -0.14  | 99.777 | -0.223 |
| 62  | 626.002 | -0.158 | 626.111 | -0.198 | 625.509 | -0.121 | 625.804 | -0.146 | 624.571 | -0.012 | 14.435 | 0.003  | 99.86  | -0.14  | 99.777 | -0.223 |
| 64  | 626.008 | -0.152 | 626.118 | -0.192 | 625.515 | -0.115 | 625.81  | -0.14  | 624.571 | -0.012 | 14.435 | 0.003  | 99.867 | -0.133 | 99.784 | -0.216 |
| 66  | 626.008 | -0.152 | 626.118 | -0.192 | 625.515 | -0.115 | 625.81  | -0.14  | 624.577 | -0.006 | 14.438 | 0.006  | 99.867 | -0.133 | 99.771 | -0.229 |
| 68  | 626.008 | -0.152 | 626.118 | -0.192 | 625.515 | -0.115 | 625.81  | -0.14  | 624.577 | -0.006 | 14.438 | 0.006  | 99.867 | -0.133 | 99.771 | -0.229 |
| 70  | 626.008 | -0.152 | 626.124 | -0.186 | 625.515 | -0.115 | 625.81  | -0.14  | 624.571 | -0.012 | 14.438 | 0.006  | 99.873 | -0.127 | 99.771 | -0.229 |
| 72  | 626.014 | -0.146 | 626.124 | -0.186 | 625.522 | -0.108 | 625.81  | -0.14  | 624.571 | -0.012 | 14.439 | 0.007  | 99.873 | -0.127 | 99.777 | -0.223 |
| 74  | 626.014 | -0.146 | 626.124 | -0.186 | 625.522 | -0.108 | 625.816 | -0.134 | 624.571 | -0.012 | 14.439 | 0.007  | 99.873 | -0.127 | 99.771 | -0.229 |
| 76  | 626.014 | -0.146 | 626.13  | -0.18  | 625.515 | -0.115 | 625.816 | -0.134 | 624.571 | -0.012 | 14.439 | 0.007  | 99.879 | -0.121 | 99.771 | -0.229 |
| 78  | 626.014 | -0.146 | 626.13  | -0.18  | 625.522 | -0.108 | 625.823 | -0.127 | 624.571 | -0.012 | 14.439 | 0.007  | 99.879 | -0.121 | 99.771 | -0.229 |
| 80  | 626.014 | -0.146 | 626.137 | -0.173 | 625.522 | -0.108 | 625.816 | -0.134 | 624.577 | -0.006 | 14.438 | 0.006  | 99.879 | -0.121 | 99.777 | -0.223 |
| 82  | 626.021 | -0.139 | 626.137 | -0.173 | 625.528 | -0.102 | 625.823 | -0.127 | 624.571 | -0.012 | 14.438 | 0.006  | 99.879 | -0.121 | 99.765 | -0.235 |
| 84  | 626.021 | -0.139 | 626.137 | -0.173 | 625.528 | -0.102 | 625.816 | -0.134 | 624.571 | -0.012 | 14.439 | 0.007  | 99.879 | -0.121 | 99.771 | -0.229 |
| 86  | 626.021 | -0.139 | 626.143 | -0.167 | 625.522 | -0.108 | 625.823 | -0.127 | 624.571 | -0.012 | 14.439 | 0.007  | 99.886 | -0.114 | 99.765 | -0.235 |
| 88  | 626.021 | -0.139 | 626.143 | -0.167 | 625.528 | -0.102 | 625.823 | -0.127 | 624.571 | -0.012 | 14.44  | 0.008  | 99.886 | -0.114 | 99.765 | -0.235 |
| 90  | 626.021 | -0.139 | 626.143 | -0.167 | 625.522 | -0.108 | 625.823 | -0.127 | 624.571 | -0.012 | 14.44  | 0.008  | 99.886 | -0.114 | 99.771 | -0.229 |
| 92  | 626.027 | -0.133 | 626.143 | -0.167 | 625.522 | -0.108 | 625.823 | -0.127 | 624.571 | -0.012 | 14.439 | 0.007  | 99.886 | -0.114 | 99.765 | -0.235 |
| 94  | 626.027 | -0.133 | 626.143 | -0.187 | 625.528 | -0.102 | 625.823 | -0.127 | 624.571 | -0.012 | 14.44  | 0.008  | 99.886 | -0.114 | 99.765 | -0.235 |
| 96  | 626.027 | -0.133 | 626.143 | -0.167 | 625.528 | -0.102 | 625.823 | -0.127 | 624.571 | -0.012 | 14.44  | 0.008  | 99.886 | -0.114 | 99.758 | -0.242 |
| 98  | 626.027 | -0.133 | 626.15  | -0.16  | 625.528 | -0.102 | 625.829 | -0.121 | 624.571 | -0.012 | 14.441 | 0.009  | 99.886 | -0.114 | 99.752 | -0.248 |
| 100 | 626.027 | -0.133 | 626.15  | -0.16  | 625.528 | -0.102 | 625.823 | -0.127 | 624.571 | -0.012 | 14.442 | 0.01   | 99.886 | -0.114 | 99.758 | -0.242 |
| 120 | 626.04  | -0.12  | 626.162 | -0.148 | 625.534 | -0.096 | 625.829 | -0.121 | 624.571 | -0.012 | 14.444 | 0.012  | 99.892 | -0.108 | 99.758 | -0.242 |
| 140 | 626.04  | -0.12  | 626.175 | -0.135 | 625.541 | -0.089 | 625.835 | -0.115 | 624.571 | -0.012 | 14.444 | 0.012  | 99.905 | -0.095 | 99.758 | -0.242 |
| 160 | 626.046 | -0.114 | 626.182 | -0.128 | 625.547 | -0.083 | 625.842 | -0.108 | 624.571 | -0.012 | 14.448 | 0.016  | 99.905 | -0.095 | 99.746 | -0.254 |
| 180 | 626.046 | -0.114 | 626.182 | -0.128 | 625.547 | -0.083 | 625.842 | -0.108 | 624.571 | -0.012 | 14.452 | 0.02   | 99.905 | -0.095 | 99.739 | -0.261 |
| 200 | 626.052 | -0.108 | 626.184 | -0.116 | 625.547 | -0.083 | 625.842 | -0.108 | 624.571 | -0.012 | 14.453 | 0.021  | 99.911 | -0.089 | 99.739 | -0.261 |
| 220 | 626.052 | -0.108 | 626.201 | -0.109 | 625.547 | -0.083 | 625.848 | -0.102 | 624.571 | -0.012 | 14.459 | 0.027  | 99.911 | -0.089 | 99.727 | -0.273 |
| 240 | 626.058 | -0.102 | 626.201 | -0.109 | 625.547 | -0.083 | 625.842 | -0.108 | 624.571 | -0.012 | 14.459 | 0.027  | 99.911 | -0.089 | 99.72  | -0.28  |
| 260 | 626.052 | -0.108 | 626.194 | -0.116 | 625.547 | -0.083 | 625.842 | -0.108 | 624.571 | -0.012 | 14.466 | 0.034  | 99.905 | -0.095 | 99.714 | -0.286 |
| 280 | 626.065 | -0.095 | 626.214 | -0.096 | 625.56  | -0.07  | 625.848 | -0.102 | 624.571 | -0.012 | 14.456 | 0.024  | 99.917 | -0.083 | 99.714 | -0.286 |
| 300 | 626.065 | -0.095 | 626.214 | -0.096 | 625.56  | -0.07  | 625.854 | -0.096 | 624.571 | -0.012 | 14.455 | 0.023  | 99.924 | -0.076 | 99.72  | -0.28  |
| 320 | 626.071 | -0.089 | 626.214 | -0.096 | 625.56  | -0.07  | 625.854 | -0.096 | 624.571 | -0.012 | 14.454 | 0.022  | 99.924 | -0.076 | 99.708 | -0.292 |
| 340 | 626.071 | -0.089 | 626.214 | -0.096 | 625.56  | -0.07  | 625.854 | -0.096 | 624.571 | -0.012 | 14.453 | 0.021  | 99.924 | -0.076 | 99.701 | -0.299 |
| 360 | 626.065 | -0.095 | 626.22  | -0.09  | 625.56  | -0.07  | 625.854 | -0.096 | 624.571 | -0.012 | 14.453 | 0.021  | 99.924 | -0.076 | 99.695 | -0.305 |
| 380 | 626.071 | -0.089 | 626.22  | -0.09  | 625.56  | -0.07  | 625.861 | -0.089 | 624.577 | -0.008 | 14.451 | 0.019  | 99.924 | -0.076 | 99.695 | -0.305 |
| 400 | 626.071 | -0.089 | 626.22  | -0.09  | 625.56  | -0.07  | 625.861 | -0.089 | 624.577 | -0.008 | 14.452 | 0.02   | 99.924 | -0.076 | 99.695 | -0.305 |
| 420 | 626.071 | -0.089 | 626.22  | -0.09  | 625.56  | -0.07  | 625.861 | -0.089 | 624.577 | -0.008 | 14.451 | 0.019  | 99.924 | -0.076 | 99.689 | -0.311 |

|     |         | RW-2   | MW-3    | 14S    | 14I     |        | DC-P3   |        | ATM     |        | MW-2R  |       | MW-6R  |        |        |        |
|-----|---------|--------|---------|--------|---------|--------|---------|--------|---------|--------|--------|-------|--------|--------|--------|--------|
| 440 | 626.071 | -0.089 | 626.22  | -0.09  | 625.56  | -0.07  | 625.854 | -0.098 | 624.571 | -0.012 | 14.452 | 0.02  | 99.924 | -0.076 | 99.682 | -0.318 |
| 460 | 626.065 | -0.085 | 626.226 | -0.084 | 625.56  | -0.07  | 625.854 | -0.096 | 624.571 | -0.012 | 14.452 | 0.02  | 99.924 | -0.076 | 99.682 | -0.318 |
| 480 | 626.071 | -0.089 | 626.226 | -0.084 | 625.56  | -0.07  | 625.854 | -0.096 | 624.571 | -0.012 | 14.451 | 0.019 | 99.924 | -0.076 | 99.87  | -0.33  |
| 500 | 626.065 | -0.085 | 626.226 | -0.084 | 625.56  | -0.07  | 625.854 | -0.096 | 624.571 | -0.012 | 14.452 | 0.02  | 99.917 | -0.083 | 99.683 | -0.337 |
| 520 | 626.065 | -0.085 | 626.22  | -0.09  | 625.56  | -0.07  | 625.848 | -0.102 | 624.571 | -0.012 | 14.455 | 0.023 | 99.917 | -0.083 | 99.683 | -0.337 |
| 540 | 626.058 | -0.102 | 626.22  | -0.09  | 625.56  | -0.07  | 625.848 | -0.102 | 624.571 | -0.012 | 14.462 | 0.03  | 99.911 | -0.089 | 99.644 | -0.356 |
| 560 | 626.071 | -0.089 | 626.226 | -0.084 | 625.56  | -0.07  | 625.854 | -0.098 | 624.571 | -0.012 | 14.453 | 0.021 | 99.924 | -0.076 | 99.65  | -0.35  |
| 580 | 626.071 | -0.089 | 626.233 | -0.077 | 625.566 | -0.064 | 625.861 | -0.089 | 624.571 | -0.012 | 14.45  | 0.018 | 99.924 | -0.076 | 99.683 | -0.337 |
| 600 | 626.065 | -0.085 | 626.226 | -0.084 | 625.56  | -0.07  | 625.854 | -0.096 | 624.577 | -0.006 | 14.455 | 0.023 | 99.917 | -0.083 | 99.85  | -0.35  |
| 620 | 626.065 | -0.085 | 626.22  | -0.09  | 625.553 | -0.077 | 625.848 | -0.102 | 624.571 | -0.012 | 14.46  | 0.028 | 99.917 | -0.083 | 99.638 | -0.362 |
| 640 | 626.058 | -0.102 | 626.22  | -0.09  | 625.553 | -0.077 | 625.848 | -0.102 | 624.571 | -0.012 | 14.461 | 0.029 | 99.917 | -0.083 | 99.638 | -0.362 |
| 660 | 626.052 | -0.108 | 626.22  | -0.09  | 625.553 | -0.077 | 625.842 | -0.108 | 624.571 | -0.012 | 14.467 | 0.035 | 99.911 | -0.089 | 99.638 | -0.362 |
| 680 | 626.058 | -0.102 | 626.226 | -0.084 | 625.553 | -0.077 | 625.848 | -0.102 | 624.571 | -0.012 | 14.465 | 0.033 | 99.911 | -0.089 | 99.644 | -0.356 |
| 700 | 626.058 | -0.102 | 626.22  | -0.09  | 625.553 | -0.077 | 625.848 | -0.102 | 624.571 | -0.012 | 14.467 | 0.035 | 99.911 | -0.089 | 99.638 | -0.362 |
| 720 | 626.058 | -0.102 | 626.22  | -0.09  | 625.553 | -0.077 | 625.848 | -0.102 | 624.571 | -0.012 | 14.47  | 0.038 | 99.911 | -0.089 | 99.638 | -0.362 |
| 740 | 626.065 | -0.085 | 626.226 | -0.084 | 625.56  | -0.07  | 625.848 | -0.102 | 624.577 | -0.006 | 14.462 | 0.03  | 99.917 | -0.083 | 99.631 | -0.369 |
| 760 | 626.058 | -0.102 | 626.22  | -0.09  | 625.553 | -0.077 | 625.842 | -0.108 | 624.571 | -0.012 | 14.465 | 0.033 | 99.911 | -0.089 | 99.631 | -0.369 |
| 780 | 626.058 | -0.102 | 626.22  | -0.09  | 625.553 | -0.077 | 625.848 | -0.102 | 624.571 | -0.012 | 14.466 | 0.034 | 99.911 | -0.089 | 99.625 | -0.375 |

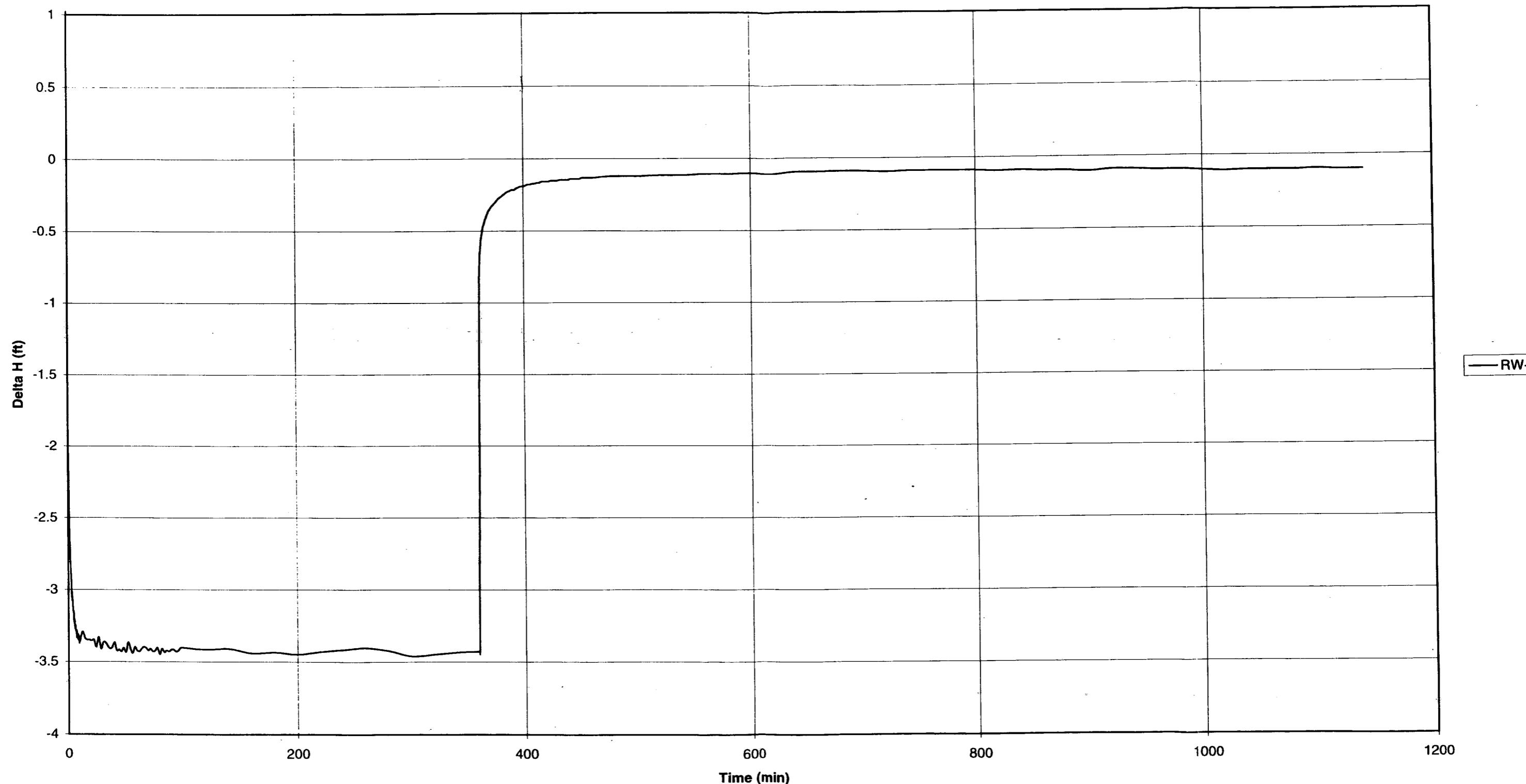
Drawdown in On-Site Monitoring Wells  
Pump Test 1; 150gpm and Recovery  
L.E. Carpenter Aquifer Test



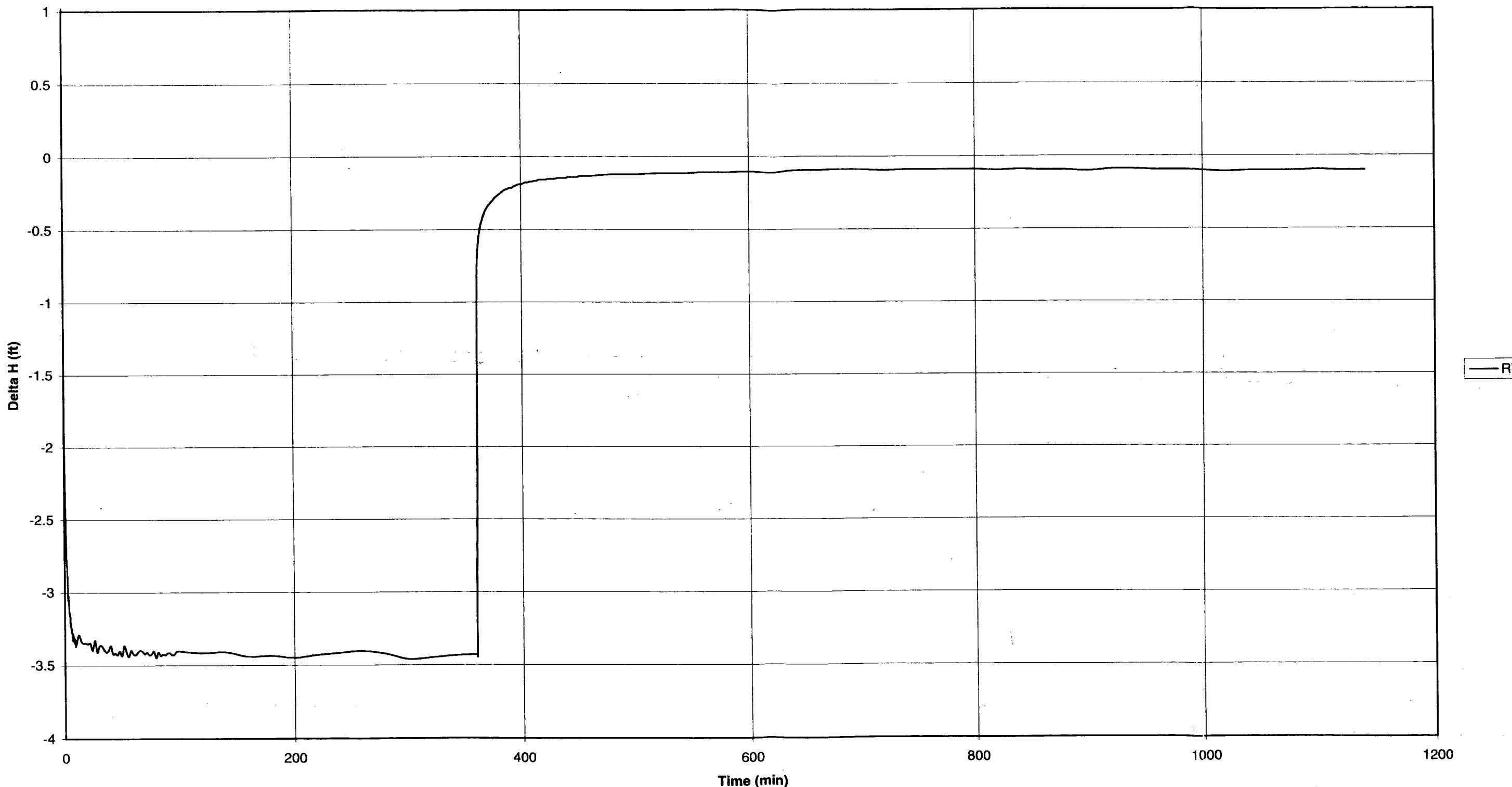
**Drawdown and Recovery in RW-2**  
**L.E. Carpenter Aquifer Test**



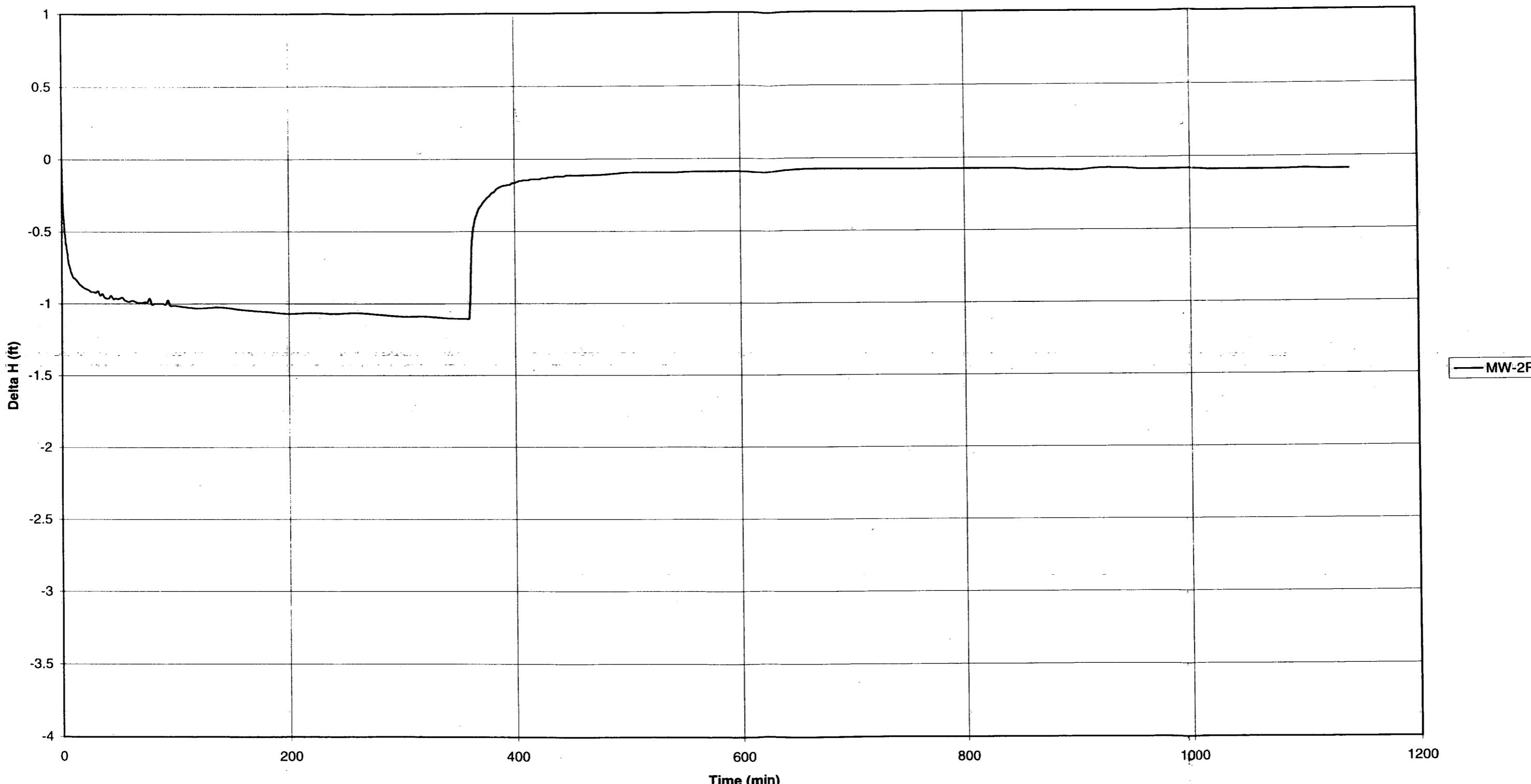
**Drawdown and Recovery in RW-2**  
**L.E. Carpenter Aquifer Test**



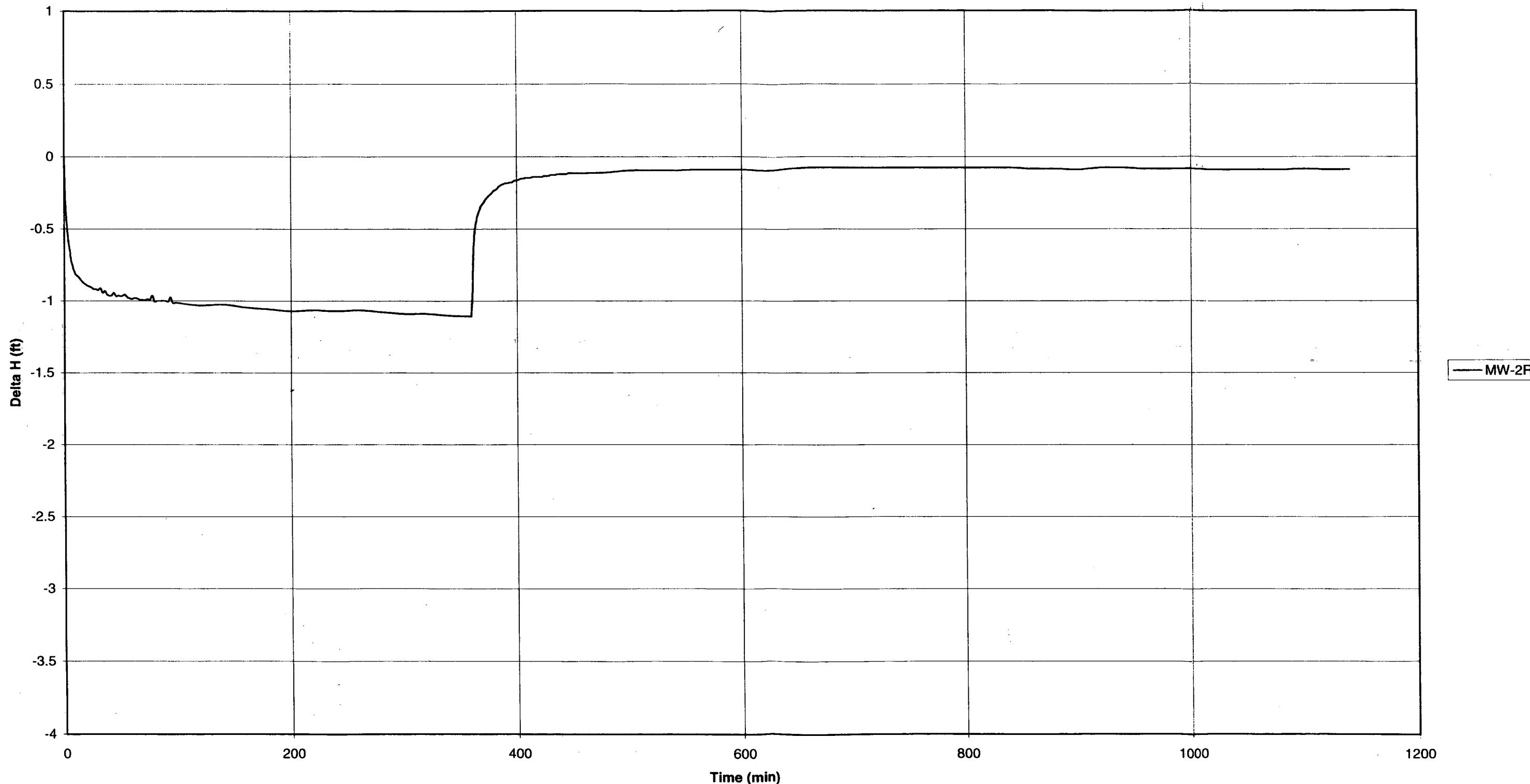
**Drawdown and Recovery in RW-2**  
**L.E. Carpenter Aquifer Test**



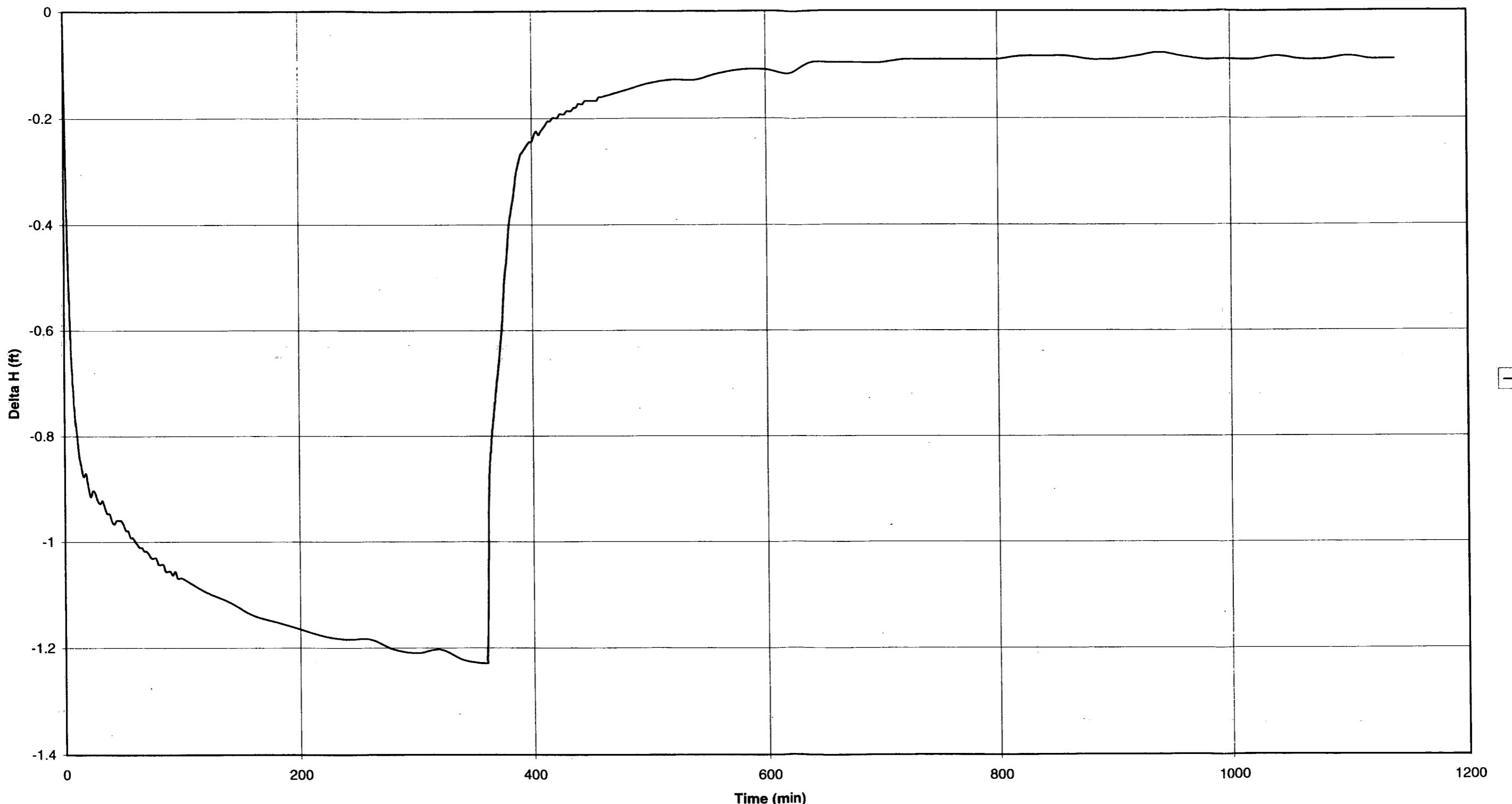
**Drawdown and Recovery in MW-2R**  
**L.E. Carpenter Aquifer Test**



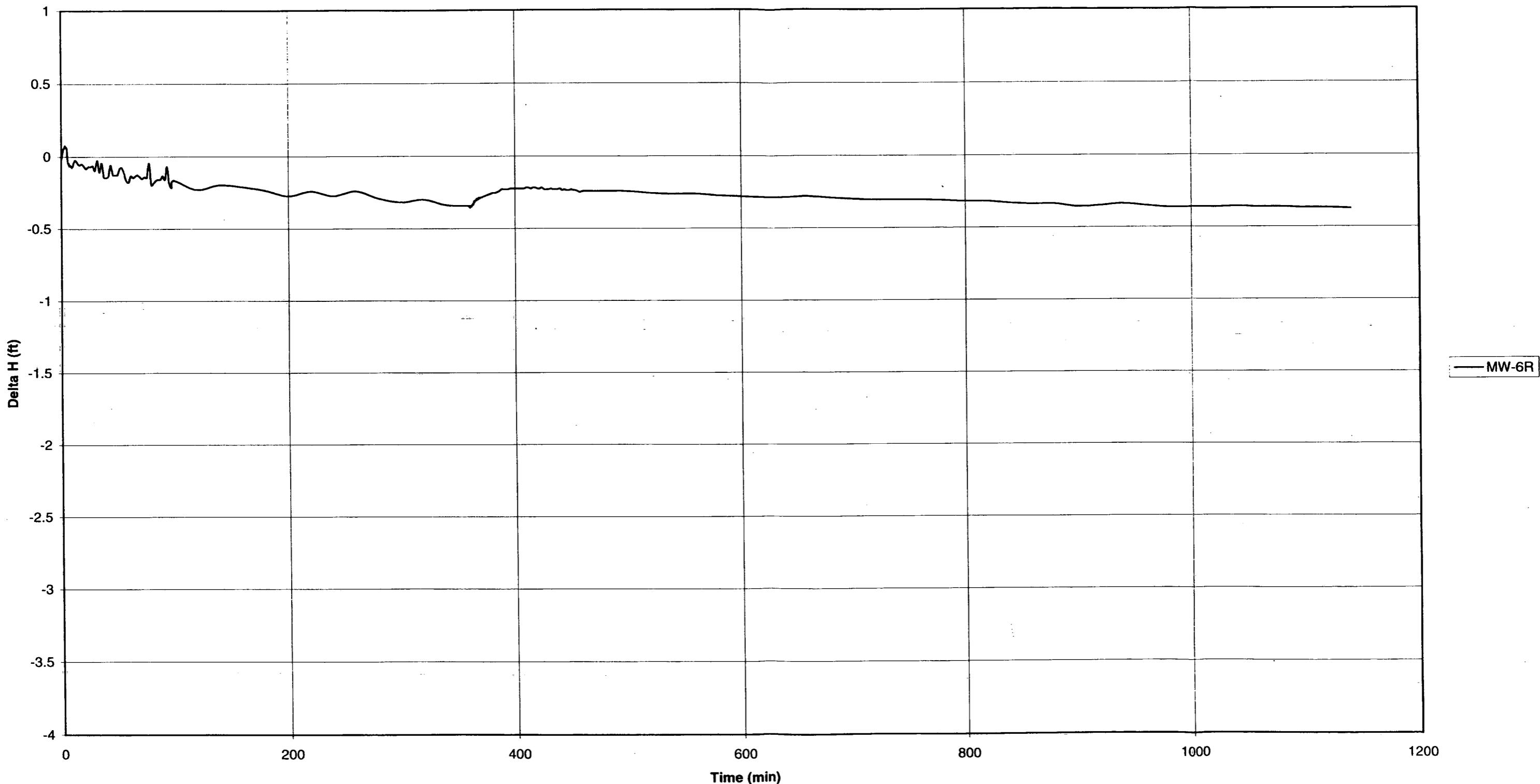
**Drawdown and Recovery in MW-2R**  
**L.E. Carpenter Aquifer Test**



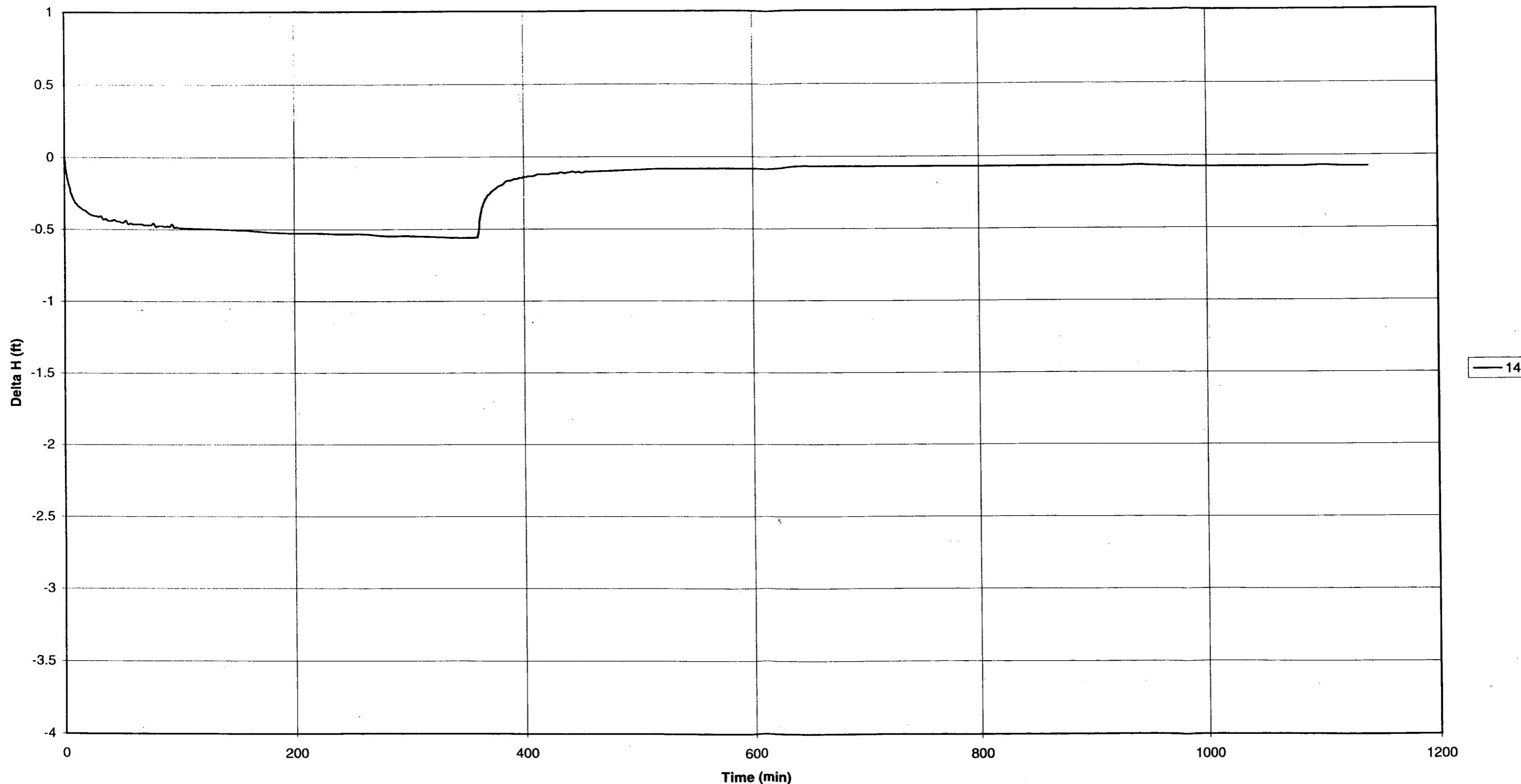
**Drawdown and Recovery in MW-3**  
**L.E. Carpenter Aquifer Test**



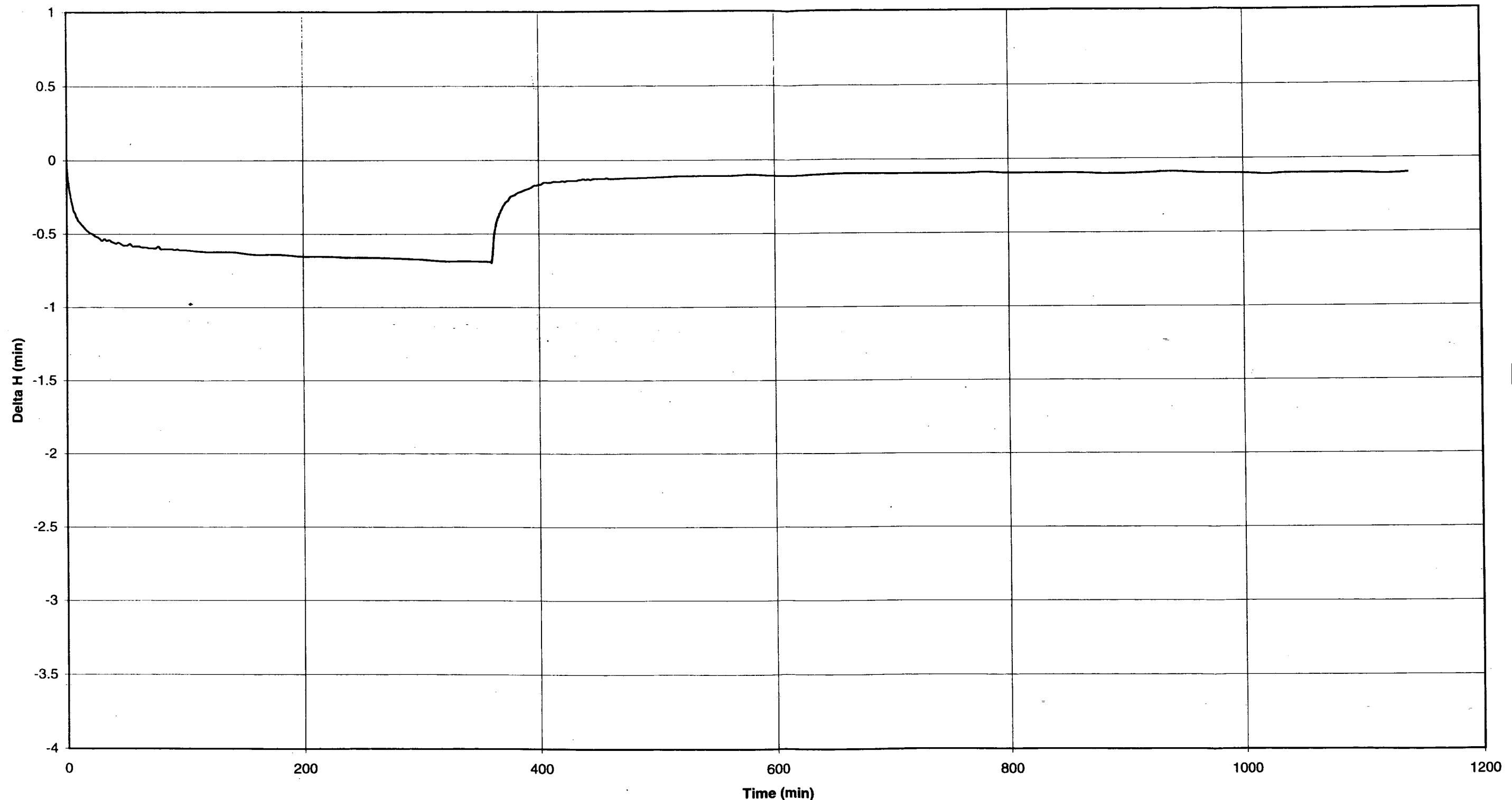
**Drawdown and Recovery in MW-6R**  
**L.E. Carpenter Aquifer Test**



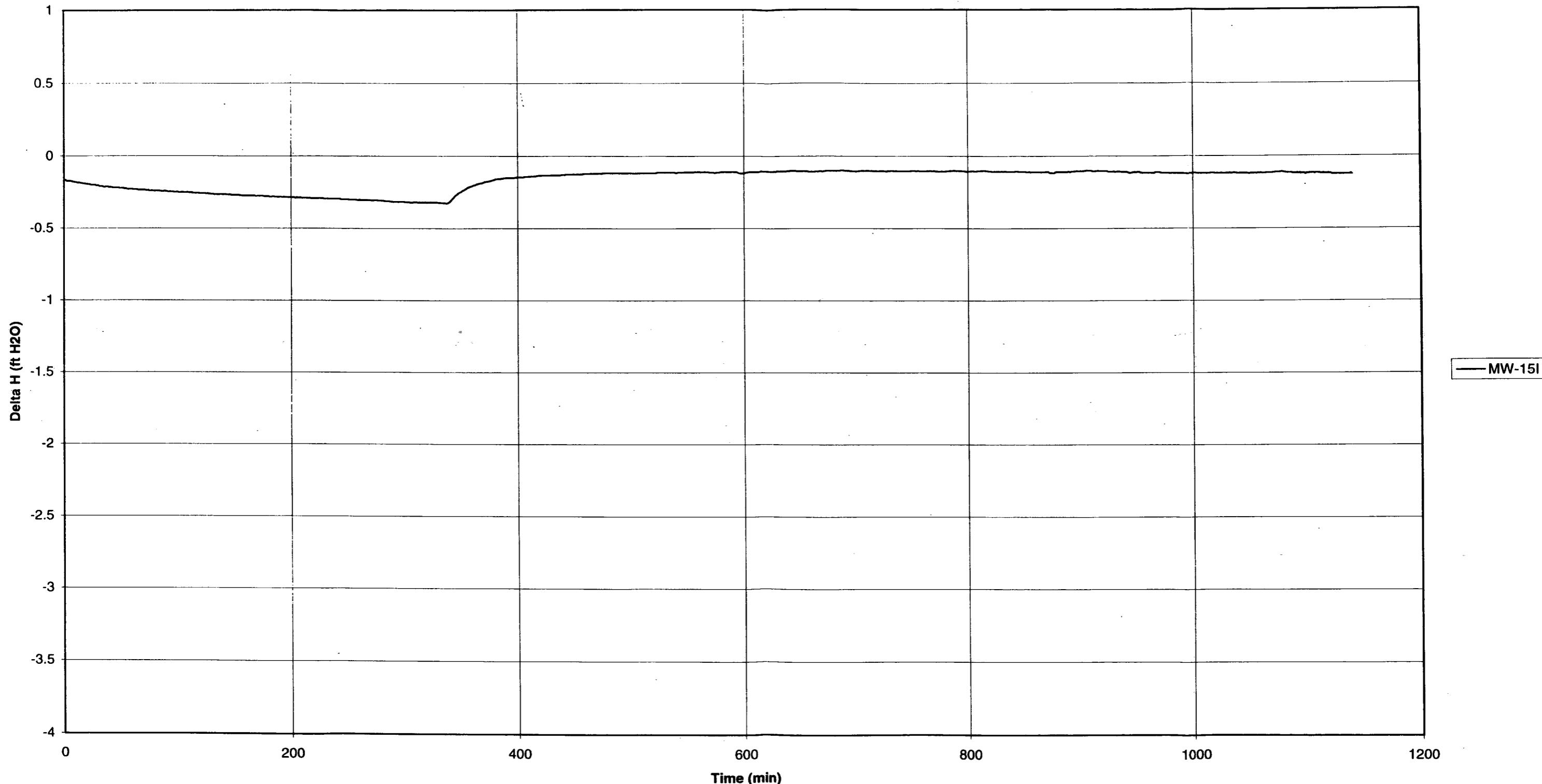
**Drawdown and Recovery in MW-14S**  
**L.E. Carpenter Aquifer Test**



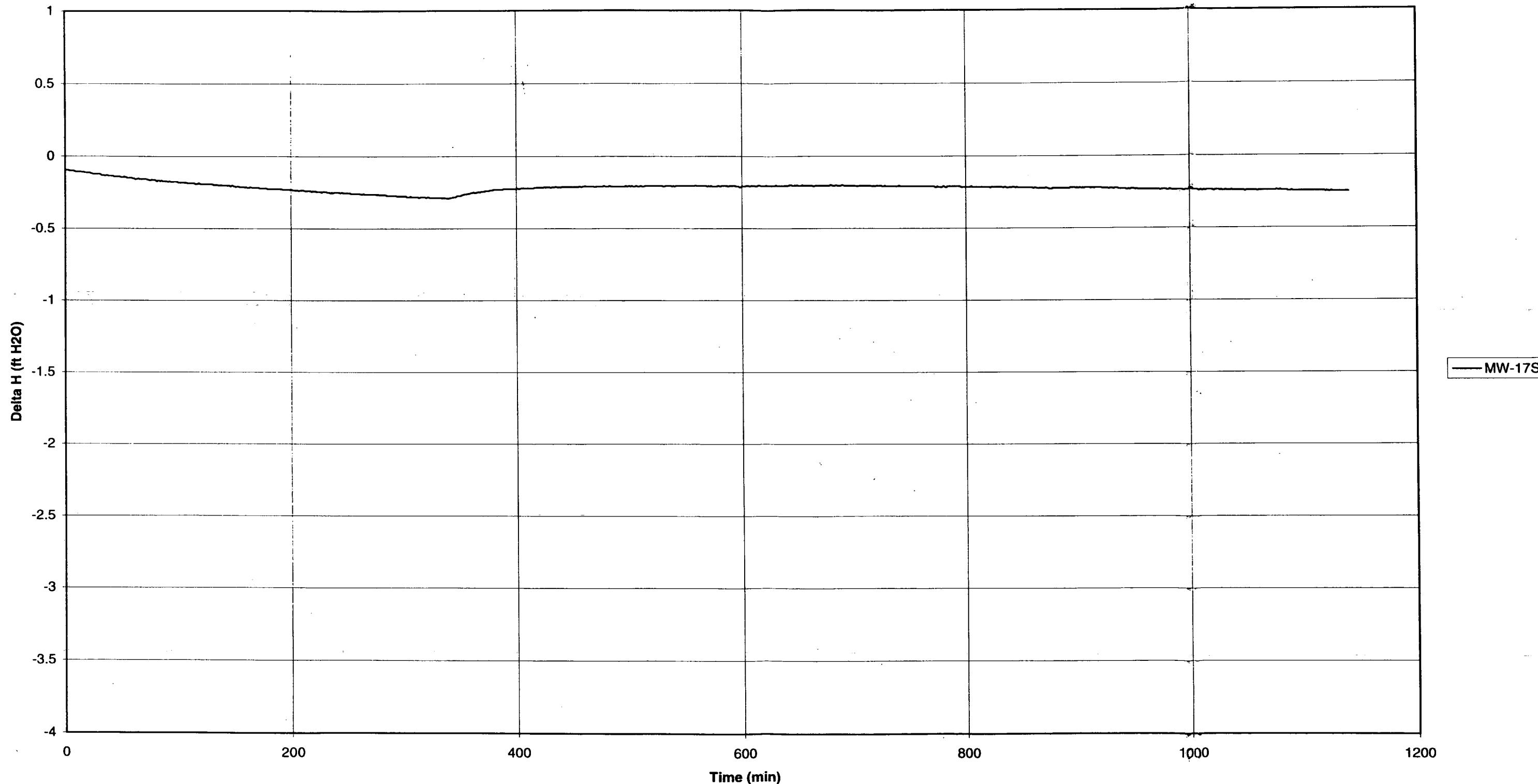
**Drawdown and Recovery in MW-14I**  
**L.E. Carpenter Aquifer Test**



**Water Levels in MW-15I During Pump Test**  
**L.E. Carpenter Aquifer Test**



**Water Levels in MW-17S During Pump Test**  
**L.E. Carpenter Aquifer Test**





**APPENDIX D**  
**TABLES/ANALYTICAL RESULTS OF GROUNDWATER SAMPLES**



TABLE 1  
SUMMARY OF GROUNDWATER SAMPLING DATA  
L.E. CARPENTER SITE  
WHARTON, NJ

| Sample ID No.             | GW-1    | GW-2    | Trip_Blank | NJDEP<br>GROUNDWATER<br>QUALITY<br>CRITERIA* |
|---------------------------|---------|---------|------------|----------------------------------------------|
| Laboratory Sample ID No:  | 55544   | 5545    | 54739-006  |                                              |
| Date:                     | 7/16/96 | 7/16/96 | 7/16/96    |                                              |
| Matrix:                   | water   | water   | water      |                                              |
| VOLATILE ORGANICS (ug/L)  | DF: 10  | DF: 5   | DF: 1      |                                              |
| Chloromethane             | 9.3 U   | 4.6 U   | 0.9 U      | 30                                           |
| Bromomethane              | 2.7 U   | 1.4 U   | 0.3 U      | 10                                           |
| Vinyl Chloride            | 3.9 U   | 2.0 U   | 0.4 U      | 5                                            |
| Chloroethane              | 10 U    | 5.2 U   | 1.0 U      | NLE                                          |
| Methylene Chloride        | 10 U    | 5.2 U   | 1.0 U      | 2                                            |
| Acetone                   | 50 U    | 25 U    | 5.0 U      | 700                                          |
| Carbon Disulfide          | 10 U    | 5.0 U   | 1.0 U      | NLE                                          |
| 1,1-Dichloroethene        | 5.5 U   | 2.8 U   | 0.6 U      | 2                                            |
| 1,1-Dichloroethane        | 3.1 U   | 1.6 U   | 0.3 U      | 70                                           |
| trans-1,2-Dichloroethene  | 3 U     | 1.5 U   | 0.3 U      | see notes                                    |
| cis-1,2-Dichloroethene    | 10 U    | 5 U     | 1.0 U      | see notes                                    |
| Chloroform                | 2.0 U   | 1.0 U   | 0.2 U      | 6                                            |
| 1,2-Dichloroethane        | 2.2 U   | 1.1 U   | 0.2 U      | 2                                            |
| 2-Butanone                | 50 U    | 25 U    | 5.0 U      | 300                                          |
| 1,1,1-Trichloroethane     | 2.0 U   | 1.0 U   | 0.2 U      | 30                                           |
| Carbon Tetrachloride      | 1.6 U   | 0.8 U   | 0.2 U      | 2                                            |
| Bromodichloromethane      | 1.9 U   | 0.9 U   | 0.2 U      | 1                                            |
| 1,2-Dichloropropane       | 4.6 U   | 2.3 U   | 0.5 U      | 1                                            |
| cis-1,3-Dichloropropene   | 3.3 U   | 1.6 U   | 0.3 U      | 5                                            |
| Trichloroethene           | 4.1 U   | 2.0 U   | 0.4 U      | 1                                            |
| Dibromochloromethane      | 2.3 U   | 1.2 U   | 0.2 U      | 10                                           |
| 1,1,2-Trichloroethane     | 4.3 U   | 2.2 U   | 0.4 U      | 3                                            |
| Benzene                   | 2.4 U   | 1.2 U   | 0.2 U      | 1                                            |
| Trans-1,3-Dichloropropene | 3.1 U   | 1.6 U   | 0.3 U      | 7                                            |
| Bromoform                 | 3.0 U   | 1.5 U   | 0.3 U      | 4                                            |
| 4-Methyl-2-Pentanone      | 50 U    | 25 U    | 5.0 U      | 400                                          |
| 2-Hexanone                | 50 U    | 25 U    | 5.0 U      | NLE                                          |
| Tetrachloroethene         | 1.0 U   | 0.5 U   | 0.1 U      | 1                                            |
| 1,1,2,2-Tetrachloroethane | 3.3 U   | 1.6 U   | 0.3 U      | 2                                            |
| Toluene                   | 1.8 U   | 0.9 U   | 0.2 U      | 1000                                         |
| Chlorobenzene             | 1.4 U   | 0.7 U   | 0.1 U      | 5                                            |
| Ethylbenzene              | 460     | 180     | 0.2 U      | 700                                          |
| Styrene                   | 10 U    | 5.0 U   | 1.0 U      | 100                                          |
| Xylenes (total)           | 1,400   | 630     | 1.0 U      | 40                                           |



**TABLE 1 (continued)**  
**SUMMARY OF GROUNDWATER SAMPLING DATA**  
**L.E. CARPENTER SITE**  
**WHARTON, NJ**

| Sample ID No.:<br>Laboratory Sample ID No:<br>Date:<br>Matrix: | GW-1<br>55544<br>7/16/96<br>water | GW-2<br>5545<br>7/16/96<br>water | Trip_Blank<br>54739-006<br>7/16/96<br>water | NJDEP<br>GROUNDWATER<br>QUALITY<br>CRITERIA* |
|----------------------------------------------------------------|-----------------------------------|----------------------------------|---------------------------------------------|----------------------------------------------|
| <b>SEMOVOLATILE ORGANICS (ug/L)</b>                            |                                   |                                  |                                             |                                              |
|                                                                | DF: 5                             | DF: 1                            |                                             |                                              |
| Phenol                                                         | 5.6 U                             | 1.2 U                            | NA                                          | 4000                                         |
| 2-Chlorophenol                                                 | 11 U                              | 2.4 U                            | NA                                          | 40                                           |
| 2-Methylphenol                                                 | 25 U                              | 5.6 U                            | NA                                          | NLE                                          |
| 4-Methylphenol                                                 | 25 U                              | 5.6 U                            | NA                                          | NLE                                          |
| 2-Nitrophenol                                                  | 15 U                              | 3.4 U                            | NA                                          | NLE                                          |
| 2,4-Dimethylphenol                                             | 14 U                              | 6.2                              | NA                                          | 100                                          |
| 2,4-Dichlorophenol                                             | 15 U                              | 3.3 U                            | NA                                          | 20                                           |
| 4-Chloro-3-methylphenol                                        | 14 U                              | 3.2 U                            | NA                                          | 20                                           |
| 2,4,6-Trichlorophenol                                          | 15 U                              | 3.4 U                            | NA                                          | NLE                                          |
| 2,4,5-Trichlorophenol                                          | 25 U                              | 5.6 U                            | NA                                          | 700                                          |
| 2,4-Dinitrophenol                                              | 29 U                              | 6.4 U                            | NA                                          | 40                                           |
| 4-Nitrophenol                                                  | 6.0 U                             | 1.3 U                            | NA                                          | NLE                                          |
| 4,6-Dinotro-2-methylphenol                                     | 20 U                              | 4.5 U                            | NA                                          | NLE                                          |
| Pentachlorophenol                                              | 13 U                              | 2.8 U                            | NA                                          | 1                                            |
| bis(2-Chloroethyl)Ether                                        | 6.2                               | 1.4 U                            | NA                                          | 10                                           |
| 1,3-Dichlorobenzene                                            | 17 U                              | 3.8 U                            | NA                                          | 600                                          |
| 1,4-Dichlorobenzene                                            | 18 U                              | 3.9 U                            | NA                                          | 75                                           |
| 1,2-Dichlorobenzene                                            | 17 U                              | 3.8 U                            | NA                                          | 600                                          |
| bis(2-Chloroisopropyl)ether                                    | 7.0 U                             | 1.6 U                            | NA                                          | 300                                          |
| N-Nitroso-di-n-propylamine                                     | 7.5 U                             | 1.7 U                            | NA                                          | 20                                           |
| Hexachloroethane                                               | 12 U                              | 2.7 U                            | NA                                          | 10                                           |
| Nitrobenzene                                                   | 7.5 U                             | 1.7 U                            | NA                                          | 10                                           |
| Isophorone                                                     | 8.5 U                             | 1.9 U                            | NA                                          | 100                                          |
| bis(2-Chloroethoxy)Methane                                     | 8.3 U                             | 1.8 U                            | NA                                          | NLE                                          |
| 1,2,4-Trichlorobenzene                                         | 19 U                              | 4.2 U                            | NA                                          | 9                                            |
| Naphthalene                                                    | 13 U                              | 2.8 U                            | NA                                          | NLE                                          |
| 4-Chloroaniline                                                | 25 U                              | 5.6 U                            | NA                                          | NLE                                          |
| Hexachlorobutadiene                                            | 11 U                              | 2.4 U                            | NA                                          | 1                                            |
| 2-Methylnaphthalene                                            | 25 U                              | 5.6 U                            | NA                                          | NLE                                          |
| Hexachlorocyclopentadiene                                      | 8.2 U                             | 1.8 U                            | NA                                          | 50                                           |
| 2-Choronaphthalene                                             | 16 U                              | 3.5 U                            | NA                                          | NLE                                          |
| 2-Nitroaniline                                                 | 25 U                              | 5.6 U                            | NA                                          | NLE                                          |
| Dimethyl Phthalate                                             | 6.4 U                             | 1.4 U                            | NA                                          | 7000                                         |
| Acenaphthylene                                                 | 10 U                              | 2.3 U                            | NA                                          | 10                                           |
| 2,6-Dinitrotoluene                                             | 7.5 U                             | 1.7 U                            | NA                                          | 10                                           |
| 3-Nitroaniline                                                 | 25 U                              | 5.6 U                            | NA                                          | NLE                                          |
| Acenaphthene                                                   | 14 U                              | 3.1 U                            | NA                                          | 400                                          |
| Dibenzofuran                                                   | 25 U                              | 5.6 U                            | NA                                          | NLE                                          |
| 2,4-Dinitrotoluene                                             | 7.5 U                             | 1.7 U                            | NA                                          | 10                                           |
| Diethylphthalate                                               | 5.8 U                             | 1.3 U                            | NA                                          | 5000                                         |
| 4-Chlorophenyl-phenylether                                     | 14 U                              | 3.2 U                            | NA                                          | NLE                                          |
| Fluorene                                                       | 10 U                              | 2.2 U                            | NA                                          | 300                                          |
| 4-Nitroaniline                                                 | 25 U                              | 5.6 U                            | NA                                          | NLE                                          |
| N-Nitrosodiphenylamine                                         | 5.6 U                             | 1.2 U                            | NA                                          | 20                                           |
| 4-Bromophenyl-phenylether                                      | 10 U                              | 2.2 U                            | NA                                          | NLE                                          |
| Hexachlorobenzene                                              | 6.3 U                             | 1.4 U                            | NA                                          | 10                                           |
| Phenanthrene                                                   | 5.2 U                             | 1.2 U                            | NA                                          | 10                                           |
| Anthracene                                                     | 5.6 U                             | 1.2 U                            | NA                                          | 2000                                         |
| Carbazole                                                      | 25 U                              | 5.6 U                            | NA                                          | NLE                                          |
| Di-n-butylphthalate                                            | 4.8 U                             | 1.1 U                            | NA                                          | 900                                          |
| Fluoranthene                                                   | 5.6 U                             | 1.2 U                            | NA                                          | 300                                          |
| Pyrene                                                         | 3.0 U                             | 0.7 U                            | NA                                          | 200                                          |
| Butylbenzylphthalate                                           | 3.3 U                             | 0.7 U                            | NA                                          | 100                                          |



**TABLE 1 (continued)**  
**SUMMARY OF GROUNDWATER SAMPLING DATA**  
**L.E. CARPENTER SITE**  
**WHARTON, NJ**

| Sample ID No.:<br>Laboratory Sample ID No:<br>Date:<br>Matrix: | GW-1<br>55544<br>7/16/96<br>water | GW-2<br>5545<br>7/16/96<br>water | Trip_Blank<br>54739-006<br>7/16/96<br>water | NJDEP<br>GROUNDWATER<br>QUALITY<br>CRITERIA* |
|----------------------------------------------------------------|-----------------------------------|----------------------------------|---------------------------------------------|----------------------------------------------|
| 3,3'-Dichlorobenzidine                                         | 7.3 U                             | 1.6 U                            | NA                                          | 60                                           |
| Benzo(a)anthracene                                             | 4.2 U                             | 0.9 U                            | NA                                          | 10                                           |
| Chrysene                                                       | 4.3 U                             | 1.0 U                            | NA                                          | 20                                           |
| bis(2-Ethylhexyl)phthalate                                     | 670                               | 68                               | NA                                          | 30                                           |
| Di-n-Octylphthalate                                            | 4.9 U                             | 1.1 U                            | NA                                          | 100                                          |
| Benzo(b)fluoranthene                                           | 3.7 U                             | 0.8 U                            | NA                                          | NLE                                          |
| Benzo(k)fluoranthene                                           | 4.6 U                             | 1.0 U                            | NA                                          | 2                                            |
| Benzo(a)pyrene                                                 | 4.0 U                             | 0.9 U                            | NA                                          | 20                                           |
| Indeno(1,2,3-cd)pyrene                                         | 3.5 U                             | 0.8 U                            | NA                                          | 20                                           |
| Dibenzo(a,h)Anthracene                                         | 4.2 U                             | 0.9 U                            | NA                                          | 0.3                                          |
| Benzo(g,h,i)Perylene                                           | 3.7 U                             | 0.8 U                            | NA                                          | 20                                           |
| <b>METAL (ug/L)</b>                                            |                                   |                                  |                                             |                                              |
| Antimony                                                       | 3.6 U                             | 3.6 U                            | NA                                          | 20                                           |
| Arsenic                                                        | 14.2                              | 13.2                             | NA                                          | 8                                            |
| Calcium                                                        | 47,300                            | 46,000                           | NA                                          | NLE                                          |
| Iron                                                           | 16,700                            | 14,600                           | NA                                          | 300                                          |
| Lead                                                           | 2.3 U                             | 2.3 U                            | NA                                          | 10                                           |
| Magnesium                                                      | 18,000                            | 17,000                           | NA                                          | NLE                                          |
| Manganese                                                      | 2,100                             | 2,020                            | NA                                          | 50                                           |
| Sodium                                                         | 19,600                            | 20,900                           | NA                                          | 50000                                        |
| <b>OTHER PARAMETERS</b>                                        | DF: 1                             | DF: 1                            |                                             |                                              |
| Hardness (mg/L)                                                | 192                               | 185                              | NA                                          | 250                                          |
| Alkalinity (mg/L)                                              | 639                               | 146                              | NA                                          | NLE                                          |
| Alkalinity-Bicarbonate (mg/L)                                  | 639                               | 146                              | NA                                          | NLE                                          |
| COD (mg/L)                                                     | 122                               | 20                               | NA                                          | NLE                                          |
| Chloride (mg/L)                                                | 97.5**                            | 53.7**                           | NA                                          | 250,000                                      |
| Nitrate (mg/L)                                                 | 0.1 U                             | 0.1 U                            | NA                                          | 10,000                                       |
| Nitrite (mg/L)                                                 | 0.1 U                             | 0.1 U                            | NA                                          | 1,000                                        |
| Ortho phosphate (mg/L)                                         | 0.17                              | 0.14                             | NA                                          | NLE                                          |
| Color (cu)                                                     | 10                                | 250**                            | NA                                          | 20                                           |
| Sulfate (mg/L)                                                 | 5.3                               | 6.1                              | NA                                          | 250,000                                      |
| Total dissolved solids (mg/L)                                  | 300                               | 278                              | NA                                          | 500,000                                      |
| Total organic carbon (mg/L)                                    | 4.2                               | 2.4                              | NA                                          | NLE                                          |
| Total suspended solids (mg/L)                                  | 37                                | 31                               | NA                                          | NLE                                          |
| Turbidity (NTU)                                                | 150                               | 140                              | NA                                          | NLE                                          |
| pH (std units)                                                 | 7.06                              | 7.22                             | NA                                          | 6.5 - 8.5                                    |
| BOD (mg/L)                                                     | 4.0                               | 4.0                              | NA                                          | NLE                                          |
| Total kjeldahl nitrogen (mg/L)                                 | 0.78                              | 0.48                             | NA                                          | NLE                                          |

Notes:

- (1) - Groundwater samples were collected from RW-2 during the aquifer pumping test.
- (2) - \* = The higher of the Practical Quantitation Level and the Groundwater Quality Criteria was used.
- (3) - Shading indicates detected concentration exceeds applicable NJDEP Groundwater Quality Criteria.
- (4) - NJDEP Groundwater Quality Criteria for total 1,1-Dichloroethene is 10 micrograms per liter.
- (5) - \*\* = Dilution factor was 5.0.
- (6) - U = Not detected at or above reported detection limit or quantitation limit.
- (7) - ug/L = Micrograms per liter.
- (8) - mg/L = Milligrams per liter.
- (9) - DF = Dilution factor.



TABLE 2  
SPECIFIC GRAVITY RESULTS  
L.E. CARPENTER SITE  
WHARTON, NJ

| MONITORING WELL | SPECIFIC GRAVITY |
|-----------------|------------------|
| MW-1R           | 0.900            |
| MW-3            | 0.920            |
| MW-6R           | 0.900            |
| MW-11S          | 0.930            |
| WP-A6           | 0.940            |
| WP-A7           | 0.940            |
| WP-A8           | 0.940            |
| WP-A9           | 0.980            |
| WP-B3           | 0.940            |
| WP-B4           | 0.910            |
| WP-B5           | 0.915            |

NOTES:

- \* Specific gravity measurements could not be conducted on all product bearing wells due to insufficient quantities.
- \* Specific gravity was field determined.

**ENVIROTECH RESEARCH, INC.**

Client ID: **GW-1**  
Site: LE Carpenter

Lab Sample No: **55544**  
Lab Job No: P223

Date Sampled: 07-16-96  
Date Received: 07-17-96  
Date Analyzed: 07-22-96  
GC Column: DB624  
Instrument ID: VOAMS4  
Lab File ID: d9325.d

Matrix: WATER  
Level: LOW  
Purge Volume: 5.0 ml  
Dilution Factor: 10.0

**VOLATILE ORGANICS - GC/MS  
METHOD 624**

| <u>Parameter</u>          | <u>Analytical Result</u><br><u>Units: ug/l</u> | <u>Method Detection</u><br><u>Limit</u><br><u>Units: ug/l</u> |
|---------------------------|------------------------------------------------|---------------------------------------------------------------|
| Chloromethane             | ND                                             | 9.3                                                           |
| Bromomethane              | ND                                             | 2.7                                                           |
| Vinyl Chloride            | ND                                             | 3.9                                                           |
| Chloroethane              | ND                                             | 10                                                            |
| Methylene Chloride        | ND                                             | 10                                                            |
| Acetone                   | ND                                             | 50                                                            |
| Carbon Disulfide          | ND                                             | 10                                                            |
| 1,1-Dichloroethene        | ND                                             | 5.5                                                           |
| 1,1-Dichloroethane        | ND                                             | 3.1                                                           |
| trans-1,2-Dichloroethene  | ND                                             | 3.0                                                           |
| cis-1,2-Dichloroethene    | ND                                             | 10                                                            |
| Chloroform                | ND                                             | 2.0                                                           |
| 1,2-Dichloroethane        | ND                                             | 2.2                                                           |
| 2-Butanone                | ND                                             | 50                                                            |
| 1,1,1-Trichloroethane     | ND                                             | 2.0                                                           |
| Carbon Tetrachloride      | ND                                             | 1.6                                                           |
| Bromodichloromethane      | ND                                             | 1.9                                                           |
| 1,2-Dichloropropane       | ND                                             | 4.6                                                           |
| cis-1,3-Dichloropropene   | ND                                             | 3.3                                                           |
| Trichloroethene           | ND                                             | 4.1                                                           |
| Dibromochloromethane      | ND                                             | 2.3                                                           |
| 1,1,2-Trichloroethane     | ND                                             | 4.3                                                           |
| Benzene                   | ND                                             | 2.4                                                           |
| trans-1,3-Dichloropropene | ND                                             | 3.1                                                           |
| Bromoform                 | ND                                             | 3.0                                                           |
| 4-Methyl-2-Pentanone      | ND                                             | 50                                                            |
| 2-Hexanone                | ND                                             | 50                                                            |
| Tetrachloroethene         | ND                                             | 1.0                                                           |
| 1,1,2,2-Tetrachloroethane | ND                                             | 3.3                                                           |
| Toluene                   | ND                                             | 1.8                                                           |
| Chlorobenzene             | ND                                             | 1.4                                                           |
| Ethylbenzene              | 460                                            | 2.4                                                           |
| Styrene                   | ND                                             | 10                                                            |
| Xylene (Total)            | 1400                                           | 10                                                            |

**ENVIROTECH RESEARCH, INC.**

Client ID: GW-1  
Site: LE Carpenter

Lab Sample No: 55544  
Lab Job No: P223

Date Sampled: 07-16-96  
Date Received: 07-17-96  
Date Analyzed: 07-22-96  
GC Column: DB624  
Instrument ID: VOAMS4  
Lab File ID: D9325.D

Matrix: WATER  
Level: LOW  
Purge Volume: 5.0 ml  
Dilution Factor: 10.0

**VOLATILE ORGANICS - GC/MS  
TENTATIVELY IDENTIFIED COMPOUNDS**

| COMPOUND NAME              | RT    | EST.<br>CONC.<br>ug/l | Q |
|----------------------------|-------|-----------------------|---|
| 1. Trimethylbenzene isomer | 15.62 | 35                    |   |
| 2.                         |       |                       |   |
| 3.                         |       |                       |   |
| 4.                         |       |                       |   |
| 5.                         |       |                       |   |
| 6.                         |       |                       |   |
| 7.                         |       |                       |   |
| 8.                         |       |                       |   |
| 9.                         |       |                       |   |
| 10.                        |       |                       |   |
| 11.                        |       |                       |   |
| 12.                        |       |                       |   |
| 13.                        |       |                       |   |
| 14.                        |       |                       |   |
| 15.                        |       |                       |   |
| 16.                        |       |                       |   |
| 17.                        |       |                       |   |
| 18.                        |       |                       |   |
| 19.                        |       |                       |   |
| 20.                        |       |                       |   |
| 21.                        |       |                       |   |
| 22.                        |       |                       |   |
| 23.                        |       |                       |   |
| 24.                        |       |                       |   |
| 25.                        |       |                       |   |
| 26.                        |       |                       |   |
| 27.                        |       |                       |   |
| 28.                        |       |                       |   |
| 29.                        |       |                       |   |
| 30.                        |       |                       |   |

TOTAL ESTIMATED CONCENTRATION

35

**ENVIROTECH RESEARCH, INC.**

Client ID: **GW-1**  
Site: LE Carpenter

Lab Sample No: **55544**  
Lab Job No: P223

Date Sampled: 07-16-96  
Date Received: 07-17-96  
Date Extracted: 07-18-96  
Date Analyzed: 08-02-96  
GC Column: DB-5  
Instrument ID: BNAMS3

Matrix: WATER  
Level: LOW  
Sample Volume: 990 ml  
Extract Final Volume: 2.0 ml  
Dilution Factor: 5.0  
Lab File ID: t6358.d

**SEMI-VOLATILE ORGANICS - GC/MS**  
**METHOD 625**

| <u>Parameter</u>           | <u>Analytical Result</u><br><u>Units: ug/l</u> | <u>Method Detection Limit</u><br><u>Units: ug/l</u> |
|----------------------------|------------------------------------------------|-----------------------------------------------------|
| Phenol                     | ND                                             | 5.6                                                 |
| 2-Chlorophenol             | ND                                             | 11                                                  |
| 2-Methylphenol             | ND                                             | 25                                                  |
| 4-Methylphenol             | ND                                             | 25                                                  |
| 2-Nitrophenol              | ND                                             | 15                                                  |
| 2,4-Dimethylphenol         | ND                                             | 14                                                  |
| 2,4-Dichlorophenol         | ND                                             | 15                                                  |
| 4-Chloro-3-methylphenol    | ND                                             | 14                                                  |
| 2,4,6-Trichlorophenol      | ND                                             | 15                                                  |
| 2,4,5-Trichlorophenol      | ND                                             | 25                                                  |
| 2,4-Dinitrophenol          | ND                                             | 29                                                  |
| 4-Nitrophenol              | ND                                             | 6.0                                                 |
| 4,6-Dinitro-2-methylphenol | ND                                             | 20                                                  |
| Pentachlorophenol          | ND                                             | 13                                                  |

**ENVIROTECH RESEARCH, INC.**

Client ID: **GW-1**  
Site: LE Carpenter

Lab Sample No: **55544**  
Lab Job No: P223

Date Sampled: 07-16-96  
Date Received: 07-17-96  
Date Extracted: 07-18-96  
Date Analyzed: 08-02-96  
GC Column: DB-5  
Instrument ID: BNAMS3

Matrix: WATER  
Level: LOW  
Sample Volume: 990 ml  
Extract Final Volume: 2.0 ml  
Dilution Factor: 5.0  
Lab File ID: t6358.d

**SEMI-VOLATILE ORGANICS - GC/MS**  
**METHOD 625**

| <u>Parameter</u>            | <u>Analytical Result</u><br><u>Units: ug/l</u> | <u>Method Detection Limit</u><br><u>Units: ug/l</u> |
|-----------------------------|------------------------------------------------|-----------------------------------------------------|
| bis(2-Chloroethyl)ether     | ND                                             | 6.2                                                 |
| 1,3-Dichlorobenzene         | ND                                             | 17                                                  |
| 1,4-Dichlorobenzene         | ND                                             | 18                                                  |
| 1,2-Dichlorobenzene         | ND                                             | 17                                                  |
| bis(2-chloroisopropyl)ether | ND                                             | 7.0                                                 |
| N-Nitroso-di-n-propylamine  | ND                                             | 7.5                                                 |
| Hexachloroethane            | ND                                             | 12                                                  |
| Nitrobenzene                | ND                                             | 7.5                                                 |
| Isophorone                  | ND                                             | 8.5                                                 |
| bis(2-Chloroethoxy)methane  | ND                                             | 8.3                                                 |
| 1,2,4-Trichlorobenzene      | ND                                             | 19                                                  |
| Naphthalene                 | ND                                             | 13                                                  |
| 4-Chloroaniline             | ND                                             | 25                                                  |
| Hexachlorobutadiene         | ND                                             | 11                                                  |
| 2-Methylnaphthalene         | ND                                             | 25                                                  |
| Hexachlorocyclopentadiene   | ND                                             | 8.2                                                 |
| 2-Chloronaphthalene         | ND                                             | 16                                                  |
| 2-Nitroaniline              | ND                                             | 25                                                  |
| Dimethylphthalate           | ND                                             | 6.4                                                 |
| Acenaphthylene              | ND                                             | 10                                                  |
| 2,6-Dinitrotoluene          | ND                                             | 7.5                                                 |
| 3-Nitroaniline              | ND                                             | 25                                                  |
| Acenaphthene                | ND                                             | 14                                                  |
| Dibenzofuran                | ND                                             | 25                                                  |
| 2,4-Dinitrotoluene          | ND                                             | 7.5                                                 |
| Diethylphthalate            | ND                                             | 5.8                                                 |
| 4-Chlorophenyl-phenylether  | ND                                             | 14                                                  |
| Fluorene                    | ND                                             | 9.8                                                 |
| 4-Nitroaniline              | ND                                             | 25                                                  |
| N-Nitrosodiphenylamine      | ND                                             | 5.6                                                 |
| 4-Bromophenyl-phenylether   | ND                                             | 10                                                  |
| Hexachlorobenzene           | ND                                             | 6.3                                                 |
| Phenanthrene                | ND                                             | 5.2                                                 |

**ENVIROTECH RESEARCH, INC.**

Client ID: GW-1  
Site: LE Carpenter

Lab Sample No: 55544  
Lab Job No: P223

Date Sampled: 07-16-96  
Date Received: 07-17-96  
Date Extracted: 07-18-96  
Date Analyzed: 08-02-96  
GC Column: DB-5  
Instrument ID: BNAMS3

Matrix: WATER  
Level: LOW  
Sample Volume: 990 ml  
Extract Final Volume: 2.0 ml  
Dilution Factor: 5.0  
Lab File ID: t6358.d

**SEMI-VOLATILE ORGANICS - GC/MS  
METHOD 625**

| <u>Parameter</u>           | <u>Analytical Result</u><br><u>Units: ug/l</u> | <u>Method Detection Limit</u><br><u>Units: ug/l</u> |
|----------------------------|------------------------------------------------|-----------------------------------------------------|
| Anthracene                 | ND                                             | 5.6                                                 |
| Carbazole                  | ND                                             | 25                                                  |
| Di-n-butylphthalate        | ND                                             | 4.8                                                 |
| Fluoranthene               | ND                                             | 5.6                                                 |
| Pyrene                     | ND                                             | 3.0                                                 |
| Butylbenzylphthalate       | ND                                             | 3.3                                                 |
| 3,3'-Dichlorobenzidine     | ND                                             | 7.3                                                 |
| Benzo(a)anthracene         | ND                                             | 4.2                                                 |
| Chrysene                   | ND                                             | 4.3                                                 |
| bis(2-Ethylhexyl)phthalate | 670                                            | 5.8                                                 |
| Di-n-octylphthalate        | ND                                             | 4.9                                                 |
| Benzo(b)fluoranthene       | ND                                             | 3.7                                                 |
| Benzo(k)fluoranthene       | ND                                             | 4.6                                                 |
| Benzo(a)pyrene             | ND                                             | 4.0                                                 |
| Indeno(1,2,3-cd)pyrene     | ND                                             | 3.5                                                 |
| Dibenz(a,h)anthracene      | ND                                             | 4.2                                                 |
| Benzo(g,h,i)perylene       | ND                                             | 3.7                                                 |

**ENVIROTECH RESEARCH, INC.**

Client ID: GW-1  
Site: LE Carpenter

Lab Sample No: 55544  
Lab Job No: P223

Date Sampled: 07-16-96  
Date Received: 07-17-96  
Date Extracted: 07-18-96  
Date Analyzed: 08-02-96  
GC Column: DB-5  
Instrument ID: BNAMS3

Matrix: WATER  
Level: LOW  
Sample Volume: 990 ml  
Extract Final Volume: 2.0 ml  
Dilution Factor: 5.0  
Lab File ID: T6358.D

**SEMI-VOLATILE ORGANICS - GC/MS  
TENTATIVELY IDENTIFIED COMPOUNDS**

| COMPOUND NAME    | RT    | EST.<br>CONC.<br>ug/l | Q |
|------------------|-------|-----------------------|---|
| 1. Ethylbenzene  | 10.86 | 290                   |   |
| 2. Xylene Isomer | 11.12 | 940                   |   |
| 3. Xylene Isomer | 11.71 | 47                    |   |
| 4.               |       |                       |   |
| 5.               |       |                       |   |
| 6.               |       |                       |   |
| 7.               |       |                       |   |
| 8.               |       |                       |   |
| 9.               |       |                       |   |
| 10.              |       |                       |   |
| 11.              |       |                       |   |
| 12.              |       |                       |   |
| 13.              |       |                       |   |
| 14.              |       |                       |   |
| 15.              |       |                       |   |
| 16.              |       |                       |   |
| 17.              |       |                       |   |
| 18.              |       |                       |   |
| 19.              |       |                       |   |
| 20.              |       |                       |   |
| 21.              |       |                       |   |
| 22.              |       |                       |   |
| 23.              |       |                       |   |
| 24.              |       |                       |   |
| 25.              |       |                       |   |
| 26.              |       |                       |   |
| 27.              |       |                       |   |
| 28.              |       |                       |   |
| 29.              |       |                       |   |
| 30.              |       |                       |   |

TOTAL ESTIMATED CONCENTRATION

1277

**ENVIROTECH RESEARCH, INC.**

Client ID: GW-1  
Site: LE Carpenter

Lab Sample No: 55544  
Lab Job No: P223

Date Sampled: 07/16/96  
Date Received: 07/17/96

Matrix: WATER  
Level: LOW

**METALS ANALYSIS**

| <u>Analyte</u> | <u>Analytical Result</u><br><u>Units: ug/l</u> | <u>Instrument Detection Limit</u> | <u>M</u> |
|----------------|------------------------------------------------|-----------------------------------|----------|
| Antimony       | ND                                             | 3.6                               | P        |
| Arsenic        | 14.2                                           | 3.2                               | P        |
| Calcium        | 47300                                          | 61.2                              | P        |
| Iron           | 16700                                          | 40.7                              | P        |
| Lead           | ND                                             | 2.3                               | P        |
| Magnesium      | 18000                                          | 59.3                              | P        |
| Manganese      | 2100                                           | 0.60                              | P        |
| Sodium         | 19600                                          | 206                               | P        |

M Column - Method Code (See Section 2 of Report)

**ENVIROTECH RESEARCH, INC.**

Client ID: **GW-2**  
Site: LE Carpenter

Lab Sample No: **55545**  
Lab Job No: P223

Date Sampled: 07-16-96  
Date Received: 07-17-96  
Date Analyzed: 07-22-96  
GC Column: DB624  
Instrument ID: VOAMS4  
Lab File ID: d9326.d

Matrix: WATER  
Level: LOW  
Purge Volume: 5.0 ml  
Dilution Factor: 5.0

**VOLATILE ORGANICS - GC/MS  
METHOD 624**

| <u>Parameter</u>          | <u>Analytical Result</u><br><u>Units: ug/l</u> | <u>Method Detection Limit</u><br><u>Units: ug/l</u> |
|---------------------------|------------------------------------------------|-----------------------------------------------------|
| Chloromethane             | ND                                             | 4.6                                                 |
| Bromomethane              | ND                                             | 1.4                                                 |
| Vinyl Chloride            | ND                                             | 2.0                                                 |
| Chloroethane              | ND                                             | 5.2                                                 |
| Methylene Chloride        | ND                                             | 5.2                                                 |
| Acetone                   | ND                                             | 25                                                  |
| Carbon Disulfide          | ND                                             | 5.0                                                 |
| 1,1-Dichloroethene        | ND                                             | 2.8                                                 |
| 1,1-Dichloroethane        | ND                                             | 1.6                                                 |
| trans-1,2-Dichloroethene  | ND                                             | 1.5                                                 |
| cis-1,2-Dichloroethene    | ND                                             | 5.0                                                 |
| Chloroform                | ND                                             | 1.0                                                 |
| 1,2-Dichloroethane        | ND                                             | 1.1                                                 |
| 2-Butanone                | ND                                             | 25                                                  |
| 1,1,1-Trichloroethane     | ND                                             | 1.0                                                 |
| Carbon Tetrachloride      | ND                                             | 0.8                                                 |
| Bromodichloromethane      | ND                                             | 0.9                                                 |
| 1,2-Dichloroproppane      | ND                                             | 2.3                                                 |
| cis-1,3-Dichloropropene   | ND                                             | 1.6                                                 |
| Trichloroethene           | ND                                             | 2.0                                                 |
| Dibromochloromethane      | ND                                             | 1.2                                                 |
| 1,1,2-Trichloroethane     | ND                                             | 2.2                                                 |
| Benzene                   | ND                                             | 1.2                                                 |
| trans-1,3-Dichloropropene | ND                                             | 1.6                                                 |
| Bromoform                 | ND                                             | 1.5                                                 |
| 4-Methyl-2-Pentanone      | ND                                             | 25                                                  |
| 2-Hexanone                | ND                                             | 25                                                  |
| Tetrachloroethene         | ND                                             | 0.5                                                 |
| 1,1,2,2-Tetrachloroethane | ND                                             | 1.6                                                 |
| Toluene                   | ND                                             | 0.9                                                 |
| Chlorobenzene             | ND                                             | 0.7                                                 |
| Ethylbenzene              | 180                                            | 1.2                                                 |
| Styrene                   | ND                                             | 5.0                                                 |
| Xylene (Total)            | 630                                            | 5.0                                                 |

**ENVIROTECH RESEARCH, INC.**

Client ID: **GW-2**  
Site: LE Carpenter

Lab Sample No: **55545**  
Lab Job No: P223

Date Sampled: 07-16-96  
Date Received: 07-17-96  
Date Analyzed: 07-22-96  
GC Column: DB624  
Instrument ID: VOAMS4  
Lab File ID: D9326.D

Matrix: WATER  
Level: LOW  
Purge Volume: 5.0 ml  
Dilution Factor: 5.0

**VOLATILE ORGANICS - GC/MS  
TENTATIVELY IDENTIFIED COMPOUNDS**

| COMPOUND NAME              | RT    | EST.<br>CONC.<br>ug/l | Q |
|----------------------------|-------|-----------------------|---|
| 1. Trimethylbenzene isomer | 15.61 | 18                    |   |
| 2.                         |       |                       |   |
| 3.                         |       |                       |   |
| 4.                         |       |                       |   |
| 5.                         |       |                       |   |
| 6.                         |       |                       |   |
| 7.                         |       |                       |   |
| 8.                         |       |                       |   |
| 9.                         |       |                       |   |
| 10.                        |       |                       |   |
| 11.                        |       |                       |   |
| 12.                        |       |                       |   |
| 13.                        |       |                       |   |
| 14.                        |       |                       |   |
| 15.                        |       |                       |   |
| 16.                        |       |                       |   |
| 17.                        |       |                       |   |
| 18.                        |       |                       |   |
| 19.                        |       |                       |   |
| 20.                        |       |                       |   |
| 21.                        |       |                       |   |
| 22.                        |       |                       |   |
| 23.                        |       |                       |   |
| 24.                        |       |                       |   |
| 25.                        |       |                       |   |
| 26.                        |       |                       |   |
| 27.                        |       |                       |   |
| 28.                        |       |                       |   |
| 29.                        |       |                       |   |
| 30.                        |       |                       |   |

TOTAL ESTIMATED CONCENTRATION

18

**ENVIROTECH RESEARCH, INC.**

Client ID: **GW-2**  
Site: LE Carpenter

Lab Sample No: **55545**  
Lab Job No: P223

Date Sampled: 07-16-96  
Date Received: 07-17-96  
Date Extracted: 07-18-96  
Date Analyzed: 07-26-96  
GC Column: DB-5  
Instrument ID: BNAMS3

Matrix: WATER  
Level: LOW  
Sample Volume: 890 ml  
Extract Final Volume: 2.0 ml  
Dilution Factor: 1.0  
Lab File ID: t6263.d

**SEMI-VOLATILE ORGANICS - GC/MS**  
**METHOD 625**

| <u>Parameter</u>           | <u>Analytical Result</u><br><u>Units: ug/l</u> | <u>Method Detection Limit</u><br><u>Units: ug/l</u> |
|----------------------------|------------------------------------------------|-----------------------------------------------------|
| Phenol                     | ND                                             | 1.2                                                 |
| 2-Chlorophenol             | ND                                             | 2.4                                                 |
| 2-Methylphenol             | ND                                             | 5.6                                                 |
| 4-Methylphenol             | ND                                             | 5.6                                                 |
| 2-Nitrophenol              | ND                                             | 3.4                                                 |
| 2,4-Dimethylphenol         | 6.2                                            | 3.1                                                 |
| 2,4-Dichlorophenol         | ND                                             | 3.3                                                 |
| 4-Chloro-3-methylphenol    | ND                                             | 3.2                                                 |
| 2,4,6-Trichlorophenol      | ND                                             | 3.4                                                 |
| 2,4,5-Trichlorophenol      | ND                                             | 5.6                                                 |
| 2,4-Dinitrophenol          | ND                                             | 6.4                                                 |
| 4-Nitrophenol              | ND                                             | 1.3                                                 |
| 4,6-Dinitro-2-methylphenol | ND                                             | 4.5                                                 |
| Pentachlorophenol          | ND                                             | 2.8                                                 |

# ENVIROTECH RESEARCH, INC.

Client ID: GW-2  
Site: LE Carpenter

Lab Sample No: 55545  
Lab Job No: P223

Date Sampled: 07-16-96  
Date Received: 07-17-96  
Date Extracted: 07-18-96  
Date Analyzed: 07-26-96  
GC Column: DB-5  
Instrument ID: BNAMS3

Matrix: WATER  
Level: LOW  
Sample Volume: 890 ml  
Extract Final Volume: 2.0 ml  
Dilution Factor: 1.0  
Lab File ID: t6263.d

## SEMI-VOLATILE ORGANICS - GC/MS METHOD 625

| <u>Parameter</u>            | <u>Analytical Result</u><br><u>Units: ug/l</u> | <u>Method Detection Limit</u><br><u>Units: ug/l</u> |
|-----------------------------|------------------------------------------------|-----------------------------------------------------|
| bis(2-Chloroethyl)ether     | ND                                             | 1.4                                                 |
| 1,3-Dichlorobenzene         | ND                                             | 3.8                                                 |
| 1,4-Dichlorobenzene         | ND                                             | 3.9                                                 |
| 1,2-Dichlorobenzene         | ND                                             | 3.8                                                 |
| bis(2-chloroisopropyl)ether | ND                                             | 1.6                                                 |
| N-Nitroso-di-n-propylamine  | ND                                             | 1.7                                                 |
| Hexachloroethane            | ND                                             | 2.7                                                 |
| Nitrobenzene                | ND                                             | 1.7                                                 |
| Isophorone                  | ND                                             | 1.9                                                 |
| bis(2-Chloroethoxy)methane  | ND                                             | 1.8                                                 |
| 1,2,4-Trichlorobenzene      | ND                                             | 4.2                                                 |
| Naphthalene                 | ND                                             | 2.8                                                 |
| 4-Chloroaniline             | ND                                             | 5.6                                                 |
| Hexachlorobutadiene         | ND                                             | 2.4                                                 |
| 2-Methylnaphthalene         | ND                                             | 5.6                                                 |
| Hexachlorocyclopentadiene   | ND                                             | 1.8                                                 |
| 2-Chloronaphthalene         | ND                                             | 3.5                                                 |
| 2-Nitroaniline              | ND                                             | 5.6                                                 |
| Dimethylphthalate           | ND                                             | 1.4                                                 |
| Acenaphthylene              | ND                                             | 2.3                                                 |
| 2,6-Dinitrotoluene          | ND                                             | 1.7                                                 |
| 3-Nitroaniline              | ND                                             | 5.6                                                 |
| Acenaphthene                | ND                                             | 3.1                                                 |
| Dibenzofuran                | ND                                             | 5.6                                                 |
| 2,4-Dinitrotoluene          | ND                                             | 1.7                                                 |
| Diethylphthalate            | ND                                             | 1.3                                                 |
| 4-Chlorophenyl-phenylether  | ND                                             | 3.2                                                 |
| Fluorene                    | ND                                             | 2.2                                                 |
| 4-Nitroaniline              | ND                                             | 5.6                                                 |
| N-Nitrosodiphenylamine      | ND                                             | 1.2                                                 |
| 4-Bromophenyl-phenylether   | ND                                             | 2.2                                                 |
| Hexachlorobenzene           | ND                                             | 1.4                                                 |
| Phenanthrene                | ND                                             | 1.2                                                 |

**ENVIROTECH RESEARCH, INC.**

Client ID: **GW-2**  
Site: LE Carpenter

Lab Sample No: **55545**  
Lab Job No: P223

Date Sampled: 07-16-96  
Date Received: 07-17-96  
Date Extracted: 07-18-96  
Date Analyzed: 07-26-96  
GC Column: DB-5  
Instrument ID: BNAMS3

Matrix: WATER  
Level: LOW  
Sample Volume: 890 ml  
Extract Final Volume: 2.0 ml  
Dilution Factor: 1.0  
Lab File ID: t6263.d

**SEMI-VOLATILE ORGANICS - GC/MS**  
**METHOD 625**

| <u>Parameter</u>           | <u>Analytical Result</u><br><u>Units: ug/l</u> | <u>Method Detection Limit</u><br><u>Units: ug/l</u> |
|----------------------------|------------------------------------------------|-----------------------------------------------------|
| Anthracene                 | ND                                             | 1.2                                                 |
| Carbazole                  | ND                                             | 5.6                                                 |
| Di-n-butylphthalate        | ND                                             | 1.1                                                 |
| Fluoranthene               | ND                                             | 1.2                                                 |
| Pyrene                     | ND                                             | 0.7                                                 |
| Butylbenzylphthalate       | ND                                             | 0.7                                                 |
| 3,3'-Dichlorobenzidine     | ND                                             | 1.6                                                 |
| Benzo(a)anthracene         | ND                                             | 0.9                                                 |
| Chrysene                   | ND                                             | 1.0                                                 |
| bis(2-Ethylhexyl)phthalate | 68                                             | 1.3                                                 |
| Di-n-octylphthalate        | ND                                             | 1.1                                                 |
| Benzo(b)fluoranthene       | ND                                             | 0.8                                                 |
| Benzo(k)fluoranthene       | ND                                             | 1.0                                                 |
| Benzo(a)pyrene             | ND                                             | 0.9                                                 |
| Indeno(1,2,3-cd)pyrene     | ND                                             | 0.8                                                 |
| Dibenz(a,h)anthracene      | ND                                             | 0.9                                                 |
| Benzo(g,h,i)perylene       | ND                                             | 0.8                                                 |

# ENVIROTECH RESEARCH, INC.

Client ID: **GW-2**  
Site: LE Carpenter

Lab Sample No: **55545**  
Lab Job No: P223

Date Sampled: 07-16-96  
Date Received: 07-17-96  
Date Extracted: 07-18-96  
Date Analyzed: 07-26-96  
GC Column: DB-5  
Instrument ID: BNAMS3

Matrix: WATER  
Level: LOW  
Sample Volume: 890 ml  
Extract Final Volume: 2.0 ml  
Dilution Factor: 1.0  
Lab File ID: T6263.D

## SEMI-VOLATILE ORGANICS - GC/MS TENTATIVELY IDENTIFIED COMPOUNDS

| COMPOUND NAME    | RT    | EST.<br>CONC.<br>ug/l | Q |
|------------------|-------|-----------------------|---|
| 1. Ethylbenzene  | 10.87 | 92                    |   |
| 2. Xylene isomer | 11.11 | 320                   |   |
| 3. Xylene isomer | 11.72 | 22                    |   |
| 4.               |       |                       |   |
| 5.               |       |                       |   |
| 6.               |       |                       |   |
| 7.               |       |                       |   |
| 8.               |       |                       |   |
| 9.               |       |                       |   |
| 10.              |       |                       |   |
| 11.              |       |                       |   |
| 12.              |       |                       |   |
| 13.              |       |                       |   |
| 14.              |       |                       |   |
| 15.              |       |                       |   |
| 16.              |       |                       |   |
| 17.              |       |                       |   |
| 18.              |       |                       |   |
| 19.              |       |                       |   |
| 20.              |       |                       |   |
| 21.              |       |                       |   |
| 22.              |       |                       |   |
| 23.              |       |                       |   |
| 24.              |       |                       |   |
| 25.              |       |                       |   |
| 26.              |       |                       |   |
| 27.              |       |                       |   |
| 28.              |       |                       |   |
| 29.              |       |                       |   |
| 30.              |       |                       |   |

TOTAL ESTIMATED CONCENTRATION

434

**ENVIROTECH RESEARCH, INC.**

Client ID: GW-2  
Site: LE Carpenter

Lab Sample No: 55545  
Lab Job No: P223

Date Sampled: 07/16/96  
Date Received: 07/17/96

Matrix: WATER  
Level: LOW

**METALS ANALYSIS**

| <u>Analyte</u> | <u>Analytical<br/>Result<br/>Units: ug/l</u> | <u>Instrument<br/>Detection<br/>Limit</u> | <u>M</u> |
|----------------|----------------------------------------------|-------------------------------------------|----------|
| Antimony       | ND                                           | 3.6                                       | P        |
| Arsenic        | 13.2                                         | 3.2                                       | P        |
| Calcium        | 46000                                        | 61.2                                      | P        |
| Iron           | 14600                                        | 40.7                                      | P        |
| Lead           | ND                                           | 2.3                                       | P        |
| Magnesium      | 17000                                        | 59.3                                      | P        |
| Manganese      | 2020                                         | 0.60                                      | P        |
| Sodium         | 20900                                        | 206                                       | P        |

M Column - Method Code (See Section 2 of Report)

**ENVIROTECH RESEARCH, INC.**

Site: LE Carpenter

Lab Job No: P223

Date Sampled: 7/16/96

Date Analyzed: 7/19/96

Date Received: 7/17/96

Matrix: WATER

QA Batch: 3752

HARDNESS (as CaCO<sub>3</sub>)

| <u>Envirotech<br/>Sample #</u> | <u>Client ID</u> | <u>Dilution<br/>Factor</u> | <u>Analytical Result<br/>Units: mg/l</u> |
|--------------------------------|------------------|----------------------------|------------------------------------------|
| 55544                          | GW-1             | 1.0                        | 192                                      |
| 55545                          | GW-2             | 1.0                        | 185                                      |

Quantitation Limit for Hardness is 0.39 mg/l for an undiluted sample.

# **ENVIROTECH RESEARCH, INC.**

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Site: LE Carpenter

Lab Job No: P223

Date Sampled: 7/16/96

Date Received: 7/17/96

Matrix: WATER

Date Analyzed: 7/29/96

QA Batch: 1041

## **ALKALINITY**

| <u>Envirotech<br/>Sample #</u> | <u>Client ID</u> | <u>Dilution<br/>Factor</u> | <u>Analytical Result<br/>Units: mg/l</u> |
|--------------------------------|------------------|----------------------------|------------------------------------------|
| 55544                          | GW-1             | 1.0                        | 639                                      |
| 55545                          | GW-2             | 1.0                        | 146                                      |

Quantitation Limit for Alkalinity is 5.0 mg/l for an undiluted sample.

# **ENVIROTECH RESEARCH, INC.**

---

Site: LE Carpenter

Lab Job No: P223

Date Sampled: 7/16/96

Date Received: 7/17/96

Matrix: WATER

Date Analyzed: 7/29/96

QA Batch: 1041

## **ALKALINITY - BICARBONATE**

| <u>Envirotech<br/>Sample #</u> | <u>Client ID</u> | <u>Dilution<br/>Factor</u> | <u>Analytical Result<br/>Units: mg/l</u> |
|--------------------------------|------------------|----------------------------|------------------------------------------|
| 55544                          | GW-1             | 1.0                        | 639                                      |
| 55545                          | GW-2             | 1.0                        | 146                                      |

Quantitation Limit for Alkalinity - Bicarbonate is 5.0 mg/l for an undiluted sample.

# **ENVIROTECH RESEARCH, INC.**

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Site: LE Carpenter

Lab Job No: P223

Date Sampled: 7/16/96

Date Received: 7/17/96

Matrix: WATER

Date Analyzed: 7/23/96

QA Batch: 1134

## COD

| <u>Envirotech<br/>Sample #</u> | <u>Client ID</u> | <u>Dilution<br/>Factor</u> | <u>Analytical Result<br/>Units: mg/l</u> |
|--------------------------------|------------------|----------------------------|------------------------------------------|
| 55544                          | GW-1             | 1.0                        | 122                                      |
| 55545                          | GW-2             | 1.0                        | 20.0                                     |

Quantitation Limit for COD is 10.0 mg/l for an undiluted sample.

# **ENVIROTECH RESEARCH, INC.**

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Site: LE Carpenter

Lab Job No: P223

Date Sampled: 7/16/96

Date Received: 7/17/96

Matrix: WATER

Date Analyzed: 7/24/96

QA Batch: 1079

## CHLORIDE

| <u>Envirotech<br/>Sample #</u> | <u>Client ID</u> | <u>Dilution<br/>Factor</u> | <u>Analytical Result<br/>Units: mg/l</u> |
|--------------------------------|------------------|----------------------------|------------------------------------------|
| 55544                          | GW-1             | 5.0                        | 97.5                                     |
| 55545                          | GW-2             | 5.0                        | 53.7                                     |

Quantitation Limit for Chloride is 5.0 mg/l for an undiluted sample.

# **ENVIROTECH RESEARCH, INC.**

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Site: LE Carpenter

Lab Job No: P223

Date Sampled: 7/16/96

Date Received: 7/17/96

Matrix: WATER

Date Analyzed: 7/19/96

QA Batch: 1058

## NITRATE

| <u>Envirotech<br/>Sample #</u> | <u>Client ID</u> | <u>Dilution<br/>Factor</u> | <u>Analytical Result<br/>Units: mg/l</u> |
|--------------------------------|------------------|----------------------------|------------------------------------------|
| 55544                          | GW-1             | 1.0                        | ND                                       |
| 55545                          | GW-2             | 1.0                        | ND                                       |

Quantitation Limit for Nitrate is 0.10 mg/l for an undiluted sample.

# **ENVIROTECH RESEARCH, INC.**

---

Site: LE Carpenter

Lab Job No: P223

Date Sampled: 7/16/96

Date Received: 7/17/96

Matrix: WATER

Date Analyzed: 7/18/96

QA Batch: 1018

## NITRITE

| <u>Envirotech<br/>Sample #</u> | <u>Client ID</u> | <u>Dilution<br/>Factor</u> | <u>Analytical Result<br/>Units: mg/l</u> |
|--------------------------------|------------------|----------------------------|------------------------------------------|
| 55544                          | GW-1             | 1.0                        | ND                                       |
| 55545                          | GW-2             | 1.0                        | ND                                       |

Quantitation Limit for Nitrite is 0.10 mg/l for an undiluted sample.

# **ENVIROTECH RESEARCH, INC.**

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Site: LE Carpenter

Lab Job No: P223

Date Sampled: 7/16/96

Date Received: 7/17/96

Matrix: WATER

Date Analyzed: 7/18/96

QA Batch: 1027

## ORTHO PHOSPHATE

| <u>Envirotech<br/>Sample #</u> | <u>Client ID</u> | <u>Dilution<br/>Factor</u> | <u>Analytical Result<br/>Units: mg/l</u> |
|--------------------------------|------------------|----------------------------|------------------------------------------|
| 55544                          | GW-1             | 1.0                        | 0.17                                     |
| 55545                          | GW-2             | 1.0                        | 0.14                                     |

Quantitation Limit for Ortho Phosphate is 0.03 mg/l for an undiluted sample.

# **ENVIROTECH RESEARCH, INC.**

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Site: LE Carpenter

Lab Job No: P223

Date Sampled: 7/16/96

Date Received: 7/17/96

Matrix: WATER

Date Analyzed: 7/18/96

QA Batch: 1051

## COLOR

| <u>Envirotech<br/>Sample #</u> | <u>Client ID</u> | <u>Dilution<br/>Factor</u> | <u>Analytical Result<br/>Units: cu</u> |
|--------------------------------|------------------|----------------------------|----------------------------------------|
| 55544                          | GW-1             | 1.0                        | 10                                     |
| 55545                          | GW-2             | 5.0                        | 250                                    |

Quantitation Limit for COLOR is 5.0 cu for an undiluted sample.

# **ENVIROTECH RESEARCH, INC.**

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Site: LE Carpenter

Lab Job No: P223

Date Sampled: 7/16/96  
Date Received: 7/17/96  
Matrix: WATER

Date Extracted: 7/22/96  
Date Analyzed: 7/22/96  
QA Batch: 1063

## SULFATE

| <u>Envirotech<br/>Sample #</u> | <u>Client ID</u> | <u>Dilution<br/>Factor</u> | <u>Analytical Result<br/>Units: mg/l</u> |
|--------------------------------|------------------|----------------------------|------------------------------------------|
| 55544                          | GW-1             | 1.0                        | 5.3                                      |
| 55545                          | GW-2             | 1.0                        | 6.1                                      |

Quantitation Limit for Sulfate is 1.0 mg/l for an undiluted sample.

**ENVIROTECH RESEARCH, INC.**

Site: LE Carpenter

Lab Job No: P223

Date Sampled: 7/16/96

Date Received: 7/17/96

Matrix: WATER

Date Analyzed: 7/19/96

QA Batch: 1328

**TOTAL DISSOLVED SOLIDS**

| <u>Envirotech<br/>Sample #</u> | <u>Client ID</u> | <u>Dilution<br/>Factor</u> | <u>Analytical Result<br/>Units: mg/l</u> |
|--------------------------------|------------------|----------------------------|------------------------------------------|
| 55544                          | GW-1             | 1.0                        | 300                                      |
| 55545                          | GW-2             | 1.0                        | 278                                      |

Quantitation Limit for Total Dissolved Solids is 10.0 mg/l for an undiluted sample.

# **ENVIROTECH RESEARCH, INC.**

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Site: LE Carpenter

Lab Job No: P223

Date Sampled: 7/16/96

Date Received: 7/17/96

Matrix: WATER

Date Analyzed: 7/19/96

QA Batch: 1199

## TOTAL ORGANIC CARBON

| <u>Envirotech<br/>Sample #</u> | <u>Client ID</u> | <u>Dilution<br/>Factor</u> | <u>Analytical Result<br/>Units: mg/l</u> |
|--------------------------------|------------------|----------------------------|------------------------------------------|
| 55544                          | GW-1             | 1.0                        | 4.2                                      |
| 55545                          | GW-2             | 1.0                        | 2.4                                      |

Quantitation Limit for Total Organic Carbon is 1.0 mg/l for an undiluted sample.

# **ENVIROTECH RESEARCH, INC.**

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Site: LE Carpenter

Lab Job No: P223

Date Sampled: 7/16/96

Date Received: 7/17/96

Matrix: WATER

Date Analyzed: 7/23/96

QA Batch: 1130

## TOTAL SUSPENDED SOLIDS

| <u>Envirotech<br/>Sample #</u> | <u>Client ID</u> | <u>Dilution<br/>Factor</u> | <u>Analytical Result<br/>Units: mg/l</u> |
|--------------------------------|------------------|----------------------------|------------------------------------------|
| 55544                          | GW-1             | 1.0                        | 37.0                                     |
| 55545                          | GW-2             | 1.0                        | 31.0                                     |

Quantitation Limit for Total Suspended Solids is 10.0 mg/l for an undiluted sample.

# **ENVIROTECH RESEARCH, INC.**

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Site: LE Carpenter

Lab Job No: P223

Date Sampled: 7/16/96

Date Received: 7/17/96

Matrix: WATER

Date Analyzed: 7/18/96

QA Batch: 1012

## TURBIDITY

| <u>Envirotech<br/>Sample #</u> | <u>Client ID</u> | <u>Dilution<br/>Factor</u> | <u>Analytical Result<br/>Units: NTU</u> |
|--------------------------------|------------------|----------------------------|-----------------------------------------|
| 55544                          | GW-1             | 5.0                        | 150                                     |
| 55545                          | GW-2             | 5.0                        | 140                                     |

Quantitation Limit for Turbidity is 0.50 NTU for an undiluted sample.

# **ENVIROTECH RESEARCH, INC.**

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Site: LE Carpenter

Lab Job No: P223

Date Sampled: 7/16/96

Date Received: 7/17/96

Matrix: WATER

Date Analyzed: 7/18/96

QA Batch: 1437

## pH

| <u>Envirotech<br/>Sample #</u> | <u>Client ID</u> | <u>Analytical Result<br/>Units: std units</u> |
|--------------------------------|------------------|-----------------------------------------------|
| 55544                          | GW-1             | 7.06                                          |
| 55545                          | GW-2             | 7.22                                          |

X - The maximum holding time specified in 40 CFR 136.3(e) for Chlorine (total residual), Hydrogen Ion (pH) Dissolved Oxygen (probe), Sulfite and Temperature is "Analyze immediately". The NJDEP Office of Quality Assurance interprets this to mean within 15 minutes. Analysis outside holding time may not be reported to NJDEP for water pollution or drinking water programs.

# **ENVIROTECH RESEARCH, INC.**

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Site: LE Carpenter

Lab Job No: P223

Date Sampled: 7/16/96

Date Received: 7/17/96

Matrix: WATER

## TOTAL KJELDAHL NITROGEN

| <u>Envirotech<br/>Sample #</u> | <u>Client ID</u> | <u>Analytical Result<br/>Units: mg/l</u> |
|--------------------------------|------------------|------------------------------------------|
| 55544                          | GW-1             | 0.78                                     |
| 55545                          | GW-2             | 0.48                                     |

**ENVIROTECH RESEARCH, INC.**

Client ID: Trip\_Blank  
Site: LE Carpenter

Lab Sample No: 55546  
Lab Job No: P223

Date Sampled: 07-16-96  
Date Received: 07-17-96  
Date Analyzed: 07-22-96  
GC Column: DB624  
Instrument ID: VOAMS4  
Lab File ID: d9324.d

Matrix: WATER  
Level: LOW  
Purge Volume: 5.0 ml  
Dilution Factor: 1.0

**VOLATILE ORGANICS - GC/MS  
METHOD 624**

| <u>Parameter</u>          | <u>Analytical Result</u><br><u>Units: ug/l</u> | <u>Method Detection</u><br><u>Limit</u><br><u>Units: ug/l</u> |
|---------------------------|------------------------------------------------|---------------------------------------------------------------|
| Chloromethane             | ND                                             | 0.9                                                           |
| Bromomethane              | ND                                             | 0.3                                                           |
| Vinyl Chloride            | ND                                             | 0.4                                                           |
| Chloroethane              | ND                                             | 1.0                                                           |
| Methylene Chloride        | ND                                             | 1.0                                                           |
| Acetone                   | ND                                             | 5.0                                                           |
| Carbon Disulfide          | ND                                             | 1.0                                                           |
| 1,1-Dichloroethene        | ND                                             | 0.6                                                           |
| 1,1-Dichloroethane        | ND                                             | 0.3                                                           |
| trans-1,2-Dichloroethene  | ND                                             | 0.3                                                           |
| cis-1,2-Dichloroethene    | ND                                             | 1.0                                                           |
| Chloroform                | ND                                             | 0.2                                                           |
| 1,2-Dichloroethane        | ND                                             | 0.2                                                           |
| 2-Butanone                | ND                                             | 5.0                                                           |
| 1,1,1-Trichloroethane     | ND                                             | 0.2                                                           |
| Carbon Tetrachloride      | ND                                             | 0.2                                                           |
| Bromodichloromethane      | ND                                             | 0.2                                                           |
| 1,2-Dichloropropane       | ND                                             | 0.5                                                           |
| cis-1,3-Dichloropropene   | ND                                             | 0.3                                                           |
| Trichloroethene           | ND                                             | 0.4                                                           |
| Dibromochloromethane      | ND                                             | 0.2                                                           |
| 1,1,2-Trichloroethane     | ND                                             | 0.4                                                           |
| Benzene                   | ND                                             | 0.2                                                           |
| trans-1,3-Dichloropropene | ND                                             | 0.3                                                           |
| Bromoform                 | ND                                             | 0.3                                                           |
| 4-Methyl-2-Pentanone      | ND                                             | 5.0                                                           |
| 2-Hexanone                | ND                                             | 5.0                                                           |
| Tetrachloroethene         | ND                                             | 0.1                                                           |
| 1,1,2,2-Tetrachloroethane | ND                                             | 0.3                                                           |
| Toluene                   | ND                                             | 0.2                                                           |
| Chlorobenzene             | ND                                             | 0.1                                                           |
| Ethylbenzene              | ND                                             | 0.2                                                           |
| Styrene                   | ND                                             | 1.0                                                           |
| Xylene (Total)            | ND                                             | 1.0                                                           |

**ENVIROTECH RESEARCH, INC.**

Client ID: Trip\_Blank  
Site: LE Carpenter

Lab Sample No: 55546  
Lab Job No: P223

Date Sampled: 07-16-96  
Date Received: 07-17-96  
Date Analyzed: 07-22-96  
GC Column: DB624  
Instrument ID: VOAMS4  
Lab File ID: D9324.D

Matrix: WATER  
Level: LOW  
Purge Volume: 5.0 ml  
Dilution Factor: 1.0

**VOLATILE ORGANICS - GC/MS  
TENTATIVELY IDENTIFIED COMPOUNDS**

| COMPOUND NAME                          | RT | EST.<br>CONC.<br>ug/l | Q |
|----------------------------------------|----|-----------------------|---|
| 1. NO VOLATILE ORGANIC COMPOUNDS FOUND |    |                       |   |
| 2.                                     |    |                       |   |
| 3.                                     |    |                       |   |
| 4.                                     |    |                       |   |
| 5.                                     |    |                       |   |
| 6.                                     |    |                       |   |
| 7.                                     |    |                       |   |
| 8.                                     |    |                       |   |
| 9.                                     |    |                       |   |
| 10.                                    |    |                       |   |
| 11.                                    |    |                       |   |
| 12.                                    |    |                       |   |
| 13.                                    |    |                       |   |
| 14.                                    |    |                       |   |
| 15.                                    |    |                       |   |
| 16.                                    |    |                       |   |
| 17.                                    |    |                       |   |
| 18.                                    |    |                       |   |
| 19.                                    |    |                       |   |
| 20.                                    |    |                       |   |
| 21.                                    |    |                       |   |
| 22.                                    |    |                       |   |
| 23.                                    |    |                       |   |
| 24.                                    |    |                       |   |
| 25.                                    |    |                       |   |
| 26.                                    |    |                       |   |
| 27.                                    |    |                       |   |
| 28.                                    |    |                       |   |
| 29.                                    |    |                       |   |
| 30.                                    |    |                       |   |

TOTAL ESTIMATED CONCENTRATION

0.0



**APPENDIX E**  
**INJECTION TEST DATA**

| Elapsed Time | INPUT 1 | Delta H | INPUT 2 | Delta H | INPUT 3 | Delta H | INPUT 4 | Delta H | INPUT 5 | Delta H | INPUT 6 | INPUT 7 | Delta H | INPUT 8 | Delta H |
|--------------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|
|              | MW-6R   | MW-6R   | CW-1    | CW-1    | WP-B2   | WP-B2   | WP-B10  | WP-B10  | MW-2R   | MW-2R   | ATM     | MW-11I  | MW-11I  | WP-B5   | WP-B5   |
| 0            | 100     | 0       | 100.012 | 0.012   | 626.319 | 0.019   | 100.018 | 0.018   | 100.006 | 0.006   | 14.464  | 626.245 | 0.025   | 626.012 | 0.012   |
| 0.0083       | 100.006 | 0.006   | 100.019 | 0.019   | 626.312 | 0.012   | 100.018 | 0.018   | 100     | 0       | 14.464  | 626.232 | 0.012   | 626.012 | 0.012   |
| 0.0166       | 100.006 | 0.006   | 100.012 | 0.012   | 626.312 | 0.012   | 100.018 | 0.018   | 100.006 | 0.006   | 14.464  | 626.232 | 0.012   | 626.012 | 0.012   |
| 0.025        | 100.006 | 0.006   | 100.012 | 0.012   | 626.312 | 0.012   | 100.018 | 0.018   | 100.006 | 0.006   | 14.464  | 626.232 | 0.012   | 626.012 | 0.012   |
| 0.0333       | 100.006 | 0.006   | 100.012 | 0.012   | 626.312 | 0.012   | 100.018 | 0.018   | 100.006 | 0.006   | 14.464  | 626.232 | 0.012   | 626.012 | 0.012   |
| 0.0416       | 100     | 0       | 100.019 | 0.019   | 626.319 | 0.019   | 100.018 | 0.018   | 100.006 | 0.006   | 14.464  | 626.232 | 0.012   | 626.012 | 0.012   |
| 0.05         | 100     | 0       | 100.012 | 0.012   | 626.312 | 0.012   | 100.018 | 0.018   | 100     | 0       | 14.464  | 626.239 | 0.019   | 626.012 | 0.012   |
| 0.0583       | 100.006 | 0.006   | 100.019 | 0.019   | 626.312 | 0.012   | 100.018 | 0.018   | 100.006 | 0.006   | 14.464  | 626.232 | 0.012   | 626.012 | 0.012   |
| 0.0666       | 100     | 0       | 100.019 | 0.019   | 626.312 | 0.012   | 100.018 | 0.018   | 100     | 0       | 14.463  | 626.226 | 0.006   | 626.012 | 0.012   |
| 0.075        | 100.006 | 0.006   | 100.012 | 0.012   | 626.312 | 0.012   | 100.025 | 0.025   | 100.006 | 0.006   | 14.464  | 626.232 | 0.012   | 626.019 | 0.019   |
| 0.0833       | 100.006 | 0.006   | 100.012 | 0.012   | 626.312 | 0.012   | 100.018 | 0.018   | 100.006 | 0.006   | 14.464  | 626.232 | 0.012   | 626.012 | 0.012   |
| 0.0916       | 100     | 0       | 100.012 | 0.012   | 626.312 | 0.012   | 100.018 | 0.018   | 100.006 | 0.006   | 14.464  | 626.232 | 0.012   | 626.012 | 0.012   |
| 0.1          | 100     | 0       | 100.012 | 0.012   | 626.319 | 0.019   | 100.018 | 0.018   | 100.006 | 0.006   | 14.464  | 626.239 | 0.019   | 626.012 | 0.012   |
| 0.1083       | 100     | 0       | 100.019 | 0.019   | 626.312 | 0.012   | 100.018 | 0.018   | 100.006 | 0.006   | 14.464  | 626.232 | 0.012   | 626.012 | 0.012   |
| 0.1166       | 100.006 | 0.006   | 100.019 | 0.019   | 626.319 | 0.019   | 100.012 | 0.012   | 100.006 | 0.006   | 14.464  | 626.232 | 0.012   | 626.012 | 0.012   |
| 0.125        | 100     | 0       | 100.012 | 0.012   | 626.312 | 0.012   | 100.018 | 0.018   | 100.006 | 0.006   | 14.463  | 626.239 | 0.019   | 626.012 | 0.012   |
| 0.1333       | 100     | 0       | 100.019 | 0.019   | 626.312 | 0.012   | 100.012 | 0.012   | 100     | 0       | 14.464  | 626.232 | 0.012   | 626.012 | 0.012   |
| 0.1416       | 100     | 0       | 100.012 | 0.012   | 626.312 | 0.012   | 100.012 | 0.012   | 100     | 0       | 14.464  | 626.232 | 0.012   | 626.012 | 0.012   |
| 0.15         | 100     | 0       | 100.012 | 0.012   | 626.312 | 0.012   | 100.018 | 0.018   | 100.006 | 0.006   | 14.463  | 626.232 | 0.012   | 626.012 | 0.012   |
| 0.1583       | 100     | 0       | 100.012 | 0.012   | 626.312 | 0.012   | 100.018 | 0.018   | 100.012 | 0.012   | 14.464  | 626.232 | 0.012   | 626.012 | 0.012   |
| 0.1666       | 100     | 0       | 100.019 | 0.019   | 626.319 | 0.019   | 100.018 | 0.018   | 100.006 | 0.006   | 14.464  | 626.239 | 0.019   | 626.012 | 0.012   |
| 0.175        | 100.006 | 0.006   | 100.019 | 0.019   | 626.312 | 0.012   | 100.018 | 0.018   | 100.006 | 0.006   | 14.464  | 626.232 | 0.012   | 626.012 | 0.012   |
| 0.1833       | 100.006 | 0.006   | 100.019 | 0.019   | 626.312 | 0.012   | 100.018 | 0.018   | 100.006 | 0.006   | 14.463  | 626.232 | 0.012   | 626.012 | 0.012   |
| 0.1916       | 100     | 0       | 100.012 | 0.012   | 626.312 | 0.012   | 100.018 | 0.018   | 100.006 | 0.006   | 14.464  | 626.232 | 0.012   | 626.012 | 0.012   |
| 0.2          | 100     | 0       | 100.012 | 0.012   | 626.312 | 0.012   | 100.012 | 0.012   | 100.006 | 0.006   | 14.463  | 626.232 | 0.012   | 626.012 | 0.012   |
| 0.2083       | 100     | 0       | 100.012 | 0.012   | 626.319 | 0.019   | 100.018 | 0.018   | 100.006 | 0.006   | 14.464  | 626.232 | 0.012   | 626.012 | 0.012   |
| 0.2166       | 100.006 | 0.006   | 100.019 | 0.019   | 626.312 | 0.012   | 100.018 | 0.018   | 100     | 0       | 14.464  | 626.232 | 0.012   | 626.012 | 0.012   |
| 0.225        | 100     | 0       | 100.012 | 0.012   | 626.312 | 0.012   | 100.018 | 0.018   | 100.006 | 0.006   | 14.463  | 626.232 | 0.012   | 626.012 | 0.012   |
| 0.2333       | 100     | 0       | 100.012 | 0.012   | 626.312 | 0.012   | 100.012 | 0.012   | 100.006 | 0.006   | 14.463  | 626.239 | 0.019   | 626.012 | 0.012   |
| 0.2416       | 100     | 0       | 100.012 | 0.012   | 626.319 | 0.019   | 100.012 | 0.012   | 100.006 | 0.006   | 14.465  | 626.239 | 0.019   | 626.012 | 0.012   |
| 0.25         | 100     | 0       | 100.019 | 0.019   | 626.312 | 0.012   | 100.012 | 0.012   | 100.006 | 0.006   | 14.463  | 626.232 | 0.012   | 626.012 | 0.012   |
| 0.2583       | 100     | 0       | 100.012 | 0.012   | 626.312 | 0.012   | 100.018 | 0.018   | 100.006 | 0.006   | 14.465  | 626.226 | 0.006   | 626.012 | 0.012   |
| 0.2666       | 100.006 | 0.006   | 100.012 | 0.012   | 626.312 | 0.012   | 100.018 | 0.018   | 100.006 | 0.006   | 14.464  | 626.232 | 0.012   | 626.012 | 0.012   |
| 0.275        | 100     | 0       | 100.012 | 0.012   | 626.312 | 0.012   | 100.018 | 0.018   | 100     | 0       | 14.464  | 626.232 | 0.012   | 626.012 | 0.012   |
| 0.2833       | 100     | 0       | 100.019 | 0.019   | 626.312 | 0.012   | 100.018 | 0.018   | 100.006 | 0.006   | 14.464  | 626.232 | 0.012   | 626.012 | 0.012   |
| 0.2916       | 100.006 | 0.006   | 100.019 | 0.019   | 626.319 | 0.019   | 100.018 | 0.018   | 100     | 0       | 14.463  | 626.232 | 0.012   | 626.012 | 0.012   |
| 0.3          | 100.006 | 0.006   | 100.012 | 0.012   | 626.312 | 0.012   | 100.018 | 0.018   | 100.006 | 0.006   | 14.464  | 626.239 | 0.019   | 626.012 | 0.012   |
| 0.3083       | 100     | 0       | 100.012 | 0.012   | 626.312 | 0.012   | 100.018 | 0.018   | 100.006 | 0.006   | 14.464  | 626.232 | 0.012   | 626.012 | 0.012   |
| 0.3166       | 100.006 | 0.006   | 100.012 | 0.012   | 626.312 | 0.012   | 100.018 | 0.018   | 100.006 | 0.006   | 14.464  | 626.232 | 0.012   | 626.012 | 0.012   |
| 0.325        | 100.006 | 0.006   | 100.012 | 0.012   | 626.312 | 0.012   | 100.018 | 0.018   | 100.006 | 0.006   | 14.464  | 626.232 | 0.012   | 626.012 | 0.012   |
| 0.3333       | 100     | 0       | 100.012 | 0.012   | 626.312 | 0.012   | 100.018 | 0.018   | 100     | 0       | 14.464  | 626.232 | 0.012   | 626.012 | 0.012   |
| 0.35         | 100     | 0       | 100.012 | 0.012   | 626.312 | 0.012   | 100.018 | 0.018   | 100     | 0       | 14.463  | 626.226 | 0.006   | 626.012 | 0.012   |
| 0.3666       | 100     | 0       | 100.012 | 0.012   | 626.312 | 0.012   | 100.018 | 0.018   | 100     | 0       | 14.464  | 626.232 | 0.012   | 626.012 | 0.012   |

|        | MW-6R   | MW-6R | CW-1    | CW-1  | WP-B2   | WP-B2 | WP-B10  | WP-B10 | MW-2R   | MW-2R | ATM    | MW-11I  | MW-11I | WP-B5   | WP-B5 |
|--------|---------|-------|---------|-------|---------|-------|---------|--------|---------|-------|--------|---------|--------|---------|-------|
| 0.3833 | 100     | 0     | 100.012 | 0.012 | 626.312 | 0.012 | 100.018 | 0.018  | 100     | 0     | 14.465 | 626.232 | 0.012  | 626.012 | 0.012 |
| 0.4    | 100     | 0     | 100.012 | 0.012 | 626.312 | 0.012 | 100.018 | 0.018  | 100     | 0     | 14.465 | 626.232 | 0.012  | 626.012 | 0.012 |
| 0.4166 | 100     | 0     | 100.012 | 0.012 | 626.312 | 0.012 | 100.018 | 0.018  | 100     | 0     | 14.464 | 626.232 | 0.012  | 626.012 | 0.012 |
| 0.4333 | 100     | 0     | 100.019 | 0.019 | 626.312 | 0.012 | 100.018 | 0.018  | 100     | 0     | 14.465 | 626.232 | 0.012  | 626.012 | 0.012 |
| 0.45   | 100     | 0     | 100.012 | 0.012 | 626.312 | 0.012 | 100.018 | 0.018  | 100.006 | 0.006 | 14.464 | 626.232 | 0.012  | 626.012 | 0.012 |
| 0.4666 | 100     | 0     | 100.012 | 0.012 | 626.312 | 0.012 | 100.018 | 0.018  | 100     | 0     | 14.464 | 626.232 | 0.012  | 626.012 | 0.012 |
| 0.4833 | 100     | 0     | 100.012 | 0.012 | 626.312 | 0.012 | 100.018 | 0.018  | 100     | 0     | 14.464 | 626.232 | 0.012  | 626.019 | 0.019 |
| 0.5    | 100     | 0     | 100.012 | 0.012 | 626.312 | 0.012 | 100.018 | 0.018  | 100     | 0     | 14.464 | 626.232 | 0.012  | 626.012 | 0.012 |
| 0.5166 | 100     | 0     | 100.019 | 0.019 | 626.312 | 0.012 | 100.018 | 0.018  | 100.006 | 0.006 | 14.465 | 626.232 | 0.012  | 626.012 | 0.012 |
| 0.5333 | 100     | 0     | 100.012 | 0.012 | 626.312 | 0.012 | 100.018 | 0.018  | 100     | 0     | 14.465 | 626.232 | 0.012  | 626.012 | 0.012 |
| 0.55   | 100     | 0     | 100.012 | 0.012 | 626.312 | 0.012 | 100.018 | 0.018  | 100     | 0     | 14.464 | 626.232 | 0.012  | 626.012 | 0.012 |
| 0.5666 | 100.006 | 0.006 | 100.012 | 0.012 | 626.312 | 0.012 | 100.018 | 0.018  | 100.006 | 0.006 | 14.464 | 626.232 | 0.012  | 626.012 | 0.012 |
| 0.5833 | 100.006 | 0.006 | 100.019 | 0.019 | 626.312 | 0.012 | 100.018 | 0.018  | 100.006 | 0.006 | 14.464 | 626.232 | 0.012  | 626.012 | 0.012 |
| 0.6    | 100.006 | 0.006 | 100.012 | 0.012 | 626.312 | 0.012 | 100.018 | 0.018  | 100.006 | 0.006 | 14.465 | 626.232 | 0.012  | 626.012 | 0.012 |
| 0.6166 | 100     | 0     | 100.012 | 0.012 | 626.312 | 0.012 | 100.018 | 0.018  | 100     | 0     | 14.465 | 626.232 | 0.012  | 626.012 | 0.012 |
| 0.6333 | 100.006 | 0.006 | 100.012 | 0.012 | 626.312 | 0.012 | 100.018 | 0.018  | 100.006 | 0.006 | 14.464 | 626.239 | 0.019  | 626.012 | 0.012 |
| 0.65   | 100.006 | 0.006 | 100.012 | 0.012 | 626.319 | 0.019 | 100.018 | 0.018  | 100.006 | 0.006 | 14.465 | 626.232 | 0.012  | 626.012 | 0.012 |
| 0.6666 | 100.006 | 0.006 | 100.012 | 0.012 | 626.319 | 0.019 | 100.018 | 0.018  | 100     | 0     | 14.464 | 626.239 | 0.019  | 626.019 | 0.019 |
| 0.6833 | 100     | 0     | 100.019 | 0.019 | 626.319 | 0.019 | 100.012 | 0.012  | 100.006 | 0.006 | 14.465 | 626.226 | 0.006  | 626.012 | 0.012 |
| 0.7    | 100     | 0     | 100.019 | 0.019 | 626.312 | 0.012 | 100.018 | 0.018  | 100     | 0     | 14.464 | 626.232 | 0.012  | 626.012 | 0.012 |
| 0.7166 | 100.006 | 0.006 | 100.019 | 0.019 | 626.312 | 0.012 | 100.018 | 0.018  | 100     | 0     | 14.464 | 626.232 | 0.012  | 626.012 | 0.012 |
| 0.7333 | 100.006 | 0.006 | 100.012 | 0.012 | 626.312 | 0.012 | 100.018 | 0.018  | 100     | 0     | 14.464 | 626.239 | 0.019  | 626.012 | 0.012 |
| 0.75   | 100.006 | 0.006 | 100.012 | 0.012 | 626.312 | 0.012 | 100.025 | 0.025  | 100.006 | 0.006 | 14.464 | 626.232 | 0.012  | 626.019 | 0.019 |
| 0.7666 | 100.006 | 0.006 | 100.012 | 0.012 | 626.312 | 0.012 | 100.018 | 0.018  | 100     | 0     | 14.464 | 626.232 | 0.012  | 626.012 | 0.012 |
| 0.7833 | 100.006 | 0.006 | 100.019 | 0.019 | 626.312 | 0.012 | 100.018 | 0.018  | 100.006 | 0.006 | 14.464 | 626.232 | 0.012  | 626.012 | 0.012 |
| 0.8    | 100     | 0     | 100.012 | 0.012 | 626.319 | 0.019 | 100.018 | 0.018  | 100     | 0     | 14.465 | 626.239 | 0.019  | 626.019 | 0.019 |
| 0.8166 | 100.006 | 0.006 | 100.012 | 0.012 | 626.312 | 0.012 | 100.018 | 0.018  | 100.006 | 0.006 | 14.464 | 626.232 | 0.012  | 626.012 | 0.012 |
| 0.8333 | 100.006 | 0.006 | 100.019 | 0.019 | 626.312 | 0.012 | 100.018 | 0.018  | 100.006 | 0.006 | 14.465 | 626.232 | 0.012  | 626.019 | 0.019 |
| 0.85   | 100.006 | 0.006 | 100.019 | 0.019 | 626.319 | 0.019 | 100.018 | 0.018  | 100.006 | 0.006 | 14.464 | 626.232 | 0.012  | 626.019 | 0.019 |
| 0.8666 | 100.006 | 0.006 | 100.019 | 0.019 | 626.319 | 0.019 | 100.018 | 0.018  | 100     | 0     | 14.465 | 626.232 | 0.012  | 626.019 | 0.019 |
| 0.8833 | 100.006 | 0.006 | 100.019 | 0.019 | 626.312 | 0.012 | 100.018 | 0.018  | 100     | 0     | 14.465 | 626.232 | 0.012  | 626.019 | 0.019 |
| 0.9    | 100     | 0     | 100.019 | 0.019 | 626.312 | 0.012 | 100.018 | 0.018  | 100     | 0     | 14.464 | 626.232 | 0.012  | 626.019 | 0.019 |
| 0.9166 | 100.006 | 0.006 | 100.019 | 0.019 | 626.312 | 0.012 | 100.018 | 0.018  | 100     | 0     | 14.464 | 626.232 | 0.012  | 626.012 | 0.012 |
| 0.9333 | 100.006 | 0.006 | 100.025 | 0.025 | 626.312 | 0.012 | 100.018 | 0.018  | 100.006 | 0.006 | 14.465 | 626.232 | 0.012  | 626.019 | 0.019 |
| 0.95   | 100.006 | 0.006 | 100.025 | 0.025 | 626.312 | 0.012 | 100.018 | 0.018  | 100.006 | 0.006 | 14.465 | 626.239 | 0.019  | 626.012 | 0.012 |
| 0.9666 | 100     | 0     | 100.025 | 0.025 | 626.312 | 0.012 | 100.018 | 0.018  | 100.006 | 0.006 | 14.465 | 626.239 | 0.019  | 626.019 | 0.019 |
| 0.9833 | 100.006 | 0.006 | 100.031 | 0.031 | 626.312 | 0.012 | 100.018 | 0.018  | 100     | 0     | 14.465 | 626.239 | 0.019  | 626.012 | 0.012 |
| 1      | 100     | 0     | 100.025 | 0.025 | 626.319 | 0.019 | 100.018 | 0.018  | 100     | 0     | 14.465 | 626.239 | 0.019  | 626.012 | 0.012 |
| 1.2    | 100     | 0     | 100.031 | 0.031 | 626.319 | 0.019 | 100.018 | 0.018  | 100     | 0     | 14.465 | 626.239 | 0.019  | 626.012 | 0.012 |
| 1.4    | 100     | 0     | 100.025 | 0.025 | 626.312 | 0.012 | 100.018 | 0.018  | 100.006 | 0.006 | 14.464 | 626.239 | 0.019  | 626.012 | 0.012 |
| 1.6    | 100     | 0     | 100.082 | 0.082 | 626.312 | 0.012 | 100.018 | 0.018  | 100     | 0     | 14.464 | 626.232 | 0.012  | 626.012 | 0.012 |
| 1.8    | 100     | 0     | 100.082 | 0.082 | 626.312 | 0.012 | 100.018 | 0.018  | 100     | 0     | 14.465 | 626.232 | 0.012  | 626.012 | 0.012 |
| 2      | 100.006 | 0.006 | 100.082 | 0.082 | 626.319 | 0.019 | 100.012 | 0.012  | 100     | 0     | 14.465 | 626.239 | 0.019  | 626.012 | 0.012 |
| 2.2    | 100     | 0     | 100.082 | 0.082 | 626.312 | 0.012 | 100.018 | 0.018  | 100     | 0     | 14.465 | 626.232 | 0.012  | 626.012 | 0.012 |

|     | MW-6R   | MW-6R  | CW-1    | CW-1  | WP-B2   | WP-B2 | WP-B10  | WP-B10 | MW-2R   | MW-2R  | ATM    | MW-11I  | MW-11I | WP-B5   | WP-B5 |
|-----|---------|--------|---------|-------|---------|-------|---------|--------|---------|--------|--------|---------|--------|---------|-------|
| 2.4 | 100     | 0      | 100.082 | 0.082 | 626.312 | 0.012 | 100.018 | 0.018  | 100     | 0      | 14.465 | 626.239 | 0.019  | 626.012 | 0.012 |
| 2.6 | 100     | 0      | 100.153 | 0.153 | 626.312 | 0.012 | 100.018 | 0.018  | 100.006 | 0.006  | 14.465 | 626.232 | 0.012  | 626.012 | 0.012 |
| 2.8 | 100     | 0      | 100.172 | 0.172 | 626.312 | 0.012 | 100.012 | 0.012  | 100     | 0      | 14.465 | 626.232 | 0.012  | 626.012 | 0.012 |
| 3   | 99.993  | -0.007 | 100.172 | 0.172 | 626.312 | 0.012 | 100.018 | 0.018  | 100     | 0      | 14.464 | 626.232 | 0.012  | 626.012 | 0.012 |
| 3.2 | 100     | 0      | 100.172 | 0.172 | 626.312 | 0.012 | 100.018 | 0.018  | 100     | 0      | 14.464 | 626.232 | 0.012  | 626.012 | 0.012 |
| 3.4 | 100     | 0      | 100.172 | 0.172 | 626.312 | 0.012 | 100.018 | 0.018  | 100     | 0      | 14.464 | 626.232 | 0.012  | 626.006 | 0.006 |
| 3.6 | 100     | 0      | 100.178 | 0.178 | 626.312 | 0.012 | 100.012 | 0.012  | 100     | 0      | 14.465 | 626.232 | 0.012  | 626.006 | 0.006 |
| 3.8 | 100     | 0      | 100.172 | 0.172 | 626.312 | 0.012 | 100.018 | 0.018  | 100     | 0      | 14.465 | 626.232 | 0.012  | 626.012 | 0.012 |
| 4   | 100     | 0      | 100.172 | 0.172 | 626.312 | 0.012 | 100.018 | 0.018  | 100     | 0      | 14.465 | 626.232 | 0.012  | 626.012 | 0.012 |
| 4.2 | 100     | 0      | 100.172 | 0.172 | 626.312 | 0.012 | 100.018 | 0.018  | 100     | 0      | 14.465 | 626.232 | 0.012  | 626.006 | 0.006 |
| 4.4 | 100     | 0      | 100.172 | 0.172 | 626.312 | 0.012 | 100.018 | 0.018  | 100     | 0      | 14.465 | 626.232 | 0.012  | 626.012 | 0.012 |
| 4.6 | 100     | 0      | 100.172 | 0.172 | 626.312 | 0.012 | 100.018 | 0.018  | 100     | 0      | 14.464 | 626.232 | 0.012  | 626.012 | 0.012 |
| 4.8 | 100     | 0      | 100.172 | 0.172 | 626.319 | 0.019 | 100.018 | 0.018  | 100     | 0      | 14.465 | 626.232 | 0.012  | 626.012 | 0.012 |
| 5   | 100     | 0      | 100.172 | 0.172 | 626.312 | 0.012 | 100.018 | 0.018  | 100     | 0      | 14.464 | 626.232 | 0.012  | 626.012 | 0.012 |
| 5.2 | 100     | 0      | 100.178 | 0.178 | 626.312 | 0.012 | 100.025 | 0.025  | 100     | 0      | 14.465 | 626.232 | 0.012  | 626.012 | 0.012 |
| 5.4 | 100     | 0      | 100.287 | 0.287 | 626.312 | 0.012 | 100.018 | 0.018  | 99.993  | -0.007 | 14.464 | 626.232 | 0.012  | 626.012 | 0.012 |
| 5.6 | 100.006 | 0.006  | 100.293 | 0.293 | 626.312 | 0.012 | 100.018 | 0.018  | 100.006 | 0.006  | 14.464 | 626.232 | 0.012  | 626.012 | 0.012 |
| 5.8 | 100     | 0      | 100.306 | 0.306 | 626.312 | 0.012 | 100.018 | 0.018  | 100     | 0      | 14.464 | 626.232 | 0.012  | 626.012 | 0.012 |
| 6   | 99.993  | -0.007 | 100.312 | 0.312 | 626.312 | 0.012 | 100.012 | 0.012  | 99.993  | -0.007 | 14.464 | 626.232 | 0.012  | 626.012 | 0.012 |
| 6.2 | 100     | 0      | 100.319 | 0.319 | 626.312 | 0.012 | 100.018 | 0.018  | 100     | 0      | 14.465 | 626.232 | 0.012  | 626.012 | 0.012 |
| 6.4 | 100     | 0      | 100.331 | 0.331 | 626.312 | 0.012 | 100.018 | 0.018  | 100     | 0      | 14.464 | 626.232 | 0.012  | 626.012 | 0.012 |
| 6.6 | 100     | 0      | 100.325 | 0.325 | 626.319 | 0.019 | 100.025 | 0.025  | 100     | 0      | 14.464 | 626.232 | 0.012  | 626.019 | 0.019 |
| 6.8 | 100     | 0      | 100.325 | 0.325 | 626.312 | 0.012 | 100.018 | 0.018  | 100     | 0      | 14.464 | 626.239 | 0.019  | 626.012 | 0.012 |
| 7   | 100     | 0      | 100.325 | 0.325 | 626.312 | 0.012 | 100.018 | 0.018  | 100     | 0      | 14.464 | 626.239 | 0.019  | 626.012 | 0.012 |
| 7.2 | 100     | 0      | 100.325 | 0.325 | 626.312 | 0.012 | 100.018 | 0.018  | 100     | 0      | 14.464 | 626.239 | 0.019  | 626.012 | 0.012 |
| 7.4 | 100     | 0      | 100.37  | 0.37  | 626.312 | 0.012 | 100.018 | 0.018  | 100     | 0      | 14.464 | 626.239 | 0.019  | 626.012 | 0.012 |
| 7.6 | 100     | 0      | 100.376 | 0.376 | 626.312 | 0.012 | 100.018 | 0.018  | 100     | 0      | 14.464 | 626.232 | 0.012  | 626.012 | 0.012 |
| 7.8 | 100     | 0      | 100.382 | 0.382 | 626.312 | 0.012 | 100.018 | 0.018  | 100     | 0      | 14.464 | 626.232 | 0.012  | 626.012 | 0.012 |
| 8   | 100     | 0      | 100.395 | 0.395 | 626.312 | 0.012 | 100.018 | 0.018  | 100     | 0      | 14.464 | 626.232 | 0.012  | 626.012 | 0.012 |
| 8.2 | 100     | 0      | 100.408 | 0.408 | 626.312 | 0.012 | 100.012 | 0.012  | 100.006 | 0.006  | 14.464 | 626.239 | 0.019  | 626.012 | 0.012 |
| 8.4 | 100     | 0      | 100.408 | 0.408 | 626.312 | 0.012 | 100.018 | 0.018  | 100.006 | 0.006  | 14.464 | 626.232 | 0.012  | 626.012 | 0.012 |
| 8.6 | 100     | 0      | 100.414 | 0.414 | 626.312 | 0.012 | 100.012 | 0.012  | 100     | 0      | 14.464 | 626.232 | 0.012  | 626.012 | 0.012 |
| 8.8 | 100     | 0      | 100.427 | 0.427 | 626.312 | 0.012 | 100.018 | 0.018  | 100     | 0      | 14.464 | 626.232 | 0.012  | 626.012 | 0.012 |
| 9   | 99.993  | -0.007 | 100.427 | 0.427 | 626.312 | 0.012 | 100.018 | 0.018  | 100     | 0      | 14.464 | 626.232 | 0.012  | 626.006 | 0.006 |
| 9.2 | 99.993  | -0.007 | 100.427 | 0.427 | 626.312 | 0.012 | 100.018 | 0.018  | 100     | 0      | 14.465 | 626.232 | 0.012  | 626.006 | 0.006 |
| 9.4 | 99.993  | -0.007 | 100.427 | 0.427 | 626.312 | 0.012 | 100.018 | 0.018  | 100     | 0      | 14.464 | 626.232 | 0.012  | 626.012 | 0.012 |
| 9.6 | 99.993  | -0.007 | 100.421 | 0.421 | 626.312 | 0.012 | 100.018 | 0.018  | 100     | 0      | 14.465 | 626.232 | 0.012  | 626.012 | 0.012 |
| 9.8 | 99.993  | -0.007 | 100.421 | 0.421 | 626.312 | 0.012 | 100.012 | 0.012  | 100     | 0      | 14.465 | 626.232 | 0.012  | 626.006 | 0.006 |
| 10  | 99.993  | -0.007 | 100.44  | 0.44  | 626.312 | 0.012 | 100.012 | 0.012  | 100     | 0      | 14.464 | 626.232 | 0.012  | 626.006 | 0.006 |
| 12  | 99.987  | -0.013 | 100.535 | 0.535 | 626.306 | 0.006 | 100.006 | 0.006  | 99.993  | -0.007 | 14.464 | 626.22  | 0      | 626     | 0     |
| 14  | 99.993  | -0.007 | 100.74  | 0.74  | 626.306 | 0.006 | 100.012 | 0.012  | 99.993  | -0.007 | 14.464 | 626.232 | 0.012  | 626.012 | 0.012 |
| 16  | 99.987  | -0.013 | 100.88  | 0.88  | 626.306 | 0.006 | 100.012 | 0.012  | 99.993  | -0.007 | 14.464 | 626.232 | 0.012  | 626.012 | 0.012 |
| 18  | 99.987  | -0.013 | 101.059 | 1.059 | 626.306 | 0.006 | 100.012 | 0.012  | 99.993  | -0.007 | 14.463 | 626.232 | 0.012  | 626.012 | 0.012 |
| 20  | 99.987  | -0.013 | 101.212 | 1.212 | 626.306 | 0.006 | 100.012 | 0.012  | 99.993  | -0.007 | 14.465 | 626.226 | 0.006  | 626.012 | 0.012 |

|     | MW-6R  | MW-6R  | CW-1    | CW-1  | WP-B2   | WP-B2 | WP-B10  | WP-B10 | MW-2R   | MW-2R  | ATM    | MW-11I  | MW-11I | WP-B5   | WP-B5  |
|-----|--------|--------|---------|-------|---------|-------|---------|--------|---------|--------|--------|---------|--------|---------|--------|
| 22  | 99.987 | -0.013 | 101.352 | 1.352 | 626.306 | 0.006 | 100.012 | 0.012  | 100.006 | 0.006  | 14.463 | 626.226 | 0.006  | 626.006 | 0.006  |
| 24  | 99.987 | -0.013 | 101.493 | 1.493 | 626.306 | 0.006 | 100.012 | 0.012  | 100     | 0      | 14.466 | 626.226 | 0.006  | 626.006 | 0.006  |
| 26  | 99.987 | -0.013 | 101.627 | 1.627 | 626.306 | 0.006 | 100.006 | 0.006  | 100     | 0      | 14.464 | 626.22  | 0      | 626.006 | 0.006  |
| 28  | 99.987 | -0.013 | 101.754 | 1.754 | 626.306 | 0.006 | 100.006 | 0.006  | 99.993  | -0.007 | 14.467 | 626.226 | 0.006  | 626.006 | 0.006  |
| 30  | 99.987 | -0.013 | 101.882 | 1.882 | 626.306 | 0.006 | 100.006 | 0.006  | 100     | 0      | 14.467 | 626.226 | 0.006  | 626.006 | 0.006  |
| 32  | 99.987 | -0.013 | 102.003 | 2.003 | 626.306 | 0.006 | 100.012 | 0.012  | 99.993  | -0.007 | 14.467 | 626.232 | 0.012  | 626.012 | 0.012  |
| 34  | 99.987 | -0.013 | 102.118 | 2.118 | 626.306 | 0.006 | 100.006 | 0.006  | 99.993  | -0.007 | 14.465 | 626.226 | 0.006  | 626.006 | 0.006  |
| 36  | 99.987 | -0.013 | 102.227 | 2.227 | 626.306 | 0.006 | 100.012 | 0.012  | 99.993  | -0.007 | 14.467 | 626.226 | 0.006  | 626.006 | 0.006  |
| 38  | 99.987 | -0.013 | 102.329 | 2.329 | 626.306 | 0.006 | 100.006 | 0.006  | 99.993  | -0.007 | 14.466 | 626.226 | 0.006  | 626.006 | 0.006  |
| 40  | 99.987 | -0.013 | 102.431 | 2.431 | 626.306 | 0.006 | 100.012 | 0.012  | 100     | 0      | 14.465 | 626.226 | 0.006  | 626.006 | 0.006  |
| 42  | 99.981 | -0.019 | 102.527 | 2.527 | 626.306 | 0.006 | 100.012 | 0.012  | 100     | 0      | 14.466 | 626.226 | 0.006  | 626.006 | 0.006  |
| 44  | 99.981 | -0.019 | 102.622 | 2.622 | 626.306 | 0.006 | 100.012 | 0.012  | 100     | 0      | 14.467 | 626.232 | 0.012  | 626.012 | 0.012  |
| 46  | 99.981 | -0.019 | 102.712 | 2.712 | 626.306 | 0.006 | 100.012 | 0.012  | 100     | 0      | 14.465 | 626.226 | 0.006  | 626.006 | 0.006  |
| 48  | 99.981 | -0.019 | 102.795 | 2.795 | 626.312 | 0.012 | 100.012 | 0.012  | 100     | 0      | 14.464 | 626.226 | 0.006  | 626.006 | 0.006  |
| 50  | 99.981 | -0.019 | 102.878 | 2.878 | 626.312 | 0.012 | 100.012 | 0.012  | 100     | 0      | 14.464 | 626.232 | 0.012  | 626.012 | 0.012  |
| 52  | 99.968 | -0.032 | 102.954 | 2.954 | 626.306 | 0.006 | 100.006 | 0.006  | 99.993  | -0.007 | 14.467 | 626.213 | -0.007 | 626     | 0      |
| 54  | 99.968 | -0.032 | 103.031 | 3.031 | 626.306 | 0.006 | 100.006 | 0.006  | 99.993  | -0.007 | 14.465 | 626.213 | -0.007 | 626.993 | -0.007 |
| 56  | 99.981 | -0.019 | 103.101 | 3.101 | 626.306 | 0.006 | 100.006 | 0.006  | 99.993  | -0.007 | 14.465 | 626.22  | 0      | 626     | 0      |
| 58  | 99.981 | -0.019 | 103.171 | 3.171 | 626.312 | 0.012 | 100.012 | 0.012  | 100     | 0      | 14.465 | 626.226 | 0.006  | 626.006 | 0.006  |
| 60  | 99.981 | -0.019 | 103.235 | 3.235 | 626.312 | 0.012 | 100.012 | 0.012  | 100     | 0      | 14.462 | 626.232 | 0.012  | 626.012 | 0.012  |
| 62  | 99.981 | -0.019 | 103.299 | 3.299 | 626.306 | 0.006 | 100.012 | 0.012  | 100     | 0      | 14.462 | 626.226 | 0.006  | 626.006 | 0.006  |
| 64  | 99.981 | -0.019 | 103.363 | 3.363 | 626.306 | 0.006 | 100.012 | 0.012  | 100     | 0      | 14.462 | 626.232 | 0.012  | 626.012 | 0.012  |
| 66  | 99.981 | -0.019 | 103.42  | 3.42  | 626.306 | 0.006 | 100.012 | 0.012  | 100     | 0      | 14.46  | 626.226 | 0.006  | 626.012 | 0.012  |
| 68  | 99.981 | -0.019 | 103.472 | 3.472 | 626.306 | 0.006 | 100.012 | 0.012  | 100     | 0      | 14.46  | 626.226 | 0.006  | 626.006 | 0.006  |
| 70  | 99.981 | -0.019 | 103.516 | 3.516 | 626.306 | 0.006 | 100.012 | 0.012  | 100     | 0      | 14.462 | 626.226 | 0.006  | 626.006 | 0.006  |
| 72  | 99.981 | -0.019 | 103.567 | 3.567 | 626.306 | 0.006 | 100.012 | 0.012  | 100     | 0      | 14.461 | 626.226 | 0.006  | 626.006 | 0.006  |
| 74  | 99.981 | -0.019 | 103.612 | 3.612 | 626.306 | 0.006 | 100.012 | 0.012  | 100     | 0      | 14.462 | 626.226 | 0.006  | 626.006 | 0.006  |
| 76  | 99.981 | -0.019 | 103.65  | 3.65  | 626.306 | 0.006 | 100.012 | 0.012  | 100     | 0      | 14.46  | 626.232 | 0.012  | 626.012 | 0.012  |
| 78  | 99.981 | -0.019 | 103.695 | 3.695 | 626.306 | 0.006 | 100.012 | 0.012  | 100     | 0      | 14.459 | 626.232 | 0.012  | 626.012 | 0.012  |
| 80  | 99.987 | -0.013 | 103.733 | 3.733 | 626.306 | 0.006 | 100.006 | 0.006  | 99.993  | -0.007 | 14.459 | 626.226 | 0.006  | 626.006 | 0.006  |
| 82  | 99.981 | -0.019 | 103.772 | 3.772 | 626.306 | 0.006 | 100.006 | 0.006  | 99.993  | -0.007 | 14.459 | 626.226 | 0.006  | 626.006 | 0.006  |
| 84  | 99.974 | -0.026 | 103.804 | 3.804 | 626.306 | 0.006 | 100.012 | 0.012  | 99.993  | -0.007 | 14.46  | 626.226 | 0.006  | 626.006 | 0.006  |
| 86  | 99.974 | -0.026 | 103.842 | 3.842 | 626.306 | 0.006 | 100.006 | 0.006  | 99.993  | -0.007 | 14.46  | 626.232 | 0.012  | 626.012 | 0.012  |
| 88  | 99.987 | -0.013 | 103.874 | 3.874 | 626.312 | 0.012 | 100.018 | 0.018  | 100     | 0      | 14.46  | 626.232 | 0.012  | 626.012 | 0.012  |
| 90  | 99.981 | -0.019 | 103.906 | 3.906 | 626.306 | 0.006 | 100.012 | 0.012  | 99.993  | -0.007 | 14.46  | 626.226 | 0.006  | 626.012 | 0.012  |
| 92  | 99.981 | -0.019 | 103.931 | 3.931 | 626.306 | 0.006 | 100.006 | 0.006  | 99.993  | -0.007 | 14.461 | 626.226 | 0.006  | 626.006 | 0.006  |
| 94  | 99.981 | -0.019 | 103.957 | 3.957 | 626.306 | 0.006 | 100.012 | 0.012  | 100     | 0      | 14.461 | 626.232 | 0.012  | 626.006 | 0.006  |
| 96  | 99.987 | -0.013 | 103.982 | 3.982 | 626.306 | 0.006 | 100.006 | 0.006  | 99.993  | -0.007 | 14.459 | 626.22  | 0      | 626.006 | 0.006  |
| 98  | 99.981 | -0.019 | 104.014 | 4.014 | 626.312 | 0.012 | 100.012 | 0.012  | 99.993  | -0.007 | 14.46  | 626.226 | 0.006  | 626.012 | 0.012  |
| 100 | 99.981 | -0.019 | 104.033 | 4.033 | 626.306 | 0.006 | 100.006 | 0.006  | 99.993  | -0.007 | 14.46  | 626.226 | 0.006  | 626.006 | 0.006  |
| 115 | 99.981 | -0.019 | 104.155 | 4.155 | 626.306 | 0.006 | 100.012 | 0.012  | 99.993  | -0.007 | 14.46  | 626.226 | 0.006  | 626.006 | 0.006  |
| 130 | 100    | 0      | 104.257 | 4.257 | 626.306 | 0.006 | 100.012 | 0.012  | 99.993  | -0.007 | 14.459 | 626.226 | 0.006  | 626.006 | 0.006  |
| 145 | 99.987 | -0.013 | 104.289 | 4.289 | 626.306 | 0.006 | 100.006 | 0.006  | 99.993  | -0.007 | 14.459 | 626.226 | 0.006  | 626.006 | 0.006  |
| 160 | 100    | 0      | 104.302 | 4.302 | 626.306 | 0.006 | 100.012 | 0.012  | 99.993  | -0.007 | 14.454 | 626.22  | 0      | 626.006 | 0.006  |

|     | MW-6R   | MW-6R | CW-1    | CW-1  | WP-B2   | WP-B2  | WP-B10  | WP-B10 | MW-2R  | MW-2R  | ATM    | MW-11I  | MW-11I | WP-B5   | WP-B5  |
|-----|---------|-------|---------|-------|---------|--------|---------|--------|--------|--------|--------|---------|--------|---------|--------|
| 175 | 100.006 | 0.006 | 104.302 | 4.302 | 626.306 | 0.006  | 100.012 | 0.012  | 99.987 | -0.013 | 14.455 | 626.226 | 0.006  | 626.006 | 0.006  |
| 190 | 100     | 0     | 104.308 | 4.308 | 626.306 | 0.006  | 100.018 | 0.018  | 99.993 | -0.007 | 14.45  | 626.226 | 0.006  | 626.006 | 0.006  |
| 205 | 100.012 | 0.012 | 104.327 | 4.327 | 626.306 | 0.006  | 100.018 | 0.018  | 99.993 | -0.007 | 14.445 | 626.226 | 0.006  | 626.006 | 0.006  |
| 220 | 100.006 | 0.006 | 104.346 | 4.346 | 626.306 | 0.006  | 100.012 | 0.012  | 99.987 | -0.013 | 14.444 | 626.22  | 0      | 626.006 | 0.006  |
| 235 | 100.012 | 0.012 | 104.372 | 4.372 | 626.3   | 0      | 100.012 | 0.012  | 99.987 | -0.013 | 14.448 | 626.226 | 0.006  | 626     | 0      |
| 250 | 100.018 | 0.018 | 104.397 | 4.397 | 626.3   | 0      | 100.006 | 0.006  | 99.987 | -0.013 | 14.443 | 626.22  | 0      | 626     | 0      |
| 265 | 100.018 | 0.018 | 104.429 | 4.429 | 626.3   | 0      | 100.012 | 0.012  | 99.987 | -0.013 | 14.441 | 626.213 | -0.007 | 625.993 | -0.007 |
| 280 | 100.012 | 0.012 | 104.455 | 4.455 | 626.293 | -0.007 | 100     | 0      | 99.981 | -0.019 | 14.444 | 626.213 | -0.007 | 625.987 | -0.013 |
| 295 | 100.018 | 0.018 | 104.487 | 4.487 | 626.3   | 0      | 100     | 0      | 99.981 | -0.019 | 14.442 | 626.226 | 0.006  | 626     | 0      |
| 310 | 100.018 | 0.018 | 104.525 | 4.525 | 626.3   | 0      | 100.006 | 0.006  | 99.987 | -0.013 | 14.439 | 626.226 | 0.006  | 626.006 | 0.006  |
| 325 | 100.025 | 0.025 | 104.557 | 4.557 | 626.3   | 0      | 100.006 | 0.006  | 99.981 | -0.019 | 14.434 | 626.213 | -0.007 | 626     | 0      |
| 340 | 100.025 | 0.025 | 104.595 | 4.595 | 626.306 | 0.006  | 100.006 | 0.006  | 99.987 | -0.013 | 14.43  | 626.213 | -0.007 | 626     | 0      |
| 355 | 100.025 | 0.025 | 104.627 | 4.627 | 626.3   | 0      | 100.006 | 0.006  | 99.987 | -0.013 | 14.428 | 626.226 | 0.006  | 626.012 | 0.012  |
| 370 | 100.031 | 0.031 | 104.672 | 4.672 | 626.3   | 0      | 100.006 | 0.006  | 99.981 | -0.019 | 14.427 | 626.22  | 0      | 626     | 0      |
| 385 | 100.025 | 0.025 | 104.71  | 4.71  | 626.3   | 0      | 100     | 0      | 99.981 | -0.019 | 14.424 | 626.213 | -0.007 | 625.993 | -0.007 |
| 400 | 100.031 | 0.031 | 104.749 | 4.749 | 626.3   | 0      | 100.006 | 0.006  | 99.981 | -0.019 | 14.421 | 626.22  | 0      | 625.993 | -0.007 |
| 415 | 100.037 | 0.037 | 104.787 | 4.787 | 626.3   | 0      | 100     | 0      | 99.981 | -0.019 | 14.419 | 626.213 | -0.007 | 625.993 | -0.007 |
| 430 | 100.025 | 0.025 | 104.832 | 4.832 | 626.293 | -0.007 | 100.006 | 0.006  | 99.974 | -0.026 | 14.418 | 626.213 | -0.007 | 625.987 | -0.013 |
| 445 | 100.031 | 0.031 | 104.876 | 4.876 | 626.3   | 0      | 100.006 | 0.006  | 99.981 | -0.019 | 14.414 | 626.226 | 0.006  | 626.006 | 0.006  |
| 460 | 100.031 | 0.031 | 104.915 | 4.915 | 626.293 | -0.007 | 100.006 | 0.006  | 99.974 | -0.026 | 14.412 | 626.22  | 0      | 625.993 | -0.007 |
| 475 | 100.018 | 0.018 | 104.953 | 4.953 | 626.293 | -0.007 | 100     | 0      | 99.974 | -0.026 | 14.411 | 626.22  | 0      | 625.993 | -0.007 |
| 490 | 100.025 | 0.025 | 104.991 | 4.991 | 626.293 | -0.007 | 100.006 | 0.006  | 99.981 | -0.019 | 14.408 | 626.22  | 0      | 625.993 | -0.007 |
| 505 | 100.025 | 0.025 | 105.023 | 5.023 | 626.293 | -0.007 | 100     | 0      | 99.974 | -0.026 | 14.406 | 626.213 | -0.007 | 625.987 | -0.013 |
| 520 | 100.025 | 0.025 | 105.055 | 5.055 | 626.293 | -0.007 | 100     | 0      | 99.974 | -0.026 | 14.406 | 626.213 | -0.007 | 625.987 | -0.013 |
| 535 | 100.031 | 0.031 | 105.087 | 5.087 | 626.293 | -0.007 | 100     | 0      | 99.974 | -0.026 | 14.402 | 626.213 | -0.007 | 625.993 | -0.007 |
| 550 | 100.031 | 0.031 | 105.113 | 5.113 | 626.293 | -0.007 | 100     | 0      | 99.974 | -0.026 | 14.401 | 626.22  | 0      | 625.993 | -0.007 |
| 565 | 100.031 | 0.031 | 105.145 | 5.145 | 626.287 | -0.013 | 99.993  | -0.007 | 99.974 | -0.026 | 14.401 | 626.213 | -0.007 | 625.987 | -0.013 |
| 580 | 100.037 | 0.037 | 105.17  | 5.17  | 626.287 | -0.013 | 99.993  | -0.007 | 99.974 | -0.026 | 14.402 | 626.213 | -0.007 | 625.987 | -0.013 |
| 595 | 100.031 | 0.031 | 105.202 | 5.202 | 626.287 | -0.013 | 99.993  | -0.007 | 99.974 | -0.026 | 14.4   | 626.213 | -0.007 | 625.987 | -0.013 |
| 610 | 100.025 | 0.025 | 105.228 | 5.228 | 626.287 | -0.013 | 99.993  | -0.007 | 99.974 | -0.026 | 14.397 | 626.213 | -0.007 | 625.987 | -0.013 |
| 625 | 100.031 | 0.031 | 105.253 | 5.253 | 626.287 | -0.013 | 99.993  | -0.007 | 99.974 | -0.026 | 14.397 | 626.213 | -0.007 | 625.987 | -0.013 |
| 640 | 100.037 | 0.037 | 105.291 | 5.291 | 626.287 | -0.013 | 99.993  | -0.007 | 99.974 | -0.026 | 14.395 | 626.213 | -0.007 | 625.987 | -0.013 |
| 655 | 100.031 | 0.031 | 105.317 | 5.317 | 626.287 | -0.013 | 99.993  | -0.007 | 99.974 | -0.026 | 14.395 | 626.207 | -0.013 | 625.987 | -0.013 |
| 670 | 100.037 | 0.037 | 105.349 | 5.349 | 626.287 | -0.013 | 99.987  | -0.013 | 99.974 | -0.026 | 14.393 | 626.213 | -0.007 | 625.987 | -0.013 |
| 685 | 100.031 | 0.031 | 105.381 | 5.381 | 626.28  | -0.02  | 99.987  | -0.013 | 99.968 | -0.032 | 14.395 | 626.207 | -0.013 | 625.981 | -0.019 |
| 700 | 100.025 | 0.025 | 105.336 | 5.336 | 626.28  | -0.02  | 99.987  | -0.013 | 99.968 | -0.032 | 14.393 | 626.207 | -0.013 | 625.981 | -0.019 |
| 715 | 100.031 | 0.031 | 105.458 | 5.458 | 626.28  | -0.02  | 99.987  | -0.013 | 99.968 | -0.032 | 14.395 | 626.207 | -0.013 | 625.981 | -0.019 |
| 730 | 100.025 | 0.025 | 105.496 | 5.496 | 626.28  | -0.02  | 99.987  | -0.013 | 99.974 | -0.026 | 14.39  | 626.213 | -0.007 | 625.987 | -0.013 |
| 745 | 100.031 | 0.031 | 105.4   | 5.4   | 626.287 | -0.013 | 99.987  | -0.013 | 99.974 | -0.026 | 14.39  | 626.213 | -0.007 | 625.981 | -0.019 |
| 760 | 100.031 | 0.031 | 105.33  | 5.33  | 626.28  | -0.02  | 99.987  | -0.013 | 99.974 | -0.026 | 14.388 | 626.213 | -0.007 | 625.987 | -0.013 |
| 775 | 100.037 | 0.037 | 105.4   | 5.4   | 626.28  | -0.02  | 99.987  | -0.013 | 99.974 | -0.026 | 14.387 | 626.213 | -0.007 | 625.981 | -0.019 |
| 790 | 100.037 | 0.037 | 105.406 | 5.406 | 626.28  | -0.02  | 99.987  | -0.013 | 99.974 | -0.026 | 14.387 | 626.207 | -0.013 | 625.981 | -0.019 |
| 805 | 100.037 | 0.037 | 105.515 | 5.515 | 626.274 | -0.026 | 99.987  | -0.013 | 99.974 | -0.026 | 14.386 | 626.207 | -0.013 | 625.981 | -0.019 |
| 820 | 100.031 | 0.031 | 105.598 | 5.598 | 626.28  | -0.02  | 99.987  | -0.013 | 99.974 | -0.026 | 14.384 | 626.207 | -0.013 | 625.981 | -0.019 |

|      | MW-6R   | MW-6R | CW-1    | CW-1  | WP-B2   | WP-B2  | WP-B10  | WP-B10 | MW-2R   | MW-2R  | ATM    | MW-11I  | MW-11I | WP-B5   | WP-B5  |
|------|---------|-------|---------|-------|---------|--------|---------|--------|---------|--------|--------|---------|--------|---------|--------|
| 835  | 100.037 | 0.037 | 105.668 | 5.668 | 626.261 | -0.039 | 99.987  | -0.013 | 99.974  | -0.026 | 14.385 | 626.207 | -0.013 | 625.981 | -0.019 |
| 850  | 100.037 | 0.037 | 105.713 | 5.713 | 626.28  | -0.02  | 99.987  | -0.013 | 99.974  | -0.026 | 14.384 | 626.207 | -0.013 | 625.981 | -0.019 |
| 865  | 100.044 | 0.044 | 105.751 | 5.751 | 626.287 | -0.013 | 99.987  | -0.013 | 99.974  | -0.026 | 14.38  | 626.213 | -0.007 | 625.981 | -0.019 |
| 880  | 100.05  | 0.05  | 105.783 | 5.783 | 626.287 | -0.013 | 99.993  | -0.007 | 99.981  | -0.019 | 14.375 | 626.207 | -0.013 | 625.987 | -0.013 |
| 895  | 100.05  | 0.05  | 105.822 | 5.822 | 626.293 | -0.007 | 100     | 0      | 99.981  | -0.019 | 14.368 | 626.22  | 0      | 625.987 | -0.013 |
| 910  | 100.044 | 0.044 | 105.847 | 5.847 | 626.287 | -0.013 | 99.993  | -0.007 | 99.981  | -0.019 | 14.366 | 626.213 | -0.007 | 625.987 | -0.013 |
| 925  | 100.056 | 0.056 | 105.879 | 5.879 | 626.287 | -0.013 | 99.993  | -0.007 | 99.981  | -0.019 | 14.365 | 626.213 | -0.007 | 625.987 | -0.013 |
| 940  | 100.062 | 0.062 | 105.905 | 5.905 | 626.287 | -0.013 | 99.993  | -0.007 | 99.981  | -0.019 | 14.363 | 626.213 | -0.007 | 625.981 | -0.019 |
| 955  | 100.062 | 0.062 | 105.93  | 5.93  | 626.28  | -0.02  | 99.993  | -0.007 | 99.981  | -0.019 | 14.359 | 626.213 | -0.007 | 625.987 | -0.013 |
| 970  | 100.062 | 0.062 | 105.956 | 5.956 | 626.287 | -0.013 | 99.993  | -0.007 | 99.987  | -0.013 | 14.357 | 626.22  | 0      | 625.987 | -0.013 |
| 985  | 100.069 | 0.069 | 105.988 | 5.988 | 626.287 | -0.013 | 100     | 0      | 99.987  | -0.013 | 14.352 | 626.213 | -0.007 | 625.987 | -0.013 |
| 1000 | 100.062 | 0.062 | 106.007 | 6.007 | 626.287 | -0.013 | 99.993  | -0.007 | 99.987  | -0.013 | 14.349 | 626.213 | -0.007 | 625.987 | -0.013 |
| 1015 | 100.062 | 0.062 | 106.039 | 6.039 | 626.28  | -0.02  | 99.987  | -0.013 | 99.987  | -0.013 | 14.347 | 626.213 | -0.007 | 625.981 | -0.019 |
| 1030 | 100.062 | 0.062 | 106.058 | 6.058 | 626.287 | -0.013 | 99.993  | -0.007 | 99.987  | -0.013 | 14.344 | 626.213 | -0.007 | 625.981 | -0.019 |
| 1045 | 100.069 | 0.069 | 106.083 | 6.083 | 626.287 | -0.013 | 99.993  | -0.007 | 99.987  | -0.013 | 14.34  | 626.213 | -0.007 | 625.987 | -0.013 |
| 1060 | 100.075 | 0.075 | 106.103 | 6.103 | 626.293 | -0.007 | 100     | 0      | 99.987  | -0.013 | 14.335 | 626.213 | -0.007 | 625.987 | -0.013 |
| 1075 | 100.075 | 0.075 | 106.122 | 6.122 | 626.287 | -0.013 | 100     | 0      | 99.993  | -0.007 | 14.332 | 626.213 | -0.007 | 625.987 | -0.013 |
| 1090 | 100.081 | 0.081 | 106.135 | 6.135 | 626.287 | -0.013 | 100     | 0      | 99.993  | -0.007 | 14.326 | 626.22  | 0      | 625.987 | -0.013 |
| 1105 | 100.094 | 0.094 | 106.154 | 6.154 | 626.287 | -0.013 | 100     | 0      | 99.993  | -0.007 | 14.324 | 626.213 | -0.007 | 625.987 | -0.013 |
| 1120 | 100.094 | 0.094 | 106.173 | 6.173 | 626.287 | -0.013 | 99.993  | -0.007 | 99.987  | -0.013 | 14.322 | 626.213 | -0.007 | 625.987 | -0.013 |
| 1135 | 100.1   | 0.1   | 106.186 | 6.186 | 626.287 | -0.013 | 99.993  | -0.007 | 99.993  | -0.007 | 14.317 | 626.213 | -0.007 | 625.987 | -0.013 |
| 1150 | 100.094 | 0.094 | 106.198 | 6.198 | 626.287 | -0.013 | 99.993  | -0.007 | 99.987  | -0.013 | 14.316 | 626.213 | -0.007 | 625.981 | -0.019 |
| 1165 | 100.088 | 0.088 | 106.211 | 6.211 | 626.28  | -0.02  | 99.993  | -0.007 | 99.987  | -0.013 | 14.315 | 626.213 | -0.007 | 625.981 | -0.019 |
| 1180 | 100.1   | 0.1   | 106.237 | 6.237 | 626.28  | -0.02  | 99.987  | -0.013 | 99.987  | -0.013 | 14.315 | 626.213 | -0.007 | 625.981 | -0.019 |
| 1195 | 100.106 | 0.106 | 106.256 | 6.256 | 626.287 | -0.013 | 99.987  | -0.013 | 99.987  | -0.013 | 14.31  | 626.213 | -0.007 | 625.981 | -0.019 |
| 1210 | 100.1   | 0.1   | 106.275 | 6.275 | 626.287 | -0.013 | 99.987  | -0.013 | 99.987  | -0.013 | 14.31  | 626.207 | -0.013 | 625.981 | -0.019 |
| 1225 | 100.106 | 0.106 | 106.294 | 6.294 | 626.287 | -0.013 | 99.987  | -0.013 | 99.993  | -0.007 | 14.305 | 626.213 | -0.007 | 625.981 | -0.019 |
| 1240 | 100.106 | 0.106 | 106.218 | 6.218 | 626.287 | -0.013 | 99.993  | -0.007 | 99.993  | -0.007 | 14.3   | 626.213 | -0.007 | 625.987 | -0.013 |
| 1255 | 100.106 | 0.106 | 106.103 | 6.103 | 626.287 | -0.013 | 100     | 0      | 99.993  | -0.007 | 14.294 | 626.213 | -0.007 | 625.987 | -0.013 |
| 1270 | 100.094 | 0.094 | 106.02  | 6.02  | 626.28  | -0.02  | 99.993  | -0.007 | 99.987  | -0.013 | 14.292 | 626.22  | 0      | 625.981 | -0.019 |
| 1285 | 100.088 | 0.088 | 105.962 | 5.962 | 626.28  | -0.02  | 99.987  | -0.013 | 99.987  | -0.013 | 14.294 | 626.207 | -0.013 | 625.981 | -0.019 |
| 1300 | 100.094 | 0.094 | 105.917 | 5.917 | 626.28  | -0.02  | 99.981  | -0.019 | 99.987  | -0.013 | 14.293 | 626.207 | -0.013 | 625.974 | -0.026 |
| 1315 | 100.088 | 0.088 | 105.898 | 5.898 | 626.28  | -0.02  | 99.981  | -0.019 | 99.981  | -0.019 | 14.293 | 626.207 | -0.013 | 625.974 | -0.026 |
| 1330 | 100.094 | 0.094 | 105.885 | 5.885 | 626.274 | -0.026 | 99.981  | -0.019 | 99.981  | -0.019 | 14.293 | 626.207 | -0.013 | 625.974 | -0.026 |
| 1345 | 100.088 | 0.088 | 105.885 | 5.885 | 626.274 | -0.026 | 99.974  | -0.026 | 99.981  | -0.019 | 14.294 | 626.27  | 0.05   | 625.968 | -0.032 |
| 1360 | 100.081 | 0.081 | 105.898 | 5.898 | 626.268 | -0.032 | 99.974  | -0.026 | 99.981  | -0.019 | 14.292 | 626.2   | -0.02  | 625.968 | -0.032 |
| 1375 | 100.088 | 0.088 | 105.917 | 5.917 | 626.274 | -0.026 | 99.981  | -0.019 | 99.981  | -0.019 | 14.291 | 626.207 | -0.013 | 625.974 | -0.026 |
| 1390 | 100.088 | 0.088 | 105.937 | 5.937 | 626.268 | -0.032 | 99.974  | -0.026 | 99.974  | -0.026 | 14.294 | 626.2   | -0.02  | 625.968 | -0.032 |
| 1405 | 100.081 | 0.081 | 105.956 | 5.956 | 626.268 | -0.032 | 99.968  | -0.032 | 99.974  | -0.026 | 14.292 | 626.2   | -0.02  | 625.968 | -0.032 |
| 1420 | 100.081 | 0.081 | 105.975 | 5.975 | 626.261 | -0.039 | 99.968  | -0.032 | 99.974  | -0.026 | 14.294 | 626.2   | -0.02  | 625.968 | -0.032 |
| 1435 | 100.081 | 0.081 | 105.994 | 5.994 | 626.274 | -0.026 | 99.974  | -0.026 | 99.981  | -0.019 | 14.289 | 626.2   | -0.02  | 625.968 | -0.032 |
| 1450 | 100.1   | 0.1   | 106.026 | 6.026 | 626.287 | -0.013 | 99.993  | -0.007 | 99.993  | -0.007 | 14.272 | 626.22  | 0      | 625.987 | -0.013 |
| 1465 | 100.125 | 0.125 | 106.058 | 6.058 | 626.312 | 0.012  | 100.018 | 0.018  | 100.012 | 0.012  | 14.25  | 626.239 | 0.019  | 626     | 0      |
| 1480 | 100.119 | 0.119 | 106.083 | 6.083 | 626.293 | -0.007 | 100.006 | 0.006  | 100     | 0      | 14.252 | 626.22  | 0      | 625.987 | -0.013 |

|      | MW-6R   | MW-6R | CW-1    | CW-1  | WP-B2   | WP-B2  | WP-B10 | WP-B10 | MW-2R  | MW-2R  | ATM    | MW-11I  | MW-11I | WP-B5   | WP-B5  |
|------|---------|-------|---------|-------|---------|--------|--------|--------|--------|--------|--------|---------|--------|---------|--------|
| 1495 | 100.119 | 0.119 | 106.109 | 6.109 | 626.293 | -0.007 | 100    | 0      | 100    | 0      | 14.244 | 626.22  | 0      | 625.983 | -0.007 |
| 1510 | 100.113 | 0.113 | 106.141 | 6.141 | 626.293 | -0.007 | 100    | 0      | 100    | 0      | 14.241 | 626.22  | 0      | 625.981 | -0.019 |
| 1525 | 100.113 | 0.113 | 106.173 | 6.173 | 626.293 | -0.007 | 100    | 0      | 100    | 0      | 14.239 | 626.213 | -0.007 | 625.981 | -0.019 |
| 1540 | 100.113 | 0.113 | 105.911 | 5.911 | 626.28  | -0.02  | 99.987 | -0.013 | 99.993 | -0.007 | 14.24  | 626.207 | -0.013 | 625.974 | -0.026 |
| 1555 | 100.113 | 0.113 | 104.889 | 4.889 | 626.287 | -0.013 | 99.993 | -0.007 | 99.993 | -0.007 | 14.234 | 626.2   | -0.02  | 625.974 | -0.026 |
| 1570 | 100.113 | 0.113 | 104.078 | 4.078 | 626.287 | -0.013 | 99.993 | -0.007 | 100    | 0      | 14.232 | 626.213 | -0.007 | 625.987 | -0.013 |
| 1585 | 100.106 | 0.106 | 103.414 | 3.414 | 626.274 | -0.026 | 99.987 | -0.013 | 99.987 | -0.013 | 14.228 | 626.194 | -0.026 | 625.968 | -0.032 |
| 1600 | 100.106 | 0.106 | 102.897 | 2.897 | 626.28  | -0.02  | 99.993 | -0.007 | 99.993 | -0.007 | 14.226 | 626.207 | -0.013 | 625.981 | -0.019 |
| 1615 | 100.106 | 0.106 | 102.469 | 2.469 | 626.287 | -0.013 | 99.993 | -0.007 | 99.987 | -0.013 | 14.221 | 626.207 | -0.013 | 625.981 | -0.019 |
| 1630 | 100.1   | 0.1   | 102.125 | 2.125 | 626.274 | -0.026 | 99.981 | -0.019 | 99.981 | -0.019 | 14.217 | 626.2   | -0.02  | 625.974 | -0.026 |
| 1645 | 100.1   | 0.1   | 101.85  | 1.85  | 626.268 | -0.032 | 99.981 | -0.019 | 99.955 | -0.045 | 14.216 | 626.188 | -0.032 | 625.955 | -0.045 |
| 1660 | 100.125 | 0.125 | 101.627 | 1.627 | 626.274 | -0.026 | 99.987 | -0.013 | 99.968 | -0.032 | 14.21  | 626.207 | -0.013 | 625.981 | -0.019 |

| Date     | Time     | ET (min) | Meters H2O | Celsius |
|----------|----------|----------|------------|---------|
| 07/18/96 | 8:28:52  | 0        | 190.962    | 13.44   |
| 07/18/96 | 8:43:52  | 15       | 190.964    | 12.74   |
| 07/18/96 | 8:58:52  | 30       | 190.964    | 12.7    |
| 07/18/96 | 9:13:52  | 45       | 190.964    | 12.7    |
| 07/18/96 | 9:28:52  | 60       | 190.964    | 12.7    |
| 07/18/96 | 9:43:52  | 75       | 190.964    | 12.7    |
| 07/18/96 | 9:58:52  | 90       | 190.964    | 12.7    |
| 07/18/96 | 10:13:52 | 105      | 190.963    | 12.7    |
| 07/18/96 | 10:28:52 | 120      | 190.963    | 12.7    |
| 07/18/96 | 10:43:52 | 135      | 190.962    | 12.7    |
| 07/18/96 | 10:58:52 | 150      | 190.963    | 12.7    |
| 07/18/96 | 11:13:52 | 165      | 190.962    | 12.7    |
| 07/18/96 | 11:28:52 | 180      | 190.963    | 12.7    |
| 07/18/96 | 11:43:52 | 195      | 190.963    | 12.7    |
| 07/18/96 | 11:58:52 | 210      | 190.963    | 12.69   |
| 07/18/96 | 12:13:52 | 225      | 190.963    | 12.7    |
| 07/18/96 | 12:28:52 | 240      | 190.963    | 12.7    |
| 07/18/96 | 12:43:52 | 255      | 190.962    | 12.7    |
| 07/18/96 | 12:58:52 | 270      | 190.961    | 12.7    |
| 07/18/96 | 13:13:52 | 285      | 190.961    | 12.7    |
| 07/18/96 | 13:28:52 | 300      | 190.96     | 12.7    |
| 07/18/96 | 13:43:52 | 315      | 190.96     | 12.7    |
| 07/18/96 | 13:58:52 | 330      | 190.96     | 12.7    |
| 07/18/96 | 14:13:52 | 345      | 190.96     | 12.7    |
| 07/18/96 | 14:28:52 | 360      | 190.961    | 12.7    |
| 07/18/96 | 14:43:52 | 375      | 190.96     | 12.7    |
| 07/18/96 | 14:58:52 | 390      | 190.959    | 12.7    |
| 07/18/96 | 15:13:52 | 405      | 190.959    | 12.7    |
| 07/18/96 | 15:28:52 | 420      | 190.959    | 12.7    |
| 07/18/96 | 15:43:52 | 435      | 190.959    | 12.7    |
| 07/18/96 | 15:58:52 | 450      | 190.959    | 12.7    |
| 07/18/96 | 16:13:52 | 465      | 190.958    | 12.7    |
| 07/18/96 | 16:28:52 | 480      | 190.958    | 12.7    |
| 07/18/96 | 16:43:52 | 495      | 190.958    | 12.7    |
| 07/18/96 | 16:58:52 | 510      | 190.958    | 12.7    |
| 07/18/96 | 17:13:52 | 525      | 190.959    | 12.71   |
| 07/18/96 | 17:28:52 | 540      | 190.958    | 12.7    |
| 07/18/96 | 17:43:52 | 555      | 190.957    | 12.7    |
| 07/18/96 | 17:58:52 | 570      | 190.957    | 12.7    |
| 07/18/96 | 18:13:52 | 585      | 190.957    | 12.71   |
| 07/18/96 | 18:28:52 | 600      | 190.957    | 12.7    |
| 07/18/96 | 18:43:52 | 615      | 190.956    | 12.71   |
| 07/18/96 | 18:58:52 | 630      | 190.957    | 12.71   |
| 07/18/96 | 19:13:52 | 645      | 190.956    | 12.71   |
| 07/18/96 | 19:28:52 | 660      | 190.957    | 12.7    |
| 07/18/96 | 19:43:52 | 675      | 190.957    | 12.7    |
| 07/18/96 | 19:58:52 | 690      | 190.957    | 12.7    |
| 07/18/96 | 20:13:52 | 705      | 190.957    | 12.71   |
| 07/18/96 | 20:28:52 | 720      | 190.956    | 12.71   |

| Date     | Time     | ET (min) | Meters H2O | Celsius |
|----------|----------|----------|------------|---------|
| 07/18/96 | 20:43:52 | 735      | 190.955    | 12.71   |
| 07/18/96 | 20:58:52 | 750      | 190.954    | 12.7    |
| 07/18/96 | 21:13:52 | 765      | 190.955    | 12.71   |
| 07/18/96 | 21:28:52 | 780      | 190.956    | 12.71   |
| 07/18/96 | 21:43:52 | 795      | 190.956    | 12.7    |
| 07/18/96 | 21:58:52 | 810      | 190.956    | 12.71   |
| 07/18/96 | 22:13:52 | 825      | 190.955    | 12.71   |
| 07/18/96 | 22:28:52 | 840      | 190.954    | 12.71   |
| 07/18/96 | 22:43:52 | 855      | 190.954    | 12.71   |
| 07/18/96 | 22:58:52 | 870      | 190.954    | 12.71   |
| 07/18/96 | 23:13:52 | 885      | 190.954    | 12.71   |
| 07/18/96 | 23:28:52 | 900      | 190.955    | 12.71   |
| 07/18/96 | 23:43:52 | 915      | 190.957    | 12.71   |
| 07/18/96 | 23:58:52 | 930      | 190.957    | 12.71   |
| 07/19/96 | 0:13:52  | 945      | 190.955    | 12.71   |
| 07/19/96 | 0:28:52  | 960      | 190.956    | 12.71   |
| 07/19/96 | 0:43:52  | 975      | 190.955    | 12.71   |
| 07/19/96 | 0:58:52  | 990      | 190.955    | 12.71   |
| 07/19/96 | 1:13:52  | 1005     | 190.957    | 12.71   |
| 07/19/96 | 1:28:52  | 1020     | 190.956    | 12.71   |
| 07/19/96 | 1:43:52  | 1035     | 190.955    | 12.71   |
| 07/19/96 | 1:58:52  | 1050     | 190.955    | 12.71   |
| 07/19/96 | 2:13:52  | 1065     | 190.956    | 12.71   |
| 07/19/96 | 2:28:52  | 1080     | 190.956    | 12.71   |
| 07/19/96 | 2:43:52  | 1095     | 190.957    | 12.71   |
| 07/19/96 | 2:58:52  | 1110     | 190.957    | 12.71   |
| 07/19/96 | 3:13:52  | 1125     | 190.957    | 12.71   |
| 07/19/96 | 3:28:52  | 1140     | 190.956    | 12.71   |
| 07/19/96 | 3:43:52  | 1155     | 190.955    | 12.71   |
| 07/19/96 | 3:58:52  | 1170     | 190.955    | 12.71   |
| 07/19/96 | 4:13:52  | 1185     | 190.954    | 12.71   |
| 07/19/96 | 4:28:52  | 1200     | 190.954    | 12.71   |
| 07/19/96 | 4:43:52  | 1215     | 190.954    | 12.71   |
| 07/19/96 | 4:58:52  | 1230     | 190.954    | 12.71   |
| 07/19/96 | 5:13:52  | 1245     | 190.955    | 12.71   |
| 07/19/96 | 5:28:52  | 1260     | 190.955    | 12.71   |
| 07/19/96 | 5:43:52  | 1275     | 190.957    | 12.71   |
| 07/19/96 | 5:58:52  | 1290     | 190.957    | 12.71   |
| 07/19/96 | 6:13:52  | 1305     | 190.954    | 12.71   |
| 07/19/96 | 6:28:52  | 1320     | 190.954    | 12.71   |
| 07/19/96 | 6:43:52  | 1335     | 190.954    | 12.71   |
| 07/19/96 | 6:58:52  | 1350     | 190.952    | 12.71   |
| 07/19/96 | 7:13:52  | 1365     | 190.952    | 12.71   |
| 07/19/96 | 7:28:52  | 1380     | 190.951    | 12.71   |
| 07/19/96 | 7:43:52  | 1395     | 190.952    | 12.71   |
| 07/19/96 | 7:58:52  | 1410     | 190.95     | 12.71   |
| 07/19/96 | 8:13:52  | 1425     | 190.95     | 12.71   |
| 07/19/96 | 8:28:52  | 1440     | 190.949    | 12.71   |
| 07/19/96 | 8:43:52  | 1455     | 190.95     | 12.71   |
| 07/19/96 | 8:58:52  | 1470     | 190.955    | 12.71   |

| Date     | Time     | ET (min) | Meters H2O | Celsius |
|----------|----------|----------|------------|---------|
| 07/19/96 | 9:13:52  | 1485     | 190.949    | 12.71   |
| 07/19/96 | 9:28:52  | 1500     | 190.944    | 12.71   |
| 07/19/96 | 9:43:52  | 1515     | 190.958    | 12.71   |
| 07/19/96 | 9:58:52  | 1530     | 190.957    | 12.71   |
| 07/19/96 | 10:13:52 | 1545     | 190.956    | 12.71   |
| 07/19/96 | 10:28:52 | 1560     | 190.954    | 12.71   |
| 07/19/96 | 10:43:52 | 1575     | 190.954    | 12.71   |
| 07/19/96 | 10:58:52 | 1590     | 190.953    | 12.71   |
| 07/19/96 | 11:13:52 | 1605     | 190.954    | 12.71   |
| 07/19/96 | 11:28:52 | 1620     | 190.952    | 12.71   |
| 07/19/96 | 11:43:52 | 1635     | 190.952    | 12.71   |
| 07/19/96 | 11:58:52 | 1650     | 190.954    | 12.71   |
| 07/19/96 | 12:13:52 | 1665     | 190.953    | 12.71   |
| 07/19/96 | 12:28:52 | 1680     | 190.952    | 12.71   |
| 07/19/96 | 12:43:52 | 1695     | 190.952    | 12.71   |
| 07/19/96 | 12:58:52 | 1710     | 190.951    | 12.71   |
| 07/19/96 | 13:13:52 | 1725     | 190.95     | 12.71   |
| 07/19/96 | 13:28:52 | 1740     | 190.95     | 12.71   |

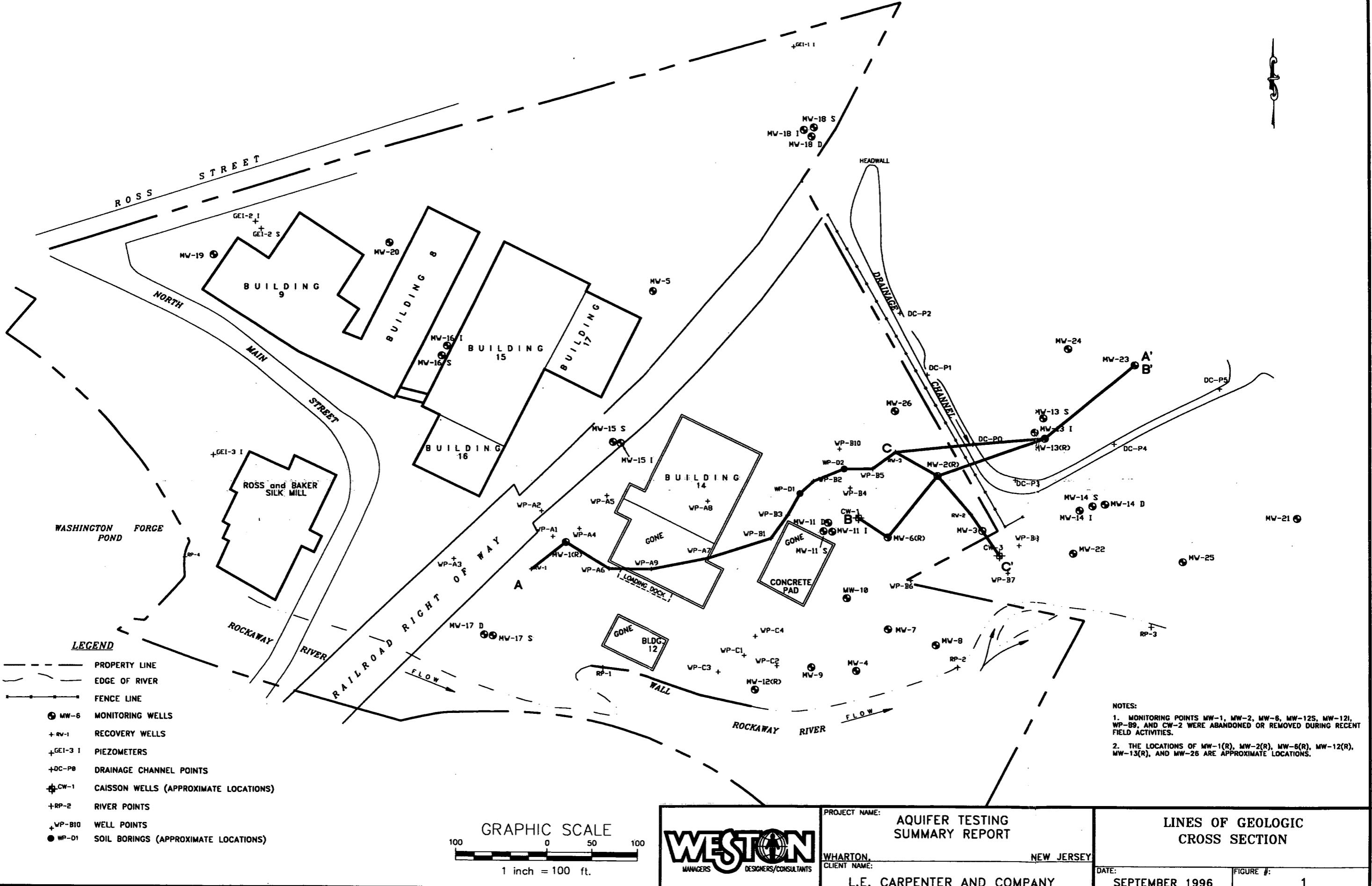
| Date     | Time     | ET (min) | Meters H2O | Celsius |
|----------|----------|----------|------------|---------|
| 07/18/96 | 8:13:38  | 0        | 191.076    | 16.15   |
| 07/18/96 | 8:28:38  | 15       | 191.078    | 15.82   |
| 07/18/96 | 8:43:38  | 30       | 191.078    | 15.8    |
| 07/18/96 | 8:58:38  | 45       | 191.078    | 15.8    |
| 07/18/96 | 9:13:38  | 60       | 191.077    | 15.8    |
| 07/18/96 | 9:28:38  | 75       | 191.077    | 15.8    |
| 07/18/96 | 9:43:38  | 90       | 191.077    | 15.8    |
| 07/18/96 | 9:58:38  | 105      | 191.077    | 15.8    |
| 07/18/96 | 10:13:38 | 120      | 191.076    | 15.8    |
| 07/18/96 | 10:28:38 | 135      | 191.074    | 15.8    |
| 07/18/96 | 10:43:38 | 150      | 191.074    | 15.81   |
| 07/18/96 | 10:58:38 | 165      | 191.074    | 15.81   |
| 07/18/96 | 11:13:38 | 180      | 191.073    | 15.81   |
| 07/18/96 | 11:28:38 | 195      | 191.073    | 15.81   |
| 07/18/96 | 11:43:38 | 210      | 191.073    | 15.81   |
| 07/18/96 | 11:58:38 | 225      | 191.073    | 15.81   |
| 07/18/96 | 12:13:38 | 240      | 191.072    | 15.81   |
| 07/18/96 | 12:28:38 | 255      | 191.072    | 15.81   |
| 07/18/96 | 12:43:38 | 270      | 191.071    | 15.81   |
| 07/18/96 | 12:58:38 | 285      | 191.071    | 15.81   |
| 07/18/96 | 13:13:38 | 300      | 191.071    | 15.81   |
| 07/18/96 | 13:28:38 | 315      | 191.069    | 15.81   |
| 07/18/96 | 13:43:38 | 330      | 191.068    | 15.81   |
| 07/18/96 | 13:58:38 | 345      | 191.068    | 15.81   |
| 07/18/96 | 14:13:38 | 360      | 191.068    | 15.81   |
| 07/18/96 | 14:28:38 | 375      | 191.068    | 15.81   |
| 07/18/96 | 14:43:38 | 390      | 191.068    | 15.81   |
| 07/18/96 | 14:58:38 | 405      | 191.066    | 15.81   |
| 07/18/96 | 15:13:38 | 420      | 191.066    | 15.81   |
| 07/18/96 | 15:28:38 | 435      | 191.065    | 15.81   |
| 07/18/96 | 15:43:38 | 450      | 191.065    | 15.81   |
| 07/18/96 | 15:58:38 | 465      | 191.065    | 15.81   |
| 07/18/96 | 16:13:38 | 480      | 191.064    | 15.81   |
| 07/18/96 | 16:28:38 | 495      | 191.064    | 15.81   |
| 07/18/96 | 16:43:38 | 510      | 191.064    | 15.82   |
| 07/18/96 | 16:58:38 | 525      | 191.064    | 15.82   |
| 07/18/96 | 17:13:38 | 540      | 191.064    | 15.82   |
| 07/18/96 | 17:28:38 | 555      | 191.064    | 15.82   |
| 07/18/96 | 17:43:38 | 570      | 191.061    | 15.82   |
| 07/18/96 | 17:58:38 | 585      | 191.061    | 15.82   |
| 07/18/96 | 18:13:38 | 600      | 191.059    | 15.82   |
| 07/18/96 | 18:28:38 | 615      | 191.059    | 15.82   |
| 07/18/96 | 18:43:38 | 630      | 191.058    | 15.82   |
| 07/18/96 | 18:58:38 | 645      | 191.059    | 15.82   |
| 07/18/96 | 19:13:38 | 660      | 191.058    | 15.82   |
| 07/18/96 | 19:28:38 | 675      | 191.059    | 15.83   |
| 07/18/96 | 19:43:38 | 690      | 191.058    | 15.83   |
| 07/18/96 | 19:58:38 | 705      | 191.058    | 15.83   |
| 07/18/96 | 20:13:38 | 720      | 191.058    | 15.83   |

| Date     | Time     | ET (min) | Meters H2O | Celsius |
|----------|----------|----------|------------|---------|
| 07/18/96 | 20:28:38 | 735      | 191.058    | 15.84   |
| 07/18/96 | 20:43:38 | 750      | 191.058    | 15.84   |
| 07/18/96 | 20:58:38 | 765      | 191.058    | 15.84   |
| 07/18/96 | 21:13:38 | 780      | 191.058    | 15.84   |
| 07/18/96 | 21:28:38 | 795      | 191.058    | 15.84   |
| 07/18/96 | 21:43:38 | 810      | 191.058    | 15.84   |
| 07/18/96 | 21:58:38 | 825      | 191.058    | 15.84   |
| 07/18/96 | 22:13:38 | 840      | 191.058    | 15.84   |
| 07/18/96 | 22:28:38 | 855      | 191.058    | 15.84   |
| 07/18/96 | 22:43:38 | 870      | 191.057    | 15.85   |
| 07/18/96 | 22:58:38 | 885      | 191.057    | 15.85   |
| 07/18/96 | 23:13:38 | 900      | 191.057    | 15.85   |
| 07/18/96 | 23:28:38 | 915      | 191.058    | 15.85   |
| 07/18/96 | 23:43:38 | 930      | 191.058    | 15.85   |
| 07/18/96 | 23:58:38 | 945      | 191.058    | 15.85   |
| 07/19/96 | 0:13:38  | 960      | 191.057    | 15.85   |
| 07/19/96 | 0:28:38  | 975      | 191.058    | 15.85   |
| 07/19/96 | 0:43:38  | 990      | 191.057    | 15.85   |
| 07/19/96 | 0:58:38  | 1005     | 191.057    | 15.85   |
| 07/19/96 | 1:13:38  | 1020     | 191.057    | 15.85   |
| 07/19/96 | 1:28:38  | 1035     | 191.057    | 15.85   |
| 07/19/96 | 1:43:38  | 1050     | 191.055    | 15.86   |
| 07/19/96 | 1:58:38  | 1065     | 191.057    | 15.86   |
| 07/19/96 | 2:13:38  | 1080     | 191.055    | 15.85   |
| 07/19/96 | 2:28:38  | 1095     | 191.055    | 15.86   |
| 07/19/96 | 2:43:38  | 1110     | 191.057    | 15.86   |
| 07/19/96 | 2:58:38  | 1125     | 191.057    | 15.86   |
| 07/19/96 | 3:13:38  | 1140     | 191.055    | 15.86   |
| 07/19/96 | 3:28:38  | 1155     | 191.057    | 15.86   |
| 07/19/96 | 3:43:38  | 1170     | 191.055    | 15.86   |
| 07/19/96 | 3:58:38  | 1185     | 191.055    | 15.87   |
| 07/19/96 | 4:13:38  | 1200     | 191.054    | 15.87   |
| 07/19/96 | 4:28:38  | 1215     | 191.054    | 15.87   |
| 07/19/96 | 4:43:38  | 1230     | 191.054    | 15.87   |
| 07/19/96 | 4:58:38  | 1245     | 191.054    | 15.87   |
| 07/19/96 | 5:13:38  | 1260     | 191.054    | 15.87   |
| 07/19/96 | 5:28:38  | 1275     | 191.054    | 15.87   |
| 07/19/96 | 5:43:38  | 1290     | 191.055    | 15.87   |
| 07/19/96 | 5:58:38  | 1305     | 191.054    | 15.87   |
| 07/19/96 | 6:13:38  | 1320     | 191.052    | 15.87   |
| 07/19/96 | 6:28:38  | 1335     | 191.052    | 15.87   |
| 07/19/96 | 6:43:38  | 1350     | 191.052    | 15.87   |
| 07/19/96 | 6:58:38  | 1365     | 191.05     | 15.88   |
| 07/19/96 | 7:13:38  | 1380     | 191.05     | 15.88   |
| 07/19/96 | 7:28:38  | 1395     | 191.05     | 15.88   |
| 07/19/96 | 7:43:38  | 1410     | 191.05     | 15.88   |
| 07/19/96 | 7:58:38  | 1425     | 191.048    | 15.88   |
| 07/19/96 | 8:13:38  | 1440     | 191.048    | 15.88   |
| 07/19/96 | 8:28:38  | 1455     | 191.048    | 15.88   |
| 07/19/96 | 8:43:38  | 1470     | 191.048    | 15.88   |

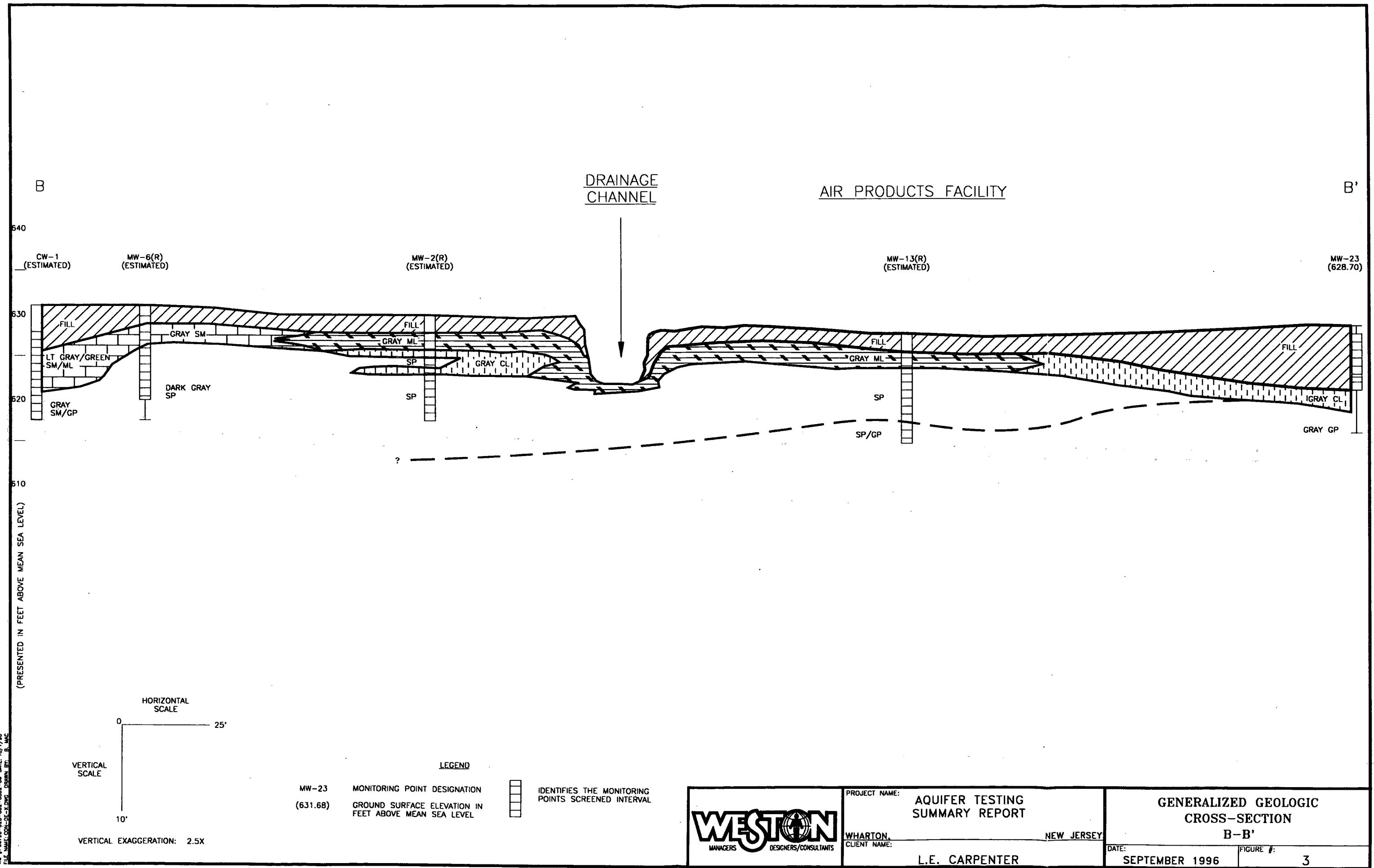
| Date     | Time     | ET (min) | Meters H2O | Celsius |
|----------|----------|----------|------------|---------|
| 07/19/96 | 8:58:38  | 1485     | 191.051    | 15.88   |
| 07/19/96 | 9:13:38  | 1500     | 191.054    | 15.88   |
| 07/19/96 | 9:28:38  | 1515     | 191.052    | 15.88   |
| 07/19/96 | 9:43:38  | 1530     | 191.052    | 15.88   |
| 07/19/96 | 9:58:38  | 1545     | 191.052    | 15.87   |
| 07/19/96 | 10:13:38 | 1560     | 191.051    | 15.88   |
| 07/19/96 | 10:28:38 | 1575     | 191.05     | 15.88   |
| 07/19/96 | 10:43:38 | 1590     | 191.048    | 15.88   |
| 07/19/96 | 10:58:38 | 1605     | 191.048    | 15.88   |
| 07/19/96 | 11:13:38 | 1620     | 191.05     | 15.88   |
| 07/19/96 | 11:28:38 | 1635     | 191.048    | 15.88   |
| 07/19/96 | 11:43:38 | 1650     | 191.048    | 15.88   |
| 07/19/96 | 11:58:38 | 1665     | 191.048    | 15.88   |
| 07/19/96 | 12:13:38 | 1680     | 191.047    | 15.88   |
| 07/19/96 | 12:28:38 | 1695     | 191.047    | 15.88   |
| 07/19/96 | 12:43:38 | 1710     | 191.047    | 15.88   |
| 07/19/96 | 12:58:38 | 1725     | 191.044    | 15.88   |
| 07/19/96 | 13:13:38 | 1740     | 191.044    | 15.88   |

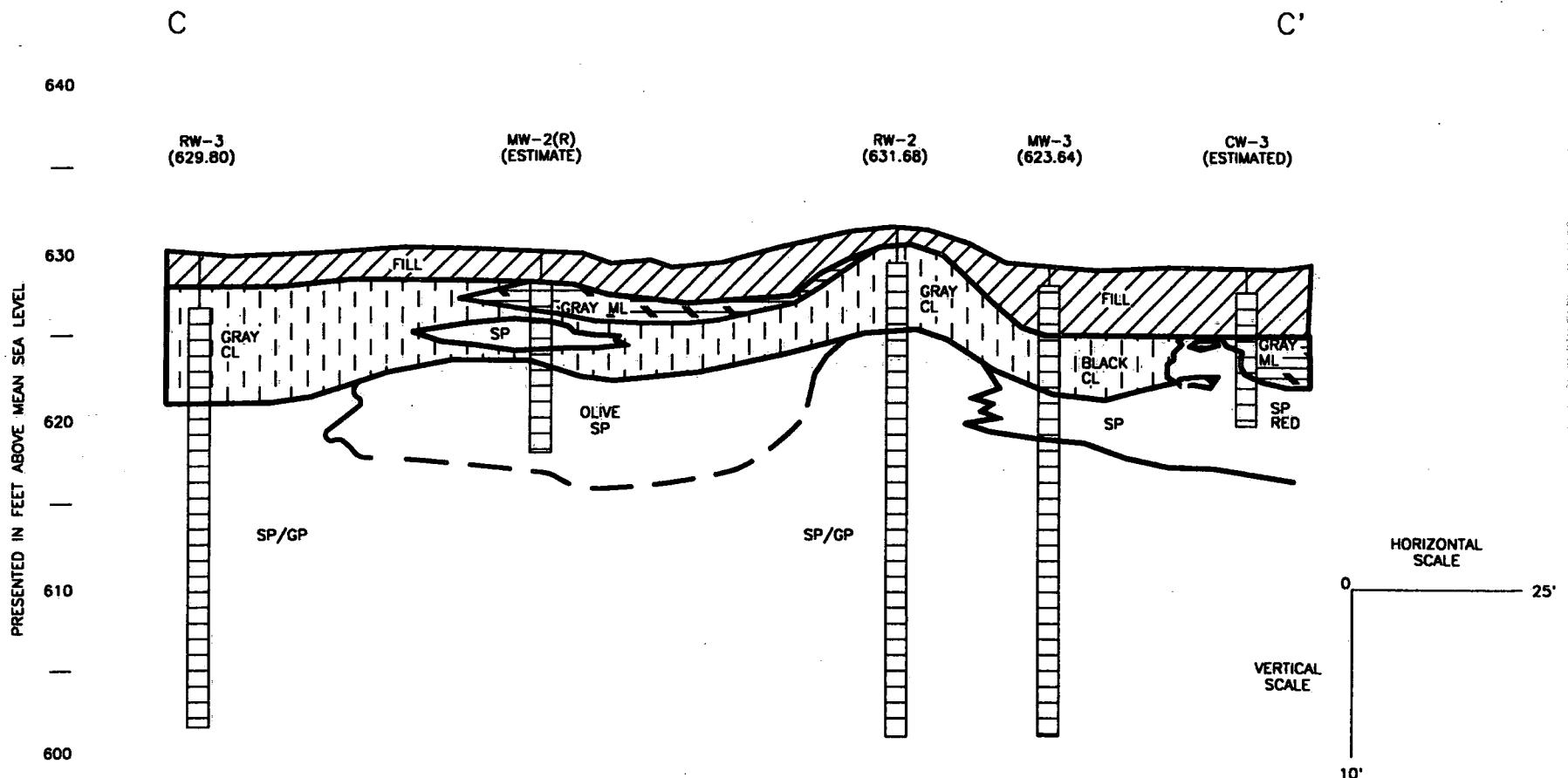


## APPENDIX F FIGURES









LEGEND

RW-2 MONITORING POINT DESIGNATION  
(631.68) GROUND SURFACE ELEVATION IN  
FEET ABOVE MEAN SEA LEVEL



IDENTIFIES THE WELL'S  
SCREENED INTERVAL



PROJECT NAME:

SUMMARY REPORT  
AQUIFER TESTING

WHARTON  
CLIENT NAME:

NEW JERSEY

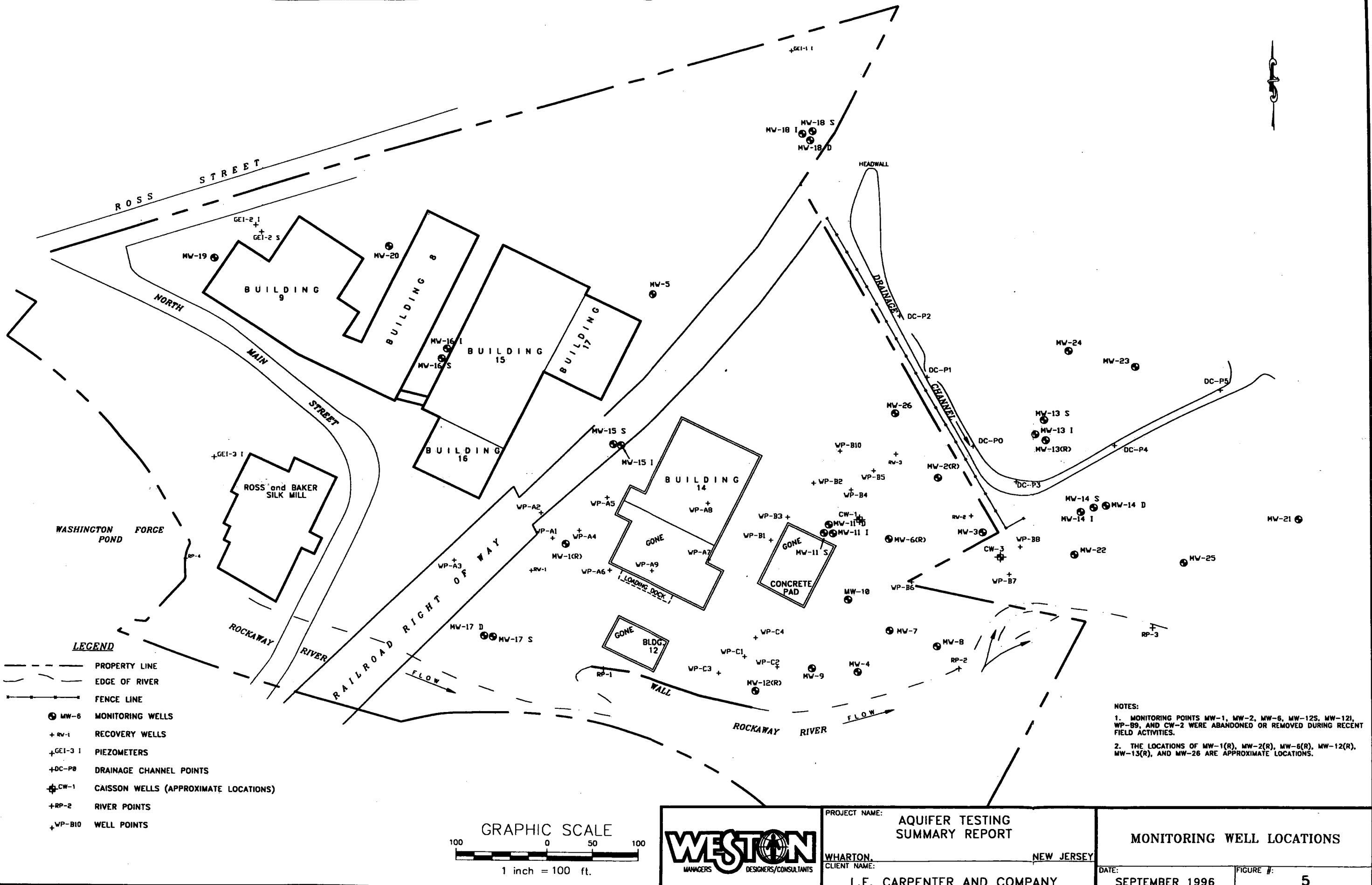
L.E. CARPENTER

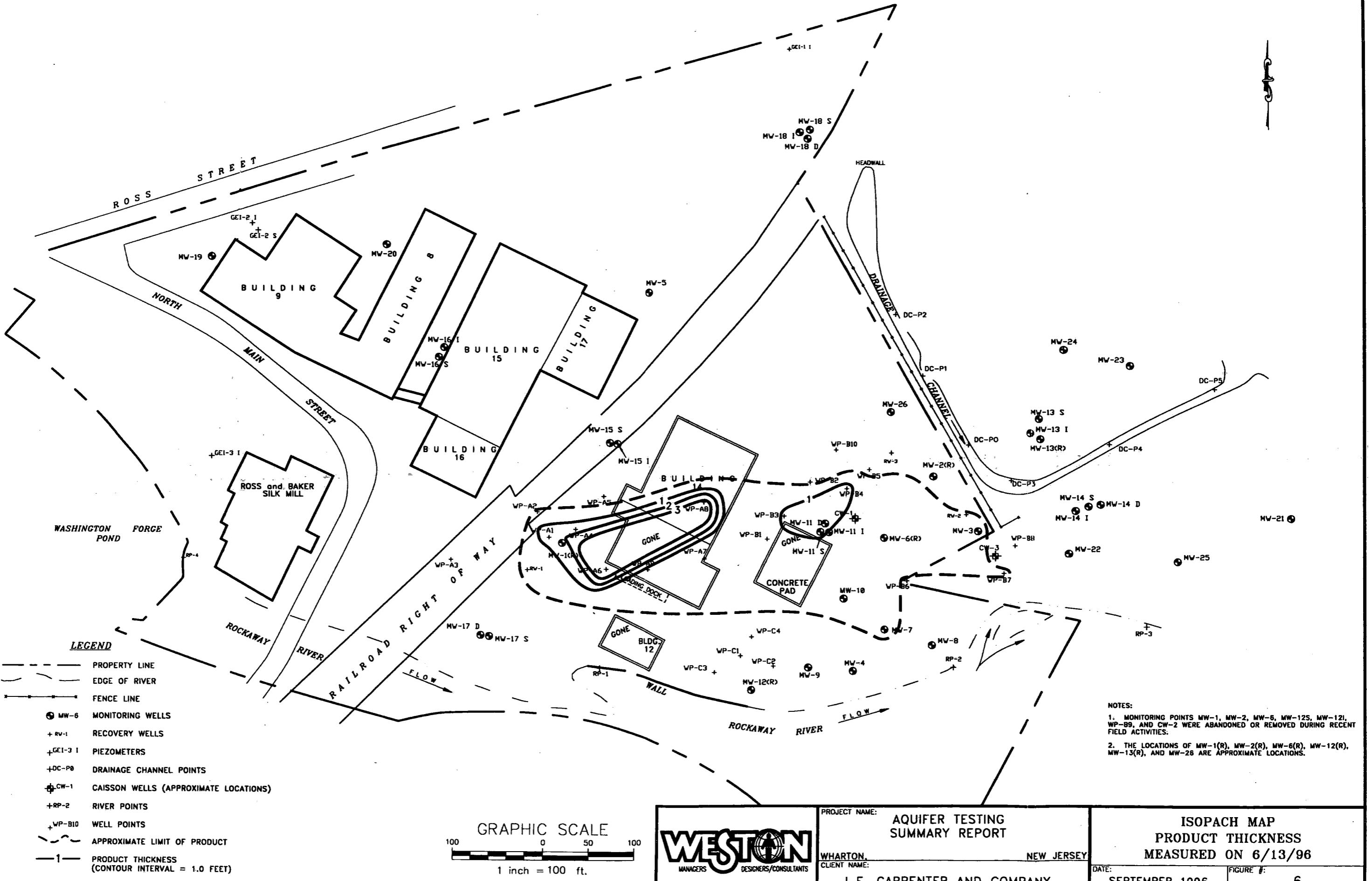
GENERALIZED GEOLOGIC  
CROSS-SECTION  
C-C'

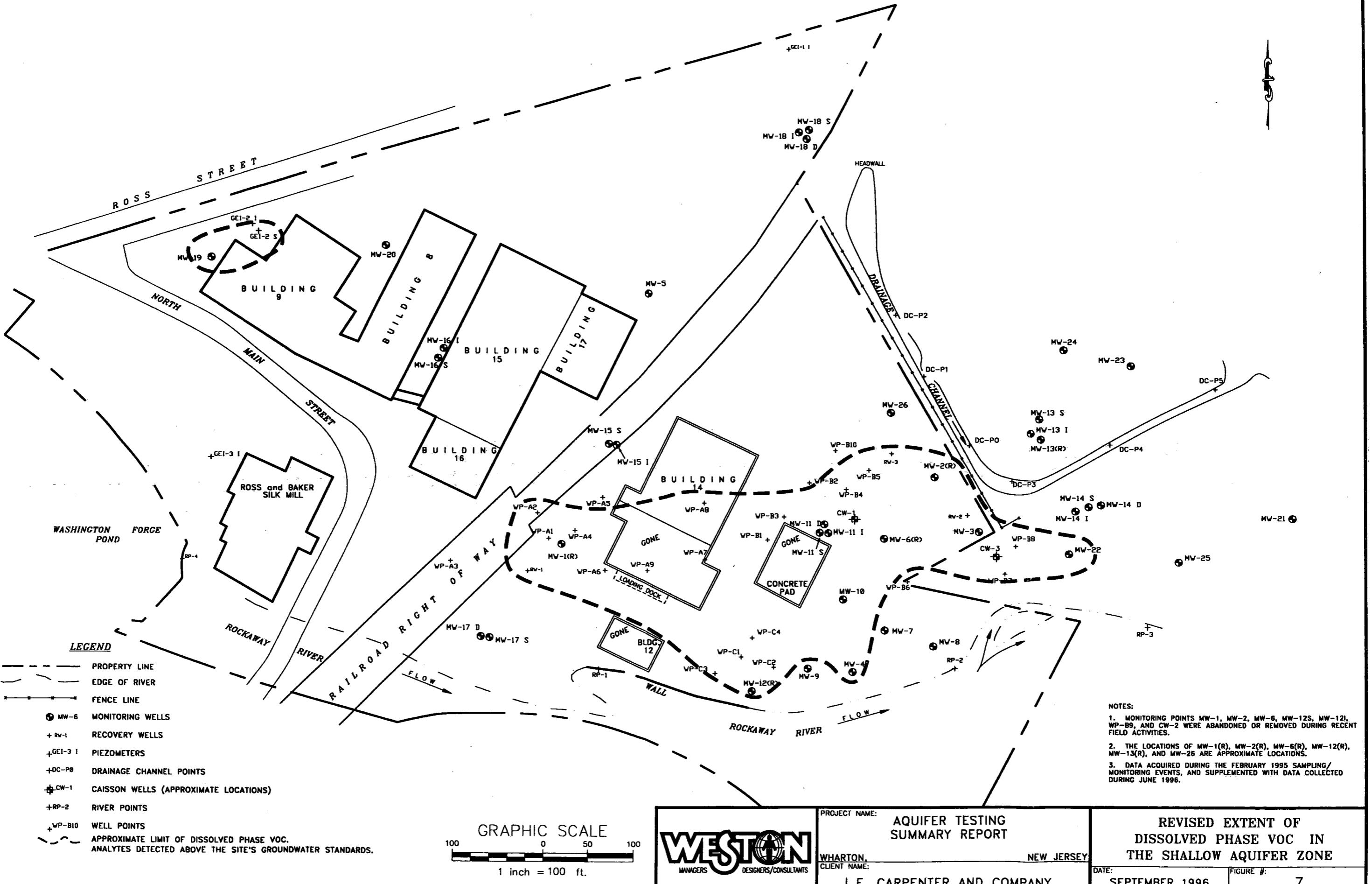
DATE:  
SEPTEMBER 1996

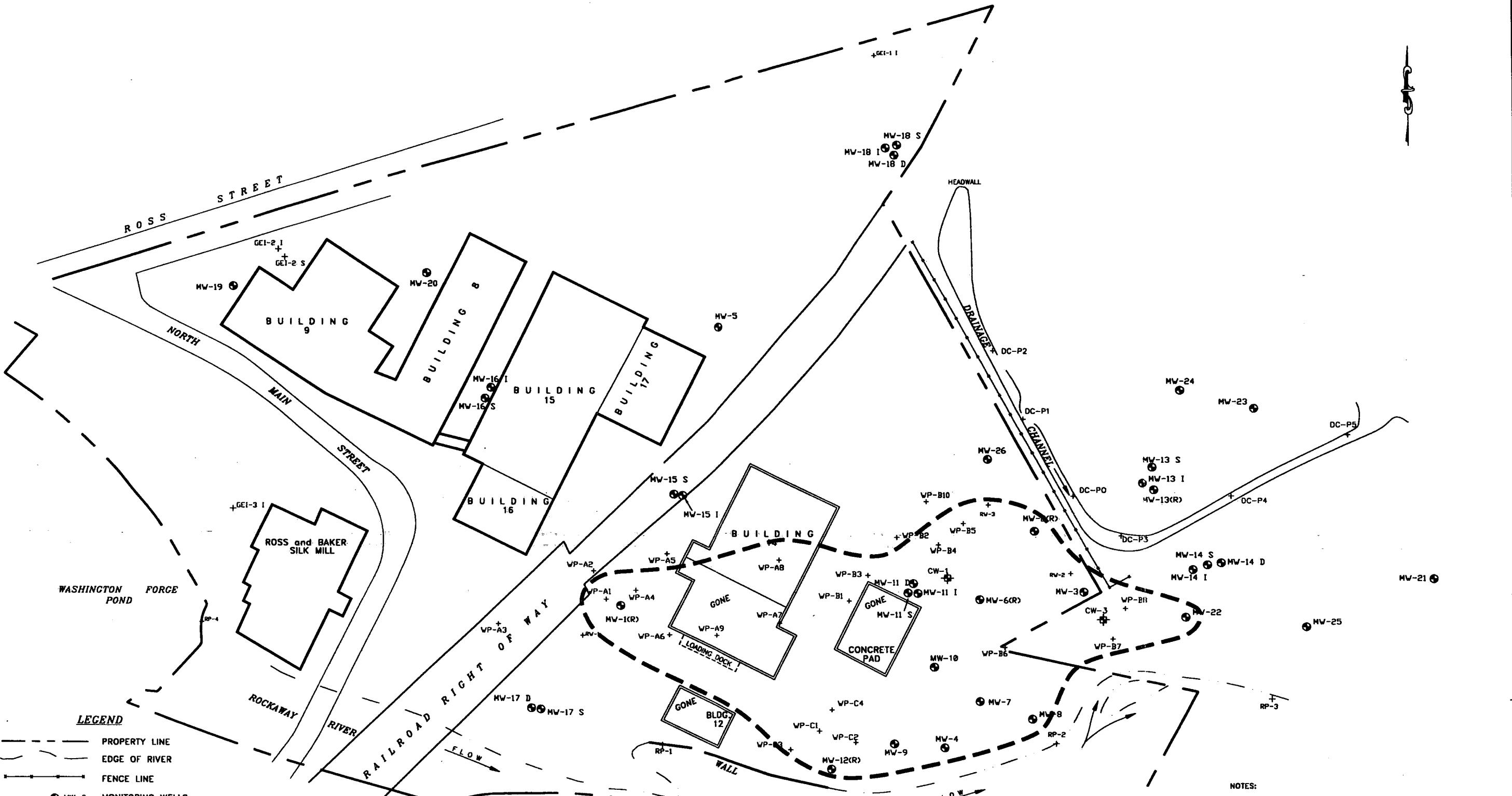
FIGURE #:

4







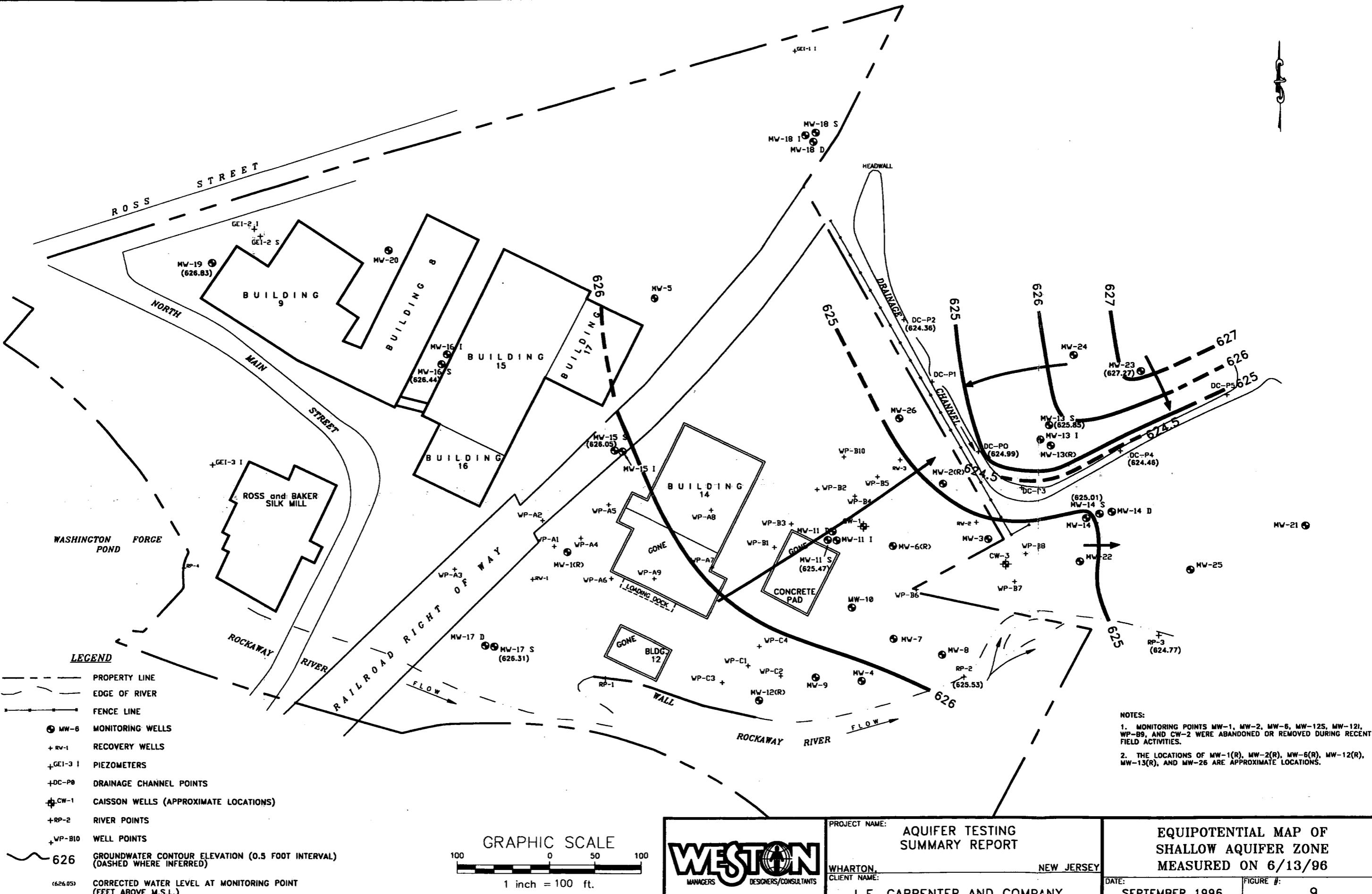


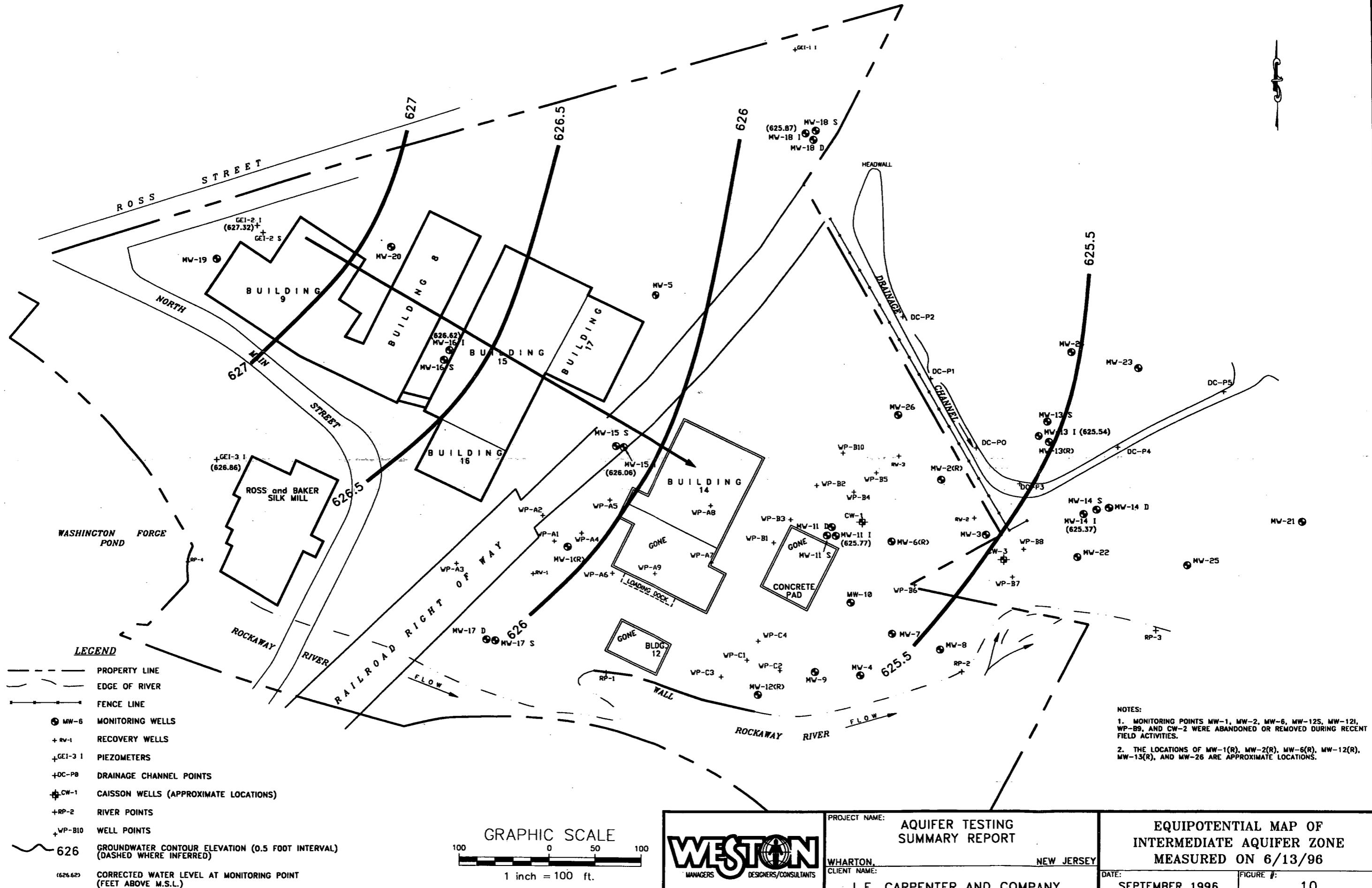
LEGEND

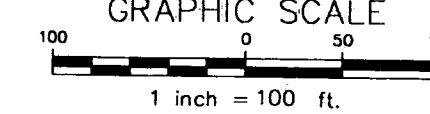
- PROPERTY LINE
- EDGE OF RIVER
- FENCE LINE
- MW-6 MONITORING WELLS
- + RV-1 RECOVERY WELLS
- + GEI-3 I PIEZOMETERS
- + DC-P0 DRAINAGE CHANNEL POINTS
- CW-1 CAISSON WELLS (APPROXIMATE LOCATIONS)
- + RP-2 RIVER POINTS
- + WP-B10 WELL POINTS
- APPROXIMATE LIMIT OF DISSOLVED PHASE BIS(2-ETHYLHEXYL)PHTHALATE (DEHP). ANALYTE DETECTED ABOVE THE SITE'S GROUNDWATER STANDARDS.

GRAPHIC SCALE  
100 0 50 100  
1 inch = 100 ft.

- NOTES:
- MONITORING POINTS MW-1, MW-2, MW-6, MW-12, MW-12S, MW-17, and CW-2 WERE ABANDONED OR REMOVED DURING RECENT FIELD ACTIVITIES.
  - THE LOCATIONS OF MW-1(R), MW-2(R), MW-6(R), MW-12(R), MW-13(R), and MW-26 ARE APPROXIMATE LOCATIONS.
  - DATA ACQUIRED DURING THE FEBRUARY AND JUNE 1995 SAMPLING/MONITORING EVENTS, AND SUPPLEMENTED WITH DATA COLLECTED DURING JUNE 1996.

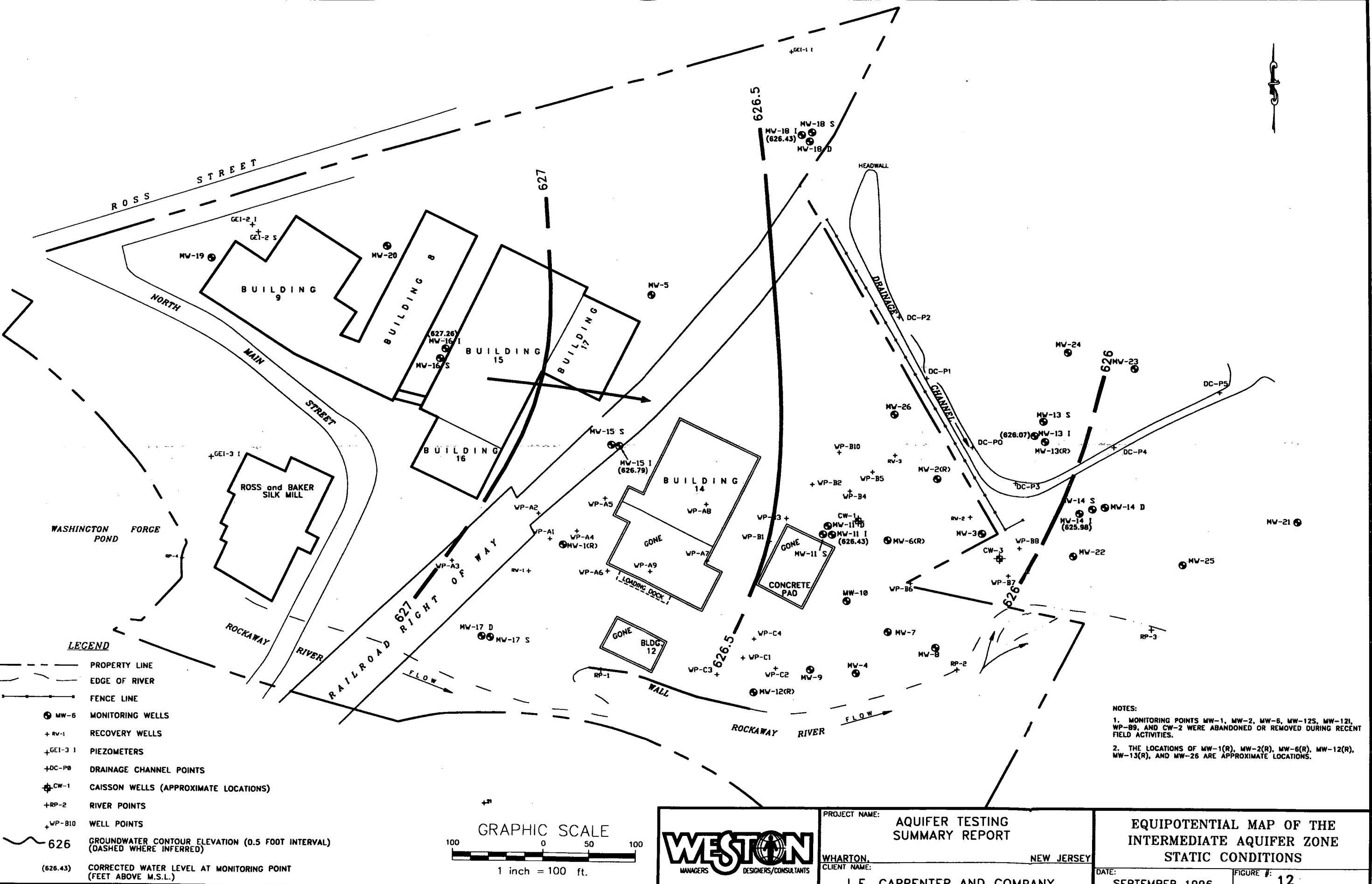


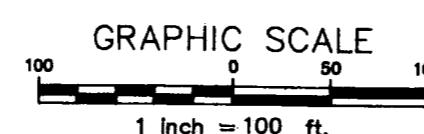
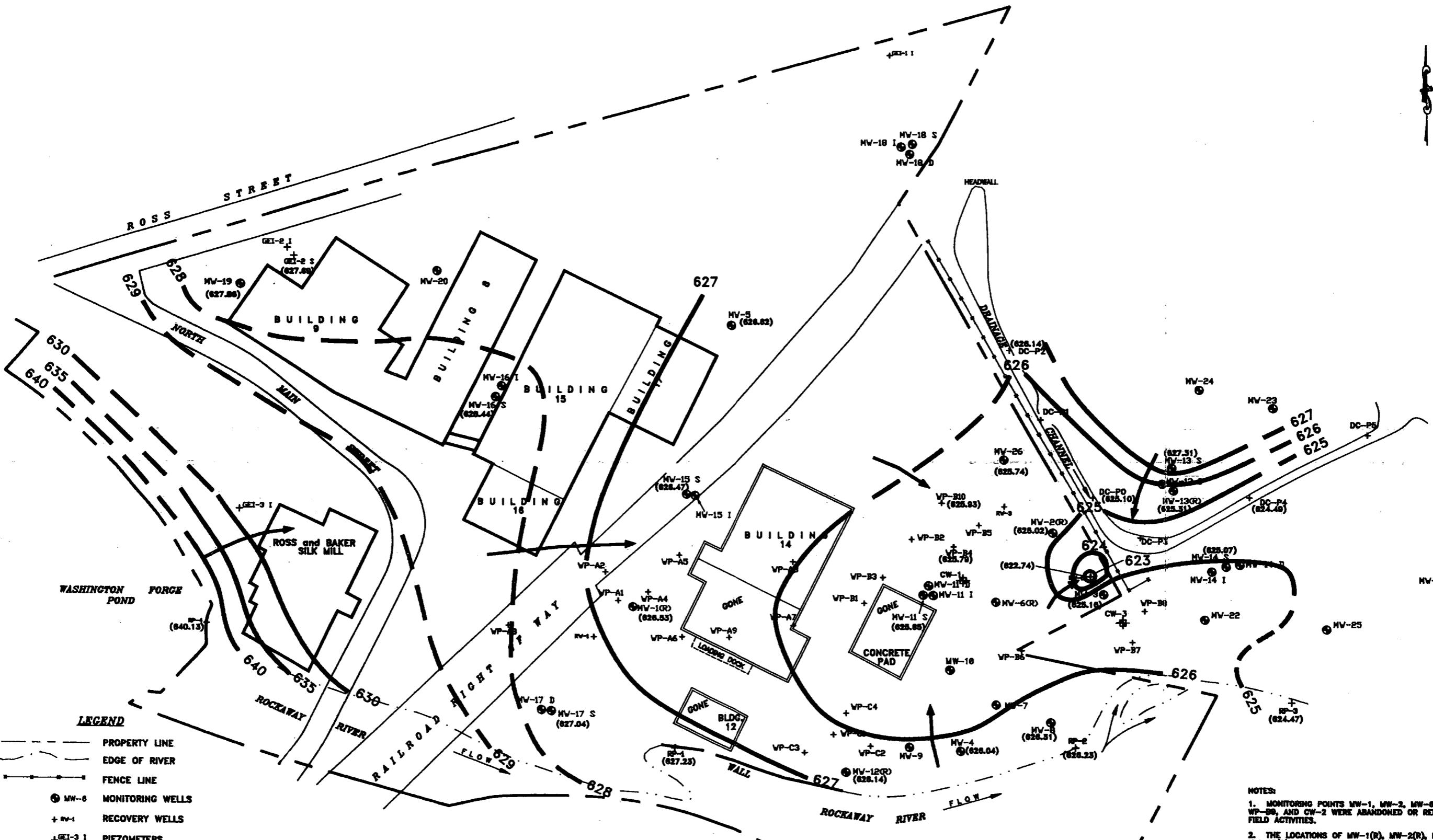




**NOTES:**

1. MONITORING POINTS MW-1, MW-2, MW-6, MW-12, MW-12I, WP-89, and CW-1 were abandoned or removed during recent field activities.
2. THE LOCATIONS OF MW-1(R), MW-2(R), MW-6(R), MW-12(R), MW-13(R), and MW-26 ARE APPROXIMATE LOCATIONS.



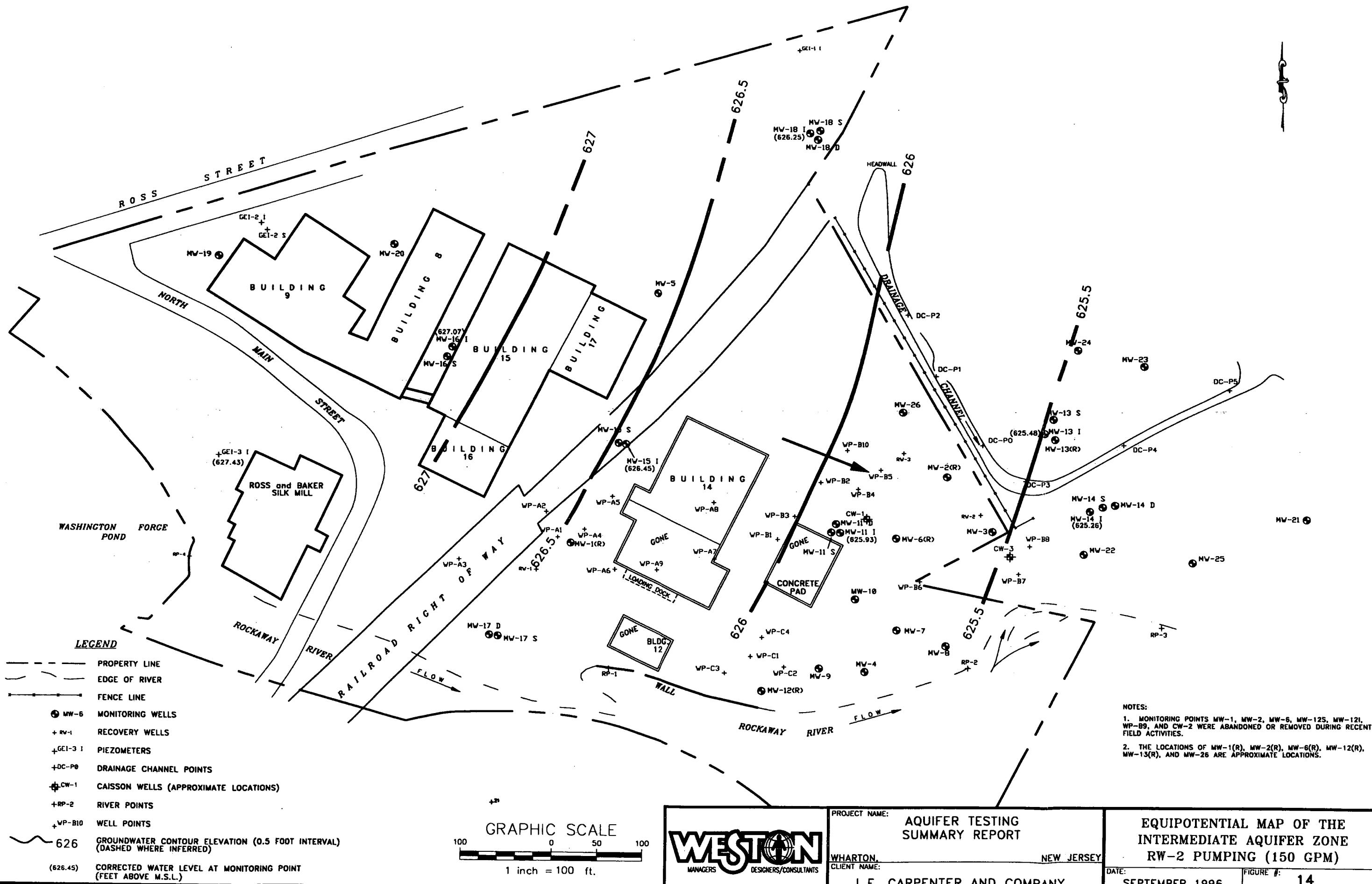


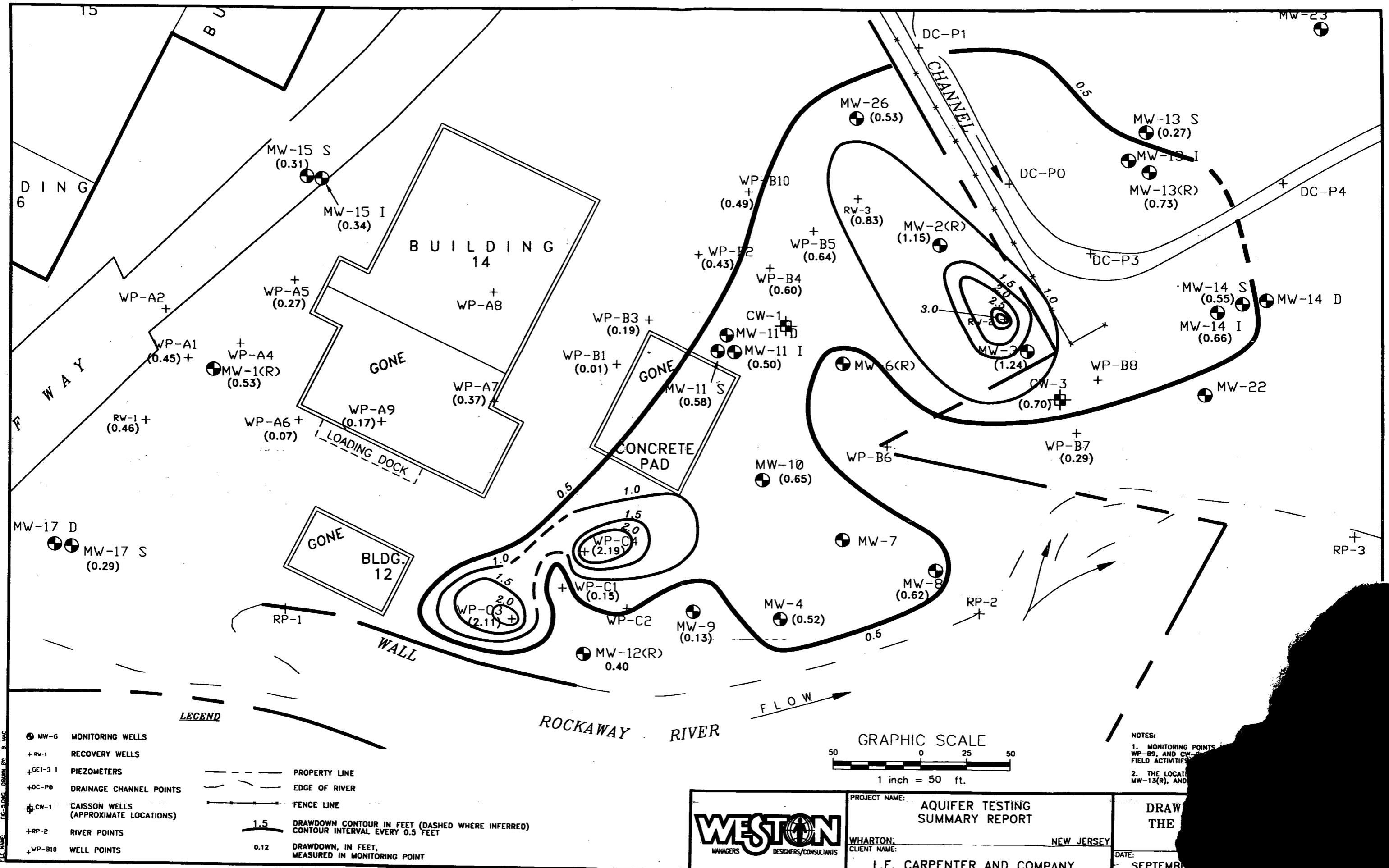
**WESTON**  
MANAGERS DESIGNERS/CONSULTANTS

PROJECT NAME: AQUIFER TESTING  
SUMMARY REPORT  
WHARTON, NEW JERSEY  
CLIENT NAME: L.E. CARPENTER AND COMPANY

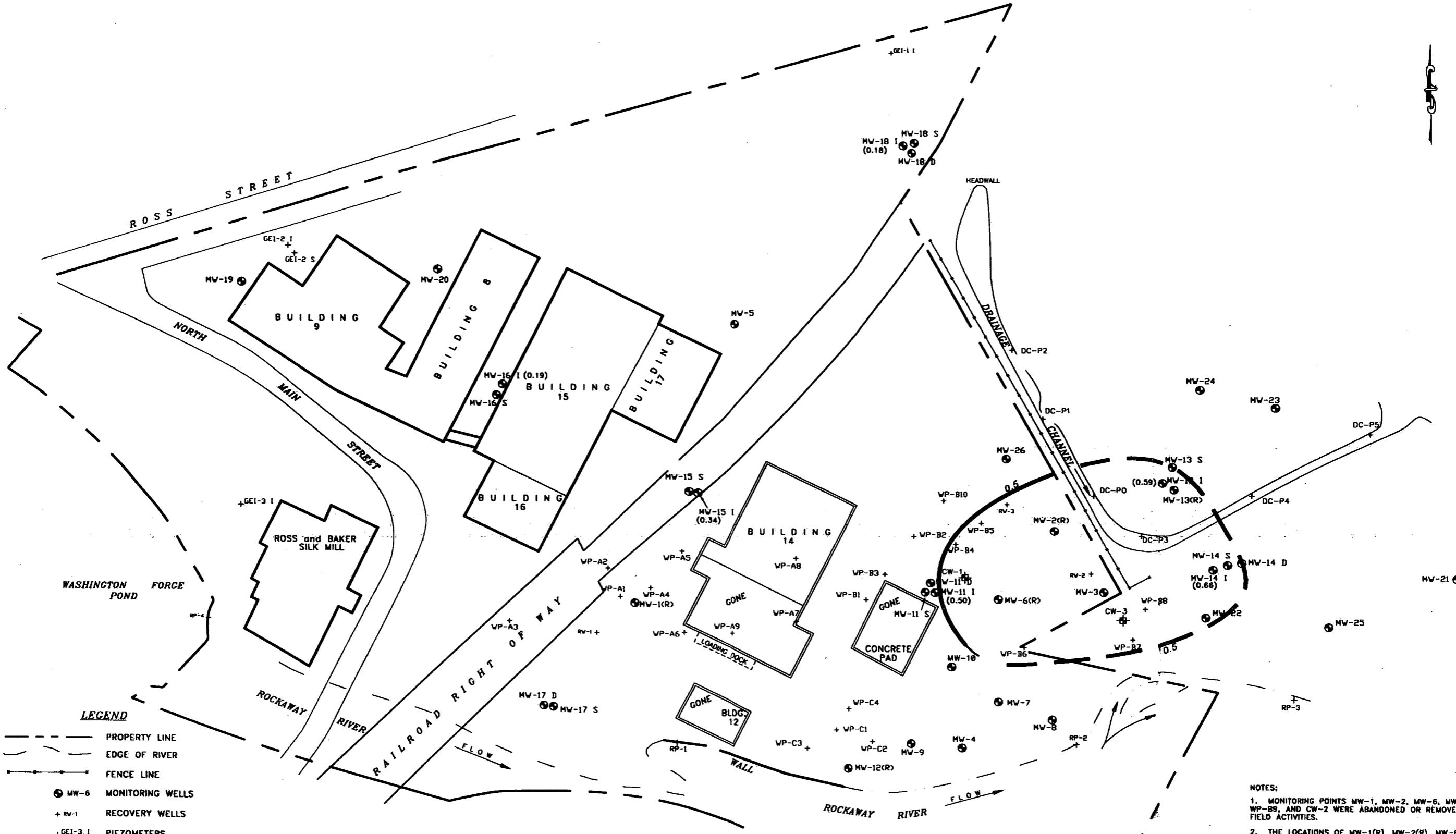
EQUIPOTENTIAL MAP OF THE  
SHALLOW AQUIFER ZONE  
RW-2 PUMPING (150 GPM)  
DATE: SEPTEMBER 1996 FIGURE #: 13

- NOTES:**
- MONITORING POINTS MW-1, MW-2, MW-8, MW-12L, MW-13L, and CW-2 WERE ABANDONED OR REMOVED DURING RECENT FIELD ACTIVITIES.
  - THE LOCATIONS OF MW-1(R), MW-2(R), MW-8(R), MW-12(R), MW-13(R), and MW-26 ARE APPROXIMATE LOCATIONS.





887720-002 -0002 -00 DATE: 8/19/98



GRAPHIC SCALE  
100 0 50 100  
1 inch = 100 ft.



PROJECT NAME: AQUIFER TESTING  
SUMMARY REPORT  
WHARTON, NEW JERSEY  
CLIENT NAME: L.E. CARPENTER AND COMPANY

DRAWDOWN CONTOUR WITHIN THE  
INTERMEDIATE AQUIFER ZONE  
DATE: SEPTEMBER 1996 FIGURE #: 16

NOTES:

- MONITORING POINTS MW-1, MW-2, MW-6, MW-12S, MW-12, MW-13, and MW-26 were abandoned or removed during recent field activities.
- THE LOCATIONS OF MW-1(R), MW-2(R), MW-6(R), MW-12(R), MW-13(R), and MW-26 are approximate locations.